

University of Hawaii at Manoa
Building Design and
Performance Standards

**MODELING
AddENDUM**

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INTRODUCTION

Early design decisions often have the largest impact on a building's energy use. These decisions are often made without the benefit of quantitative analysis. Later in the design process, when energy and possibly thermal comfort analyses become available, changing these large-scale decisions can be difficult.

For this reason, these UHM BDP Standards include a Modeling Addendum with combined climate and program analysis for classroom, offices and laboratory buildings. This is a "pre-design information package" to be handed out to the design team, outlining critical climate and program issues that need to be Addressed throughout the design process. The goal of this pre-design information is two-fold: first, it presents a process for developing useful quantitative energy analysis for a site and program before detailed project design actually begins. Second, it gives a context for the metrics required by these Standards and confirms that they are both ACHievable and reasonable in this climate.

This information was generated for the Standards and is grounded in scientific principles, rather than less precise rule-of-thumb measures and general guidelines often employed at these early project stages. The Project Development Report (PDR) provided to the architectural design team at the beginning of the design phase of the project could also include or refer to these studies to give an example of what is expected of the design teams in terms of analysis process and submittal documentation. The studies will allow the design to commence strategically with regard to daylight, comfort, energy and will be useful in moving projects progressively towards the mandated zero net energy goal by 2035.

This information is specific to each building type on UHM campus and includes a weather data analysis, daylighting and shading studies, HVAC autonomy and thermal comfort studies, and energy studies. These provide a reference for design teams to pursue similar analysis to evaluate building performance against the metrics required in these Standards. Some examples of efficient electric lighting designs for classrooms, offices and laboratories are also included, to support assumptions included in thermal comfort and energy models.

Add/ Introduction (Continued)

The UHM BDP Standards require multiple updates to energy models during the design process on new construction projects and significant building renovations (Group 1) to ensure that appropriate measures are being tested at every stage of design. Energy modeling allows in-depth comparative analysis of potential building systems and design strategies to optimize energy performance. Modeling is to be used as a design tool first and a compliance tool second. Building performance modeling as a design tool enables the team to make integrated design decisions based on a full understanding of cost and how systems interact.

The following pages present a process for developing comparative quantitative daylight, energy and comfort analysis for an existing building and program before actual design begins. The classroom, which is repeated many times in buildings on campus, was the starting point for investigation.

Shading and daylighting are both primary tools to increase occupant comfort and lower energy use, but they are often in conflict. In order to determine the potential for maximizing visual comfort, lighting levels and solar control while reducing use of electric lighting, the daylight studies focused on a typical existing classroom. These studies generated balanced design solutions that then served as input in terms of shading strategies (recommended profile angles) and window sizes (minimum and maximum window to wall ratio) for the comfort and energy models.

The next step towards understanding the potential for existing buildings on UHM campus to reduce energy use, as mandated by both State and University policies, and also move towards net zero performance by 2035, focused on the passive potential for each building type and each orientation.

The goal of zero-net-energy performance requires maximum hours of comfort delivered passively through building envelope design and control without mechanical conditioning. The most energy is saved if comfort is Achieved passively, without active systems. Using comfort load factor diagrams and parametric simulations we identified suites of passive strategies that minimize need for mechanical conditioning. Simulations of various envelope configurations quantify the impact of natural ventilation, thermal mass, roof and wall insulation, glazing specification, efficient

Add/ Introduction (Continued)

lighting design and daylighting controls on both the annual energy use and the hour-by-hour thermal comfort of occupants.

Once a set of suites representing the potential new and retrofit projects for existing UHM buildings were identified, an appropriate mechanical system was included in the models. Assumptions for ceiling fans and smart controls were also made. Energy use was then studied and compared between the different suites.

In most integrated, sustainable design practices, energy analyses beyond a baseline model do not come into the process until after an initial design has been proposed. Working without a preliminary design and instead using conceptually defined “ideal” design characteristics for repeated units on campus sets a high bar for the design teams. This strategy is well suited to any program with repeated or dominant elements.

Providing the design team with detailed analysis of the energy potential of the climate and program allows the design teams to move in a direction conducive to passive strategies immediately in their design process. Access to light and air become primary informants to program locations and orientations on the site at the onset. Typical space studies allow the design team to understand the passive needs of each project so they can immediately negotiate these with other needs of the project including mitigating outdoor air quality and acoustics.

Finally, a preliminary basic net zero feasibility study assuming potential PV output for both typical and high performance PV panels in this climate was developed to establish how far from Achieving the net zero performance goal each building type is.

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Add/A. CLIMATE AND WEATHER DATA ANALYSIS

The climatic conditions have a strong influence on the optimal design of a high performance building and can reveal potential design opportunities and limitations. Culturally, local climate knowledge such as local winds is already used in everyday decision-making. Thus, climate issues need to be one of the key drivers throughout the design process. In this section, we provide a detailed data analysis of the TMY3 weather data from Honolulu Airport. We highlighted and identified the information that is critical for building performance in order to identify conditions and periods that might affect the modeling results and, as a consequence, the building designs.

A typical meteorological year (TMY) is a collation of selected weather data for a specific location, generated from a data bank derived from a 1973-2005 period of record. It is selected so that it presents the range of weather phenomena for the location in question, while still giving annual averages that are consistent with the long-term averages. In other words, these data were selected because they did not contain extremes.

Some of the variables that are used as input in building performance models include:

- Sky conditions (Global Horizontal Radiation, Diffuse horizontal radiation, Direct normal irradiation and Cloud Cover)
- Wind conditions (Wind Speed and Direction)
- Air Conditions (Dry bulb Temperature, Relative Humidity)

We compared the weather data from the Honolulu Airport to the weather data collected by several weather stations on UHM campus to understand the effect of microclimate impacts on building performance.

There is general meso-climatic knowledge, if not data, regarding the location of the campus. The trade winds are typically funneled down the valley. They can run parallel to the valley walls and have up-slope edges along the East ridge. Weather stations on the campus should confirm historic wind directions that may vary from the airport. The

Add/A. Climate and Weather Data Analysis (Continued)

confirmation of this data would also help at a planning scale in siting buildings as well as developing strategies to ventilate them.

However, in the campus data for air and sky conditions, microclimatic differences are either not evident or show that the UHM campus is minimally cooler than the airport. University of Hawaii at Manoa Campus is higher in altitude and further away from the ocean than the Honolulu airport. The temperature tends to be generally lower, which will make interior comfortable conditions easier to Achieve in buildings. Thus, the weather data from the Honolulu Airport provides a useful conservative assumptions and is valid for building performance prediction purposes.

As the weather stations on campus only collected reliable information for certain variables, a complete weather data set to be used in energy modeling was not available, and thus daylight, comfort and energy models results could not be compared between using typical meteorological data sets (TMY) and actual meteorological year (AMY) data sets.

In order to simulate conditions under actual peak conditions (such as heat waves), it is critical to compare building performance under this typical meteorological data set (TMY) to an actual meteorological year (AMY) data that might be more representative of the future conditions buildings will need to endure in the next 20 years. This should be included in an update of the Standards when possible.

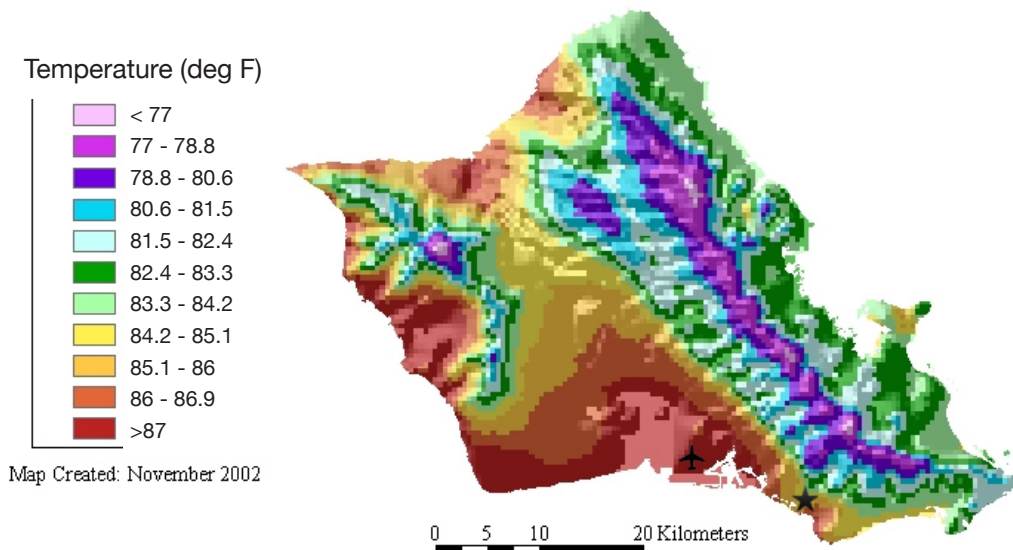
The design team should review available weather data in order to select or build a dataset that is representative of the weather expected on site. Review any available site-specific data to determine if any adjustments from airport (TMY or AMY) data are required to account for differences in microclimate, especially regarding wind conditions and opportunities for naturally ventilated spaces.

Add/A. CLIMATE AND WEATHER DATA ANALYSIS

1. CLIMATE ANALYSIS

The Hawaiian climate zones can be grouped into four types according to air temperature, precipitation, cloud cover, wind and elevation. Honolulu, Oahu is a representative example of a leeward, dry site at low elevation while Manoa is higher in elevation and closer to the mountains.

Climate includes other variables like humidity and solar radiation. To assess the climate of Honolulu, Typical Meteorological Year (TMY) data was used. This type of data is standard for performance evaluation and highly useful for simulations because it includes a large number of variables (60). The TMY data sets are based on measured data for every hour over the course of the year. The data set also does not simply, average all the years together, but tries to accurately portray a typical year, including storms, heat spells, dry spells, etc.



Add/A.1 Climate Analysis (Continued)

1. TEMPERATURE

Temperature in Hawaii is strongly correlated to elevation, distance from the coast and the influence of trade winds. However, the diurnal temperature change is fairly consistent among locations and is generally limited to a 10F swing. Throughout the Hawaiian islands, the temperature band is typically between 60F-80F. Temperature affects the comfort of the occupants, and is directly related to the potential performance of natural ventilation to provide comfort, as well as to the demand on the cooling system.

Honolulu experiences a tropical semi-arid climate, with a mostly dry summer season, due to a rain shadow effect. Temperatures vary little throughout the months, with average high temperatures of 80–90 °F (27–32°C) and average lows of 65–75 °F (18–24 °C) throughout the year. Temperatures reach or exceed 90 °F (32 °C) on an average 38 days annually, with lows in the upper 50s °F (14–15 °C) occurring once or twice a year. The highest recorded temperature was 95 °F (35 °C) during a heat wave in September 1998. According to the National Weather Service, high temperatures in Honolulu are more frequently tying the record set for each date in the past. The lowest recorded temperature was 52 °F (11 °C) on February 16, 1902, and January 20, 1969. In 2014, the record high was 94°F on September 5th and the record low was 53°F on February 9th.

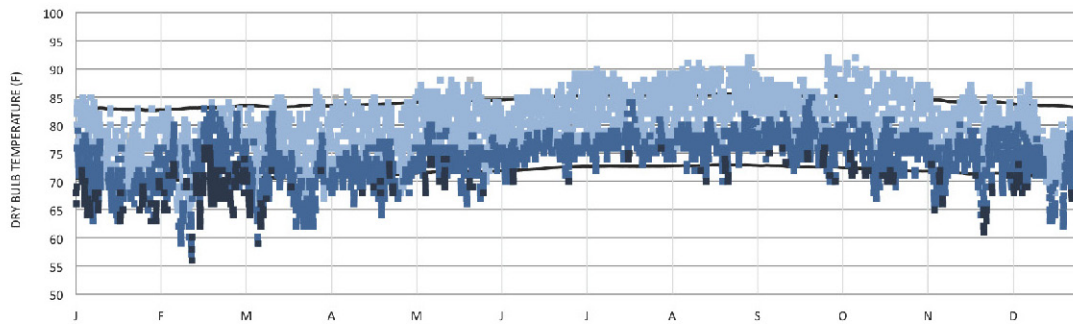


Fig 4.2. Honolulu Annual Outdoor Dry bulb Temperature and Humidity

Add /A.1 Climate Analysis (Continued)

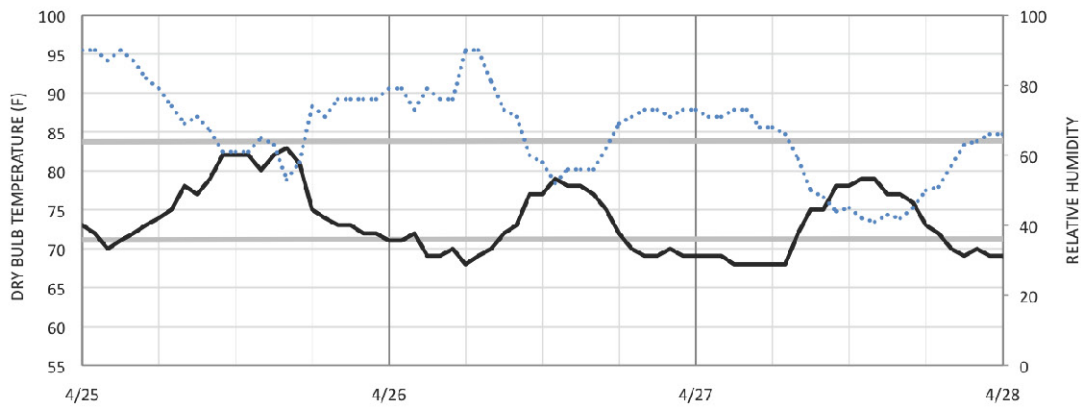


Fig 4.3. Honolulu Outdoor Dry Bulb Temperature and Humidity During A Typical Three Day Period (April 25th Thru April 28th)

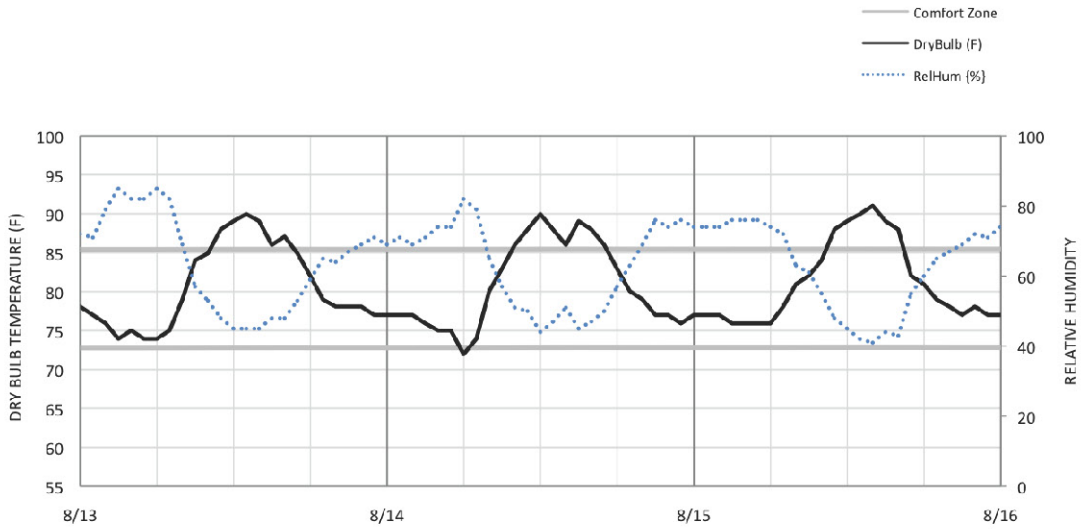


Fig 4.4. Honolulu Outdoor Dry Bulb Temperature and Humidity During A Hot Three Day Period (Aug 13th Thru Aug 16th)

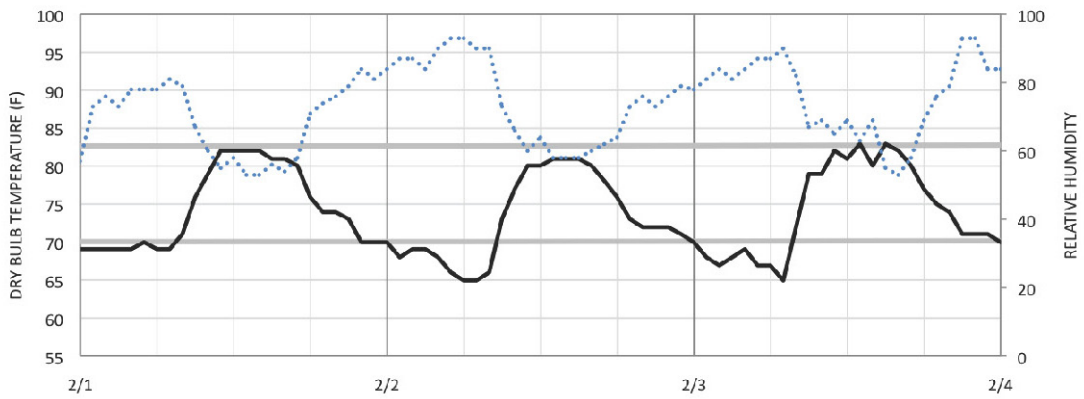
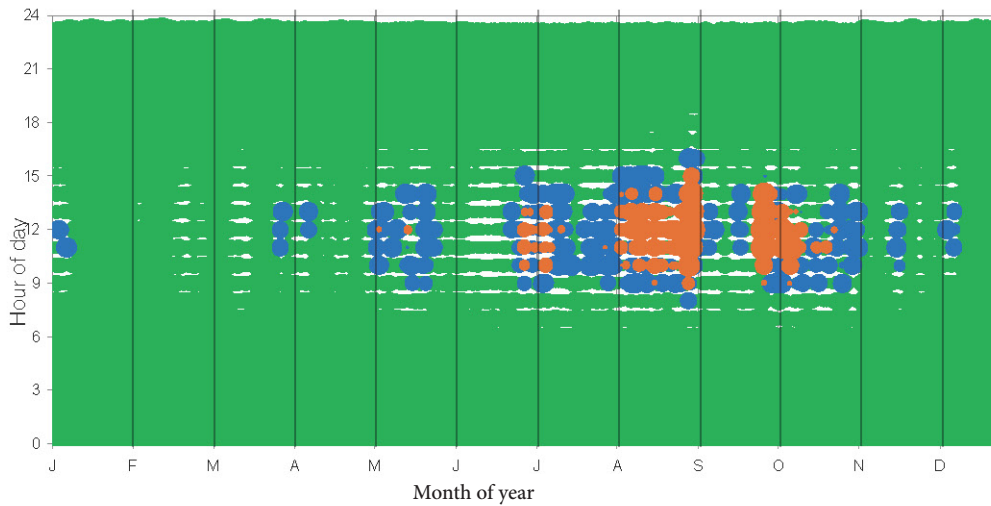


Fig 4.5. Honolulu Outdoor Dry Bulb Temperature and Humidity During A Three Day Period with Cold Nights (Feb 1st Thru Feb 4th)

Add/A.1 Climate Analysis (Continued)



Outside in Shade (with 1 m/s air speed) : **131** Hours of Discomfort Per Year



Fig 1. Honolulu Outdoor Conditions

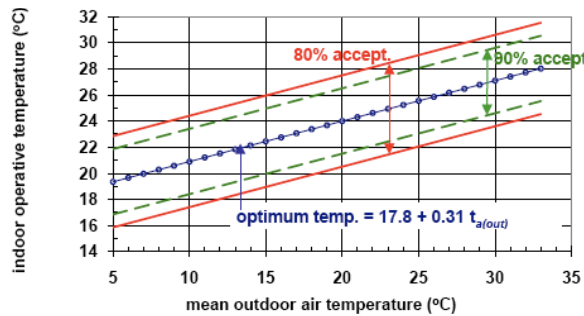


Fig 2. The ASHRAE Std 55 2010 Adaptive Comfort Standard in naturally ventilated spaces as a function of prevailing outdoor temperature. To (out) is simply an arithmetic average of the mean monthly minimum and maximum daily air temperatures for the month in question. The optimum indoor temperature is expressed in terms of operative temperature (approximately the average of air and mean radiant temperatures).

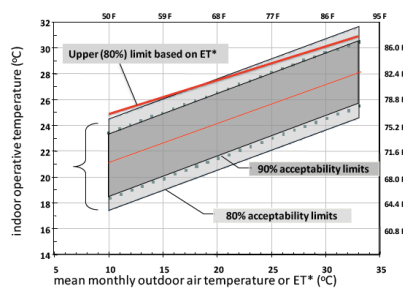


Fig 3. The ASHRAE Std 55 2010 Adaptive Comfort Standard in naturally ventilated spaces showing upper (80% acceptability) limit based on mean monthly ET*.

Add /A.1 Climate Analysis (Continued)

2. THERMAL COMFORT

A comfort analysis of outdoor conditions in Honolulu identifies when people feel comfortable throughout the year, and what they need to feel comfortable (in the shade with a breeze of 1m/sec).

The comfort criteria were set by collectively reviewing ASHRAE comfort standards. The upper limit for comfort is currently defined by an operative temperature of:

Upper 80% Acceptable Limit = $18.9\text{ }^{\circ}\text{C} + 0.255 * \text{outdoor mean ET}^*$ of past 15 days + $3.5\text{ }^{\circ}\text{C} + 2\text{ }(^{\circ}\text{C})$ increase from a mean air speed of about 1 m/s

Operative Temperature (OT) = $1/2 * \text{MRT} + 1/2 * \text{DBT}$

MRT = Mean radiant temperature DBT = Dry bulb temperature

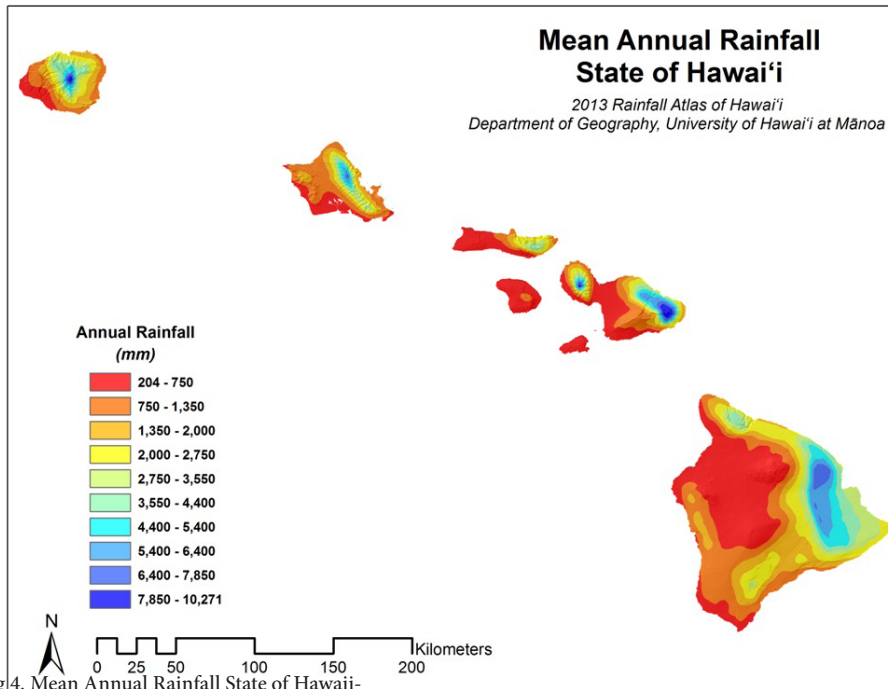
ET-Star (ET) is defined as the temperature at 50% relative humidity which would cause the same sensible plus latent heat exchange from a person as would the actual environment. This combines temperature and humidity into a single index, so two environments with the same ET* should provide the same thermal response even though they have different temperatures and humidities, as long as they have the same air velocities.*

The results showed that both being in the shade and having a 1m/s air movement, with no collected internal gains, provide comfort during most of the year. In other words, someone sitting under a tree with a breeze would feel comfortable most of the time.

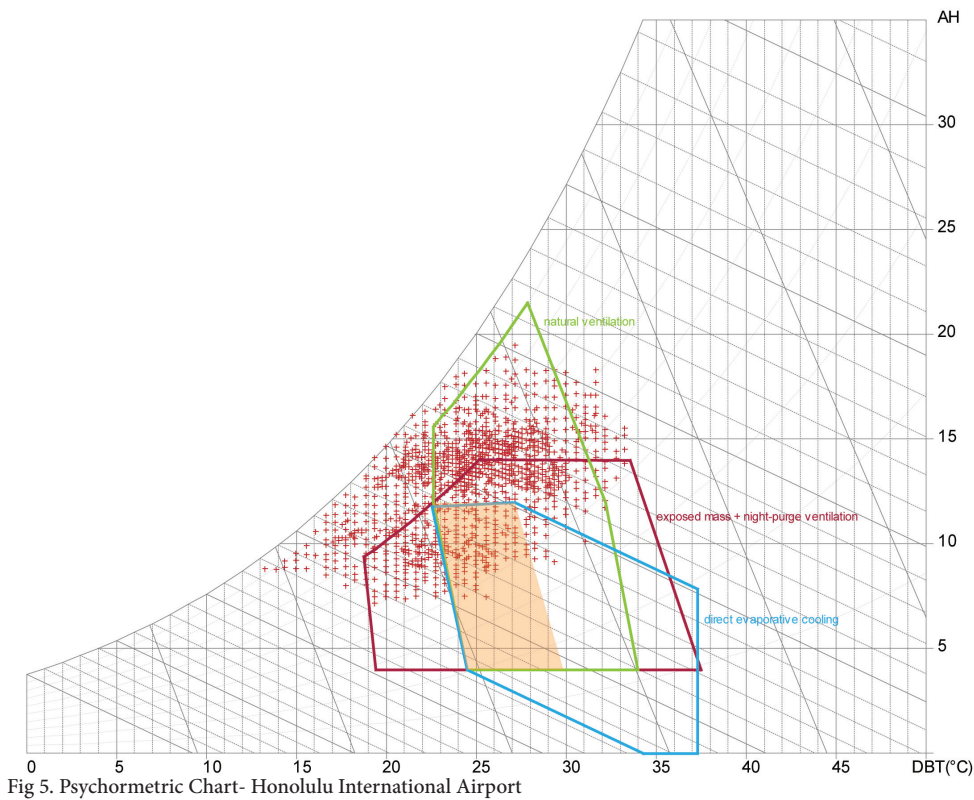
Fig 1 shows hourly comfort conditions outdoors. The horizontal axis gives each day of the year and the vertical axis shows each hour of the day with noon in the middle and midnight at the bottom and top. Green dots represent hours when people would feel comfortable; the “warm” dots (orange) represent hours warmer than comfortable; and light blue dots represent hours within 1degree C (1.8F) hotter than comfortable, meaning borderline of comfort conditions. The size of the dot represents the comparative intensity of comfort or discomfort.

In Fig 1, outdoors, the uncomfortable hours are only 131 per year and the bulk of them occurs between 9am and 3pm (when classes are in session), especially in August. There are also times of discomfort at the end of September/ beginning of October and end of July/ beginning of June, also between 9am and 3pm.

Add/A.1 Climate Analysis (Continued)



Source : 2013 Rainfall Atlas of Hawaii- UHM Dept of Geography



Add /A.1 Climate Analysis (Continued)**3. PRECIPITATION AND HUMIDITY**

Annual rainfall is influenced by location and elevation. Sites on the windward side of the islands can be very wet, as the tradewinds hit the higher elevations and drop precipitation, while those on the leeward side can be extremely dry. In Addition, as clouds rise up in elevation following volcanoes, they tend to release more of their moisture at the higher elevations. Precipitation levels affect the design of the envelope, the materials used in the structure and the amount of rainwater that the site can harvest. Relative humidity throughout the Hawaiian islands tends to be high which impacts the comfort of the occupants and the design of the envelope, the heating/cooling systems and the operation of the facility.

Relative humidity and dry bulb temperature move in opposite direction, making hot and relatively dry days and cool and humid nights. Because of the higher altitude and distance away from the ocean, the cold days at University of Hawaii are likely to be more temperate than that at the airport.

A psychometric chart helps to initially define the distribution of energy in the outdoor environment between “latent” energy carried by the moisture in the air, and “sensible” energy carried into the air molecules at a particular site. Figure 5 shows this distribution for Honolulu by plotting one point for each hour of the year, with daytime conditions in orange (gray box) shown on the chart is one of the main functions of a facility and its conditioning system. Temperature is along the x-axis and relative humidity along the y-axis. The orange box marks the comfort zone.

The combination of high humidity (close to upper curve) and high temperature (toward the right side of the chart) is the most challenging, as only compressive cooling can remove moisture and its energy from the air to make the internal environment comfortable. Compressive mechanical systems such as air conditioners reduce the relative humidity of the air in the facility as well as cooling the air, delivering comfort to occupants by making the interior conditions quite different than exterior conditions. A less energy intensive means of providing comfort under high humidity is to provide air movement across the skin with cross ventilation or ceiling fans.

Add/A.1 Climate Analysis (Continued)

With the conditions described above for temperature, relative humidity and outdoor thermal comfort, conditioning strategies such as mixed mode buildings will become critical in this climate. A well-designed mixed-mode building allows spaces to be naturally ventilated during periods of the day or year when it is feasible or desirable, and uses mechanical cooling only as necessary for supplemental cooling when natural ventilation is not sufficient. The goal is to maximize comfort while minimizing the significant energy use and operating costs of air conditioning.

4. WIND

Wind direction, frequency and velocity can have a significant effect on the potential to naturally ventilate a space, as well as the potential for wind power.

Regular trade winds are a key feature of the climate in the Hawaiian Islands. Mauka (mow-kah) means on the mountain side and Makai (mah-kigh) means on the ocean side. Moa’e, a’e, a’e loa, Moa’e Lehua, or Moa’e pehu are the names for the tradewind. Trade winds, which blow from a NE and ENE direction, account for 70% of all winds in Hawaii and are the most common winds over Hawaiian waters. During the summer, trades used to prevail more than 90% of the time, sometimes persisting throughout an entire month (see section B. *Impact of Climate Change*). However, in the winter (January through March), trade winds may occur only 40% to 60% of the time.

It is important to note that winds also change direction throughout the day (from Mauka to Makai) as highlighted in Figure 6 below. Buildings should be designed to accomodate such varying wind directions.

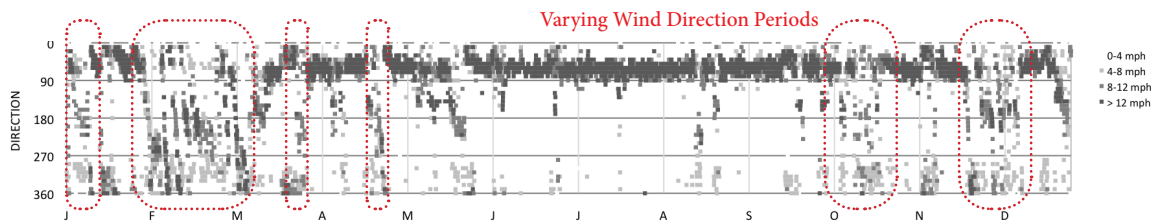


Fig 6. Honolulu Wind Speed and Direction

Add /A.1 Climate Analysis (Continued)

5. CLOUD COVER AND SOLAR RADIATION

Cloud cover is tied closely to solar radiation, which is important when designing for renewable solar energy, as well as to daylight design and performance. The amount of direct solar radiation influences the type of solar panels that can be used. In Addition, the amount of direct solar radiation influences the envelope design, such as shade length, insulation level, radiant barrier use and fenestration pattern, as well as orientation.

Overcast skies deliver daylight optimally through the horizontal plane (roof) since the sky is brighter at the zenith than the horizon. In contrast, clear skies deliver daylight effectively through the vertical plane (walls) as long as the direct sun

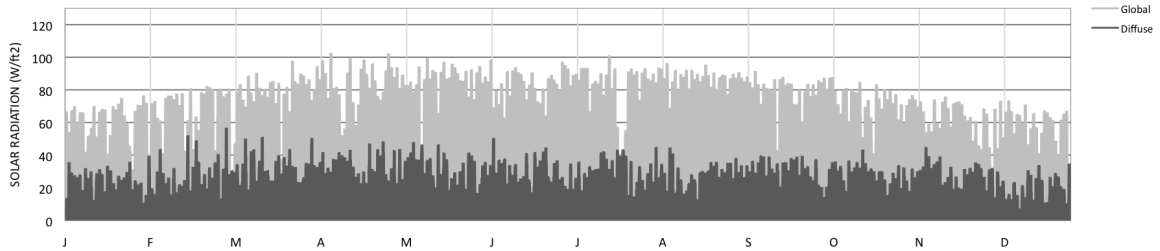


Fig 7. Honolulu Solar Radiation

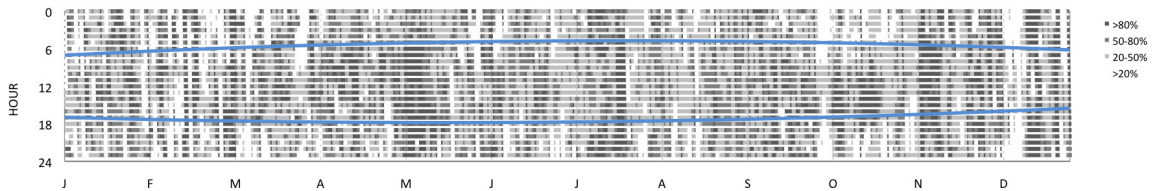


Fig 8. Honolulu Cloud Cover

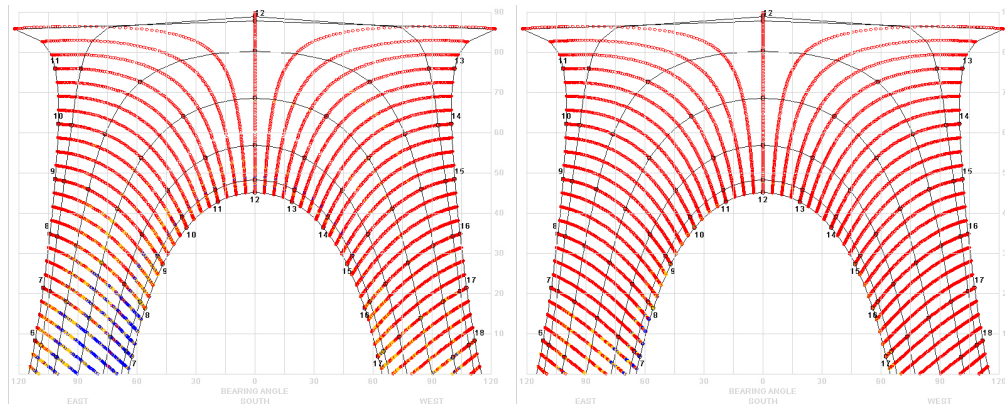


Fig 9. Honolulu Sun Shading Chart

- **WARM/HOT**
 (SHADE NEEDED)
 > 75 degrees F
- **COMFORT**
 (SHADE HELPS)
 > 70 degrees F
- **COOL/COLD**
 (SUN NEEDED)

Add/A.1 Climate Analysis (Continued)

penetration can be controlled. This is usually the cause for conflicts between the design of facade shading devices and daylight needs inside the buildings.

Another aspect of the Hawaii climate is that the sky conditions change from overcast to clear very frequently throughout the same day. Therefore, static shading devices often prove inadequate for these changeable conditions.

In summary, design teams for buildings in the UHM Campus need to be aware of the following:

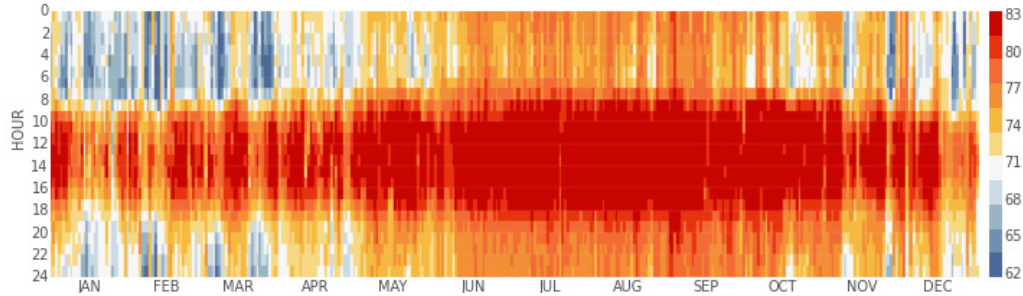
- Mixed mode conditioning strategies are critical. Thermal comfort is achievable: being outdoors, sitting on the shade and having a 1m/s air movement, provides comfort during most of the year.
- Sky and wind conditions change frequently throughout the day, impacting daylighting and shading designs.

Add /A.1 Climate Analysis (Continued)

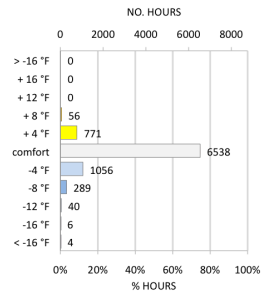
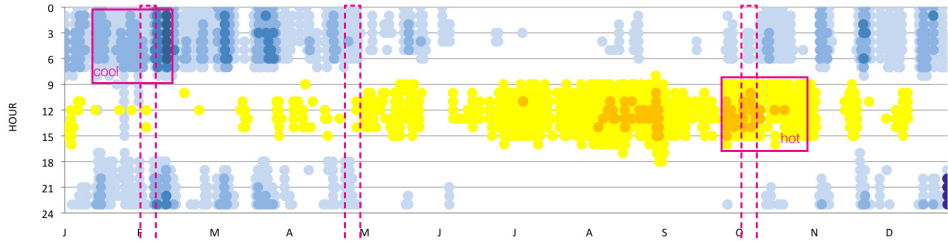
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Add/A.1 Climate Analysis (Continued)

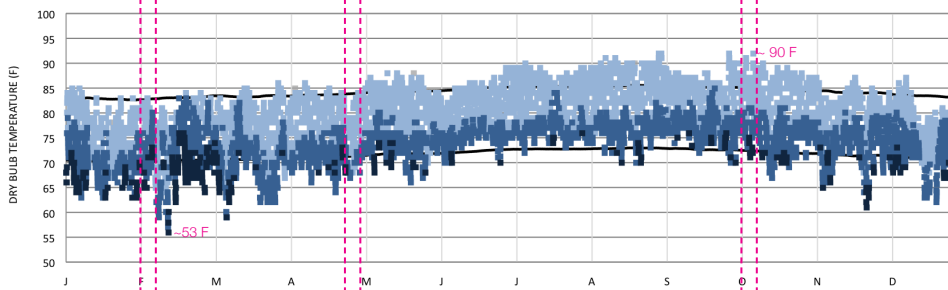
Site Outdoor Air Drybulb Temperature



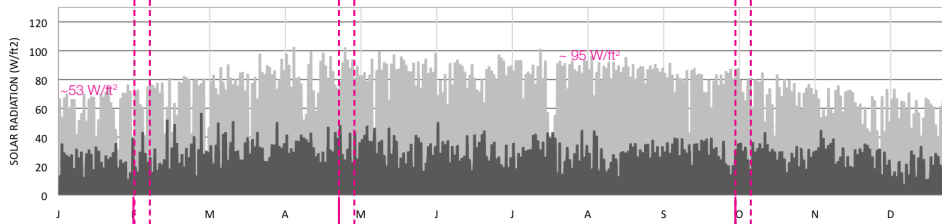
THERMAL COMFORT



DRY BULB TEMPERATURE AND HUMIDITY



SOLAR RADIATION



Add/A CLIMATE AND WEATHER DATA ANALYSIS**2. TMY 3 FROM HONOLULU INTERNATIONAL AIRPORT**

Temperature in Hawaii is closely tied to elevation, distance from the coast and the trade winds. The prevailing wind comes mostly from northeast. Wind direction influence the precipitation and humidity distribution among the islands. Sites on the windward side of the islands can be wet, while places on the leeward side, can be relatively dry. Also, as clouds rise up to higher elevation, they tend to release moisture to the air. Relative humidity tends to be high which can impact occupants comfort and the design of the heating and cooling system.

To read the two first graphs on the left, locate the day of the year along the horizontal axis (January to December) and locate the time of day along the vertical axis (morning at the top and evening at the bottom). In this example here, the color of the point represents the outdoor temperature at that time of day and year.

The first graph shows the outdoor dry bulb temperature.

The second graph was made based on the adaptive comfort model, and it shows that the Honolulu climate is moderate for most of the time. The yellow dots in the thermal comfort graph represent the hot time of the year, and they account for about 10% of the year. The situation is different during the night time, of which the air is cooled down.

The third graph shows again the outdoor dry bulb temperature but highlights the daily temperature swings, which is about 15 degrees F, It also overlays data for relative humidity (color of the dot) which is high at night and low during the daytime.

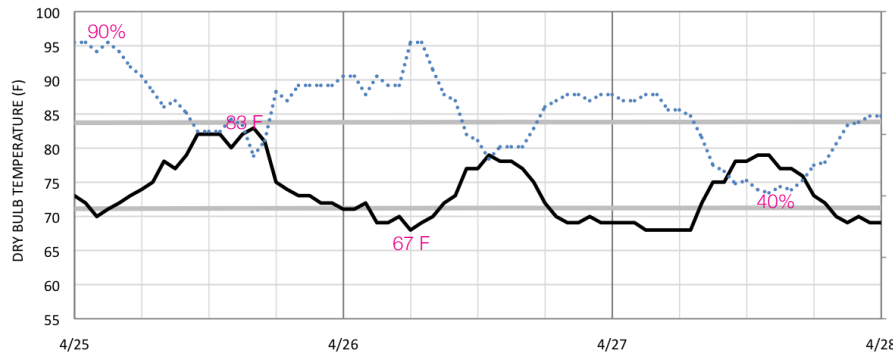
The fourth chart shows the solar radiation throughout the year, where indicates that the direct radiation is dominant.

Three sets of days were picked to represented the typical cool, hot and average days throughout the year.

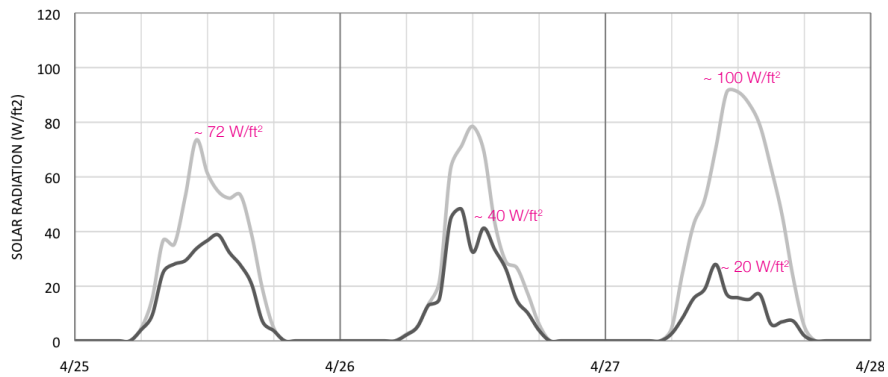
Add/A.2 TMY 3 From Honolulu International Airport (Continued)

Relative humidity and dry bulb temperature move in opposite direction, making hot and relatively dry days and cool and humid nights. Again, because of the higher altitude and distance away from the ocean, the cold days at University of Hawaii is more temperate than that at the airport.

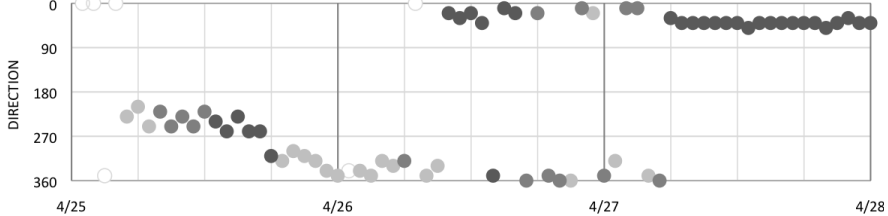
Typical Days



SOLAR RADIATION :: HONOLULU AIRPORT

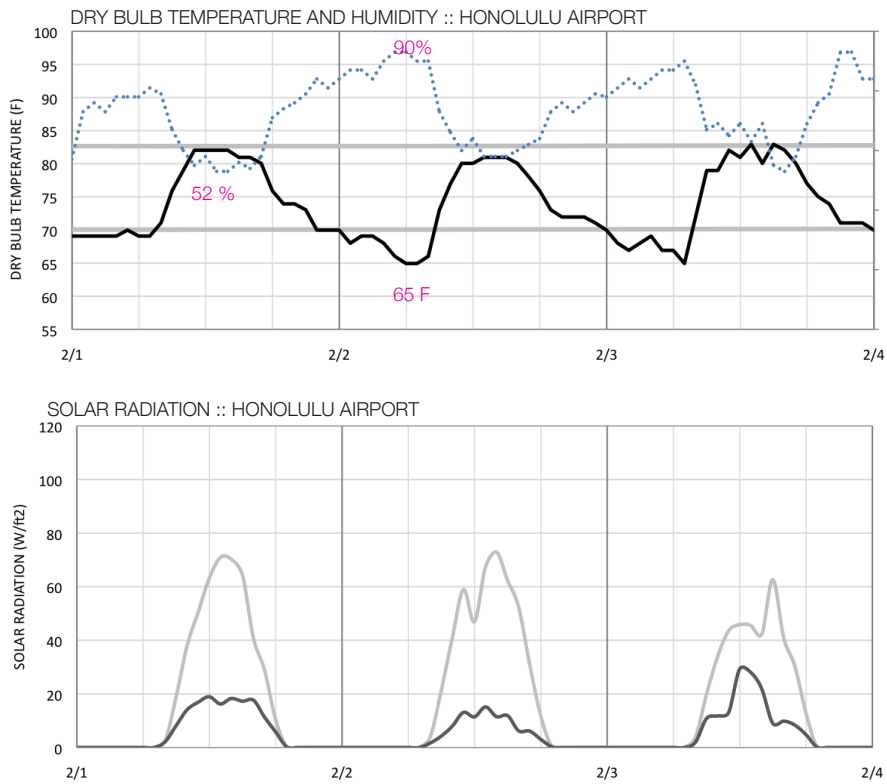


WIND SPEED AND DIRECTION :: HONOLULU AIRPORT

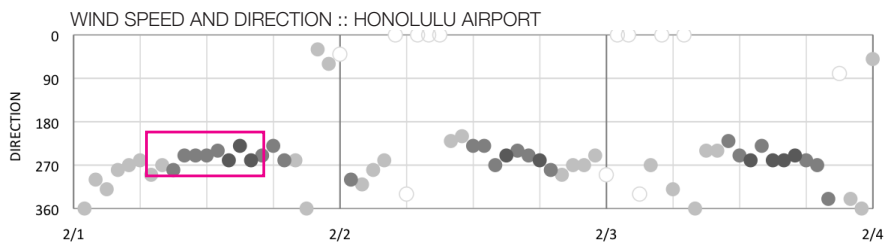


Add/A.2 TMY 3 From Honolulu International Airport (Continued)

Cool Days

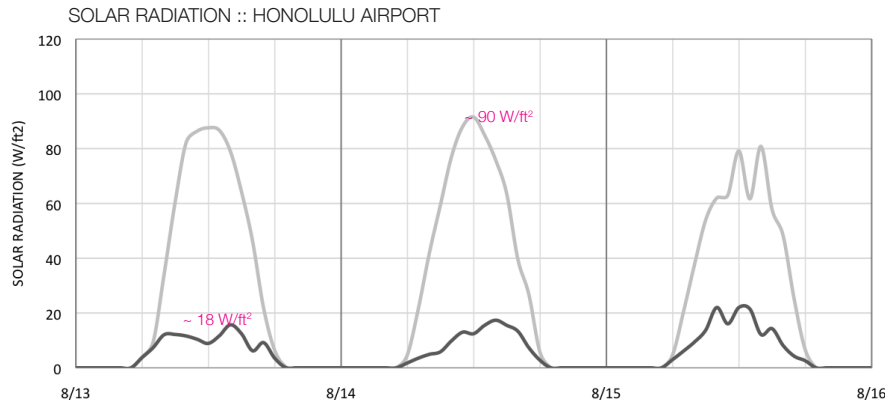
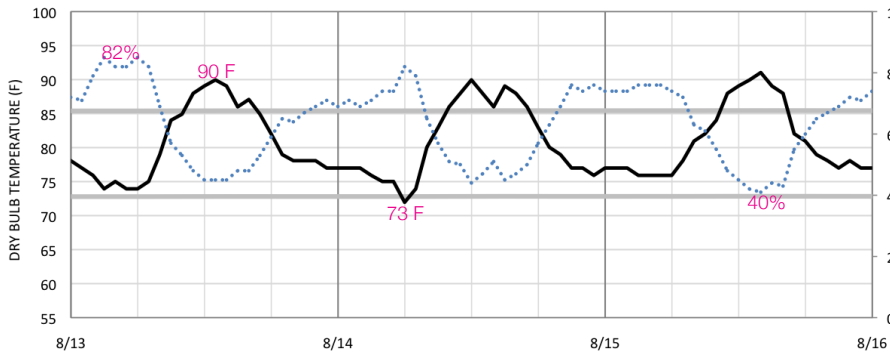


The solar radiation graph indicates that there are more direct solar radiation at the airport and there are more diffusive skies at Kuykendall during the colder days.

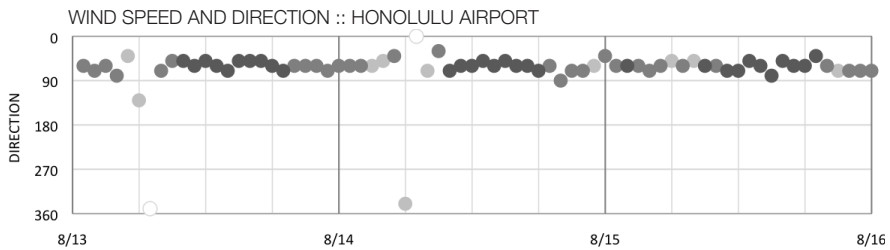


Add/A.2 TMY 3 From Honolulu International Airport (Continued)

Hot Days



The solar radiation pattern is rather consistent at the airport, while at Kuykendall, as the dry bulb temperature rises, the skies become less diffusive than during the colder days.



At the airport, strong southwest wind brings down the relative humidity level, and UHM cooler days happen when the consistence northeast wind is dominant, which induce a more tempered humidity and temperature level.

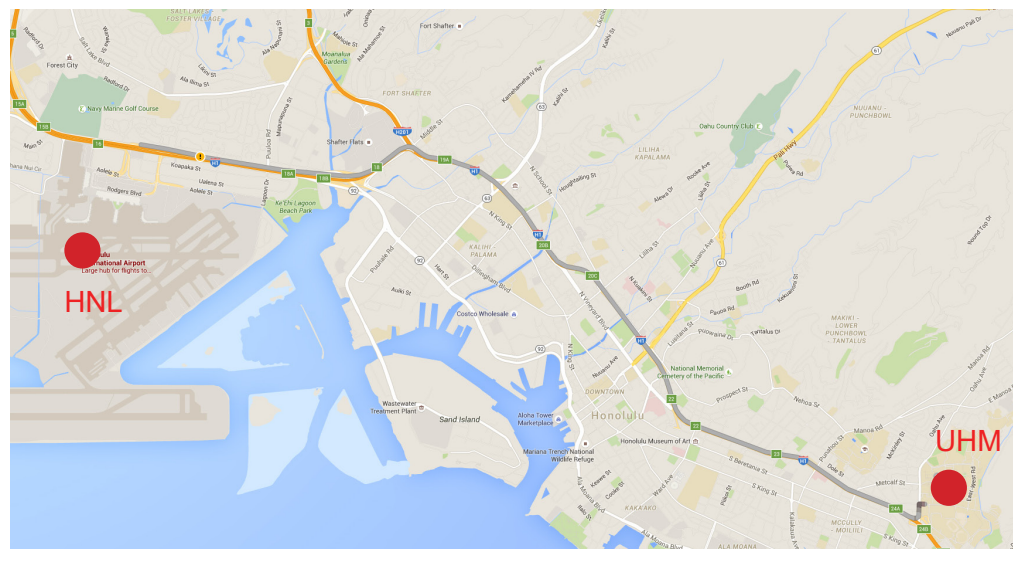
Add/A CLIMATE AND WEATHER DATA ANALYSIS

3. WEATHER DATA FROM UHM CAMPUS

Typical Meteorological Year (TMY) weather data are published and available for Honolulu airport (HNL), which is located about 7 miles to the northwest of the UHM campus. In modeling trying to predict building performance, especially to accurately assume microclimatic differences in wind conditions, this TMY weather file needs to be adjusted to account for differences in weather conditions at HNL compared to the weather conditions on UHM sites.

We were provided with weather data collected from two weather stations located on campus: one station is located at Holmes Hall, and the other is located at Kuykendall Hall. The Holmes Hall data include 31,296 timestamps on a 60 minute interval from September 1, 2011 through December 31, 2015. The Kuykendall Hall weather data include 106,338 timestamps on a 15 minute interval from July 16, 2011 through January 21, 2015. Both data sets include occasional gaps in the data.

Weather from HNL was downloaded from Weather Underground for 2011 through 2015. Data were hourly and included air temperature, wind speed and wind direction among other variables. The analysis in the following pages compares conditions at HNL with simultaneous conditions at UHM. Some comparisons were studied as dependent on wind direction. We present the comparisons below in order for UHM personnel to review the data for quality assurance.



Add/A.3 Weather Data from UHM Campus (Continued)

a. Wind Direction

First we reviewed wind direction variation between HNL and UHM. Due to the turbulent nature of boundary layer wind conditions, we expect wind measurements to vary significantly between each weather station for any particular pair of simultaneous measurements. We compare the full set of simultaneous measurements to see if the general relationship between wind directions at each site exhibits systematic inconsistency.

For Holmes Hall, we note that the wind data appear to be unusable, as wind data show no data points for wind directions between 90° and 270°. For Kuykendall hall, we note generally corresponding wind directions, with a cluster of points showing similar variation of trade wind wind directions between 0° and 90°. We also note clusters where wind directions at Kuykendall of around 30° to 60° for HNL wind directions of around 130°, 220°, and 340°. These clusters indicate inconsistencies between airport and site for which we don't yet have an explanation.

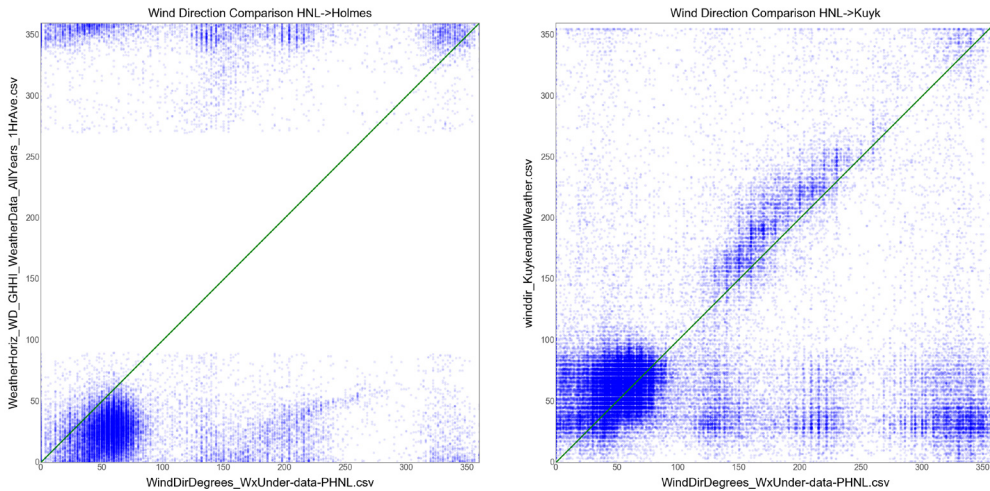


Figure 1. Wind direction relationships for Holmes Hall (left) and Kuykendall Hall (right) vs the HNL airport.

Add/A.3 Weather Data from UHM Campus (Continued)

b. Wind Speed

We reviewed wind speed variation between HNL and UHM. Due to the turbulent nature of boundary layer wind conditions, we expect wind measurements to vary significantly between each weather station for any particular pair of simultaneous measurements. We compare the full set of simultaneous measurements to see if the general relationship between wind speeds at each site exhibits a systematic relationship that can be used for adjustment.

We also anticipate that this relationship may be dependent upon the wind direction, so we examine the relationship by wind direction, in bins of 10°. For each bin, we plotted a scatterplot of simultaneous measurements of wind speed at UHM vs HNL (ie, measurements taken within an hour). We also calculated the line of best fit using OLS regression (see Figure 2 below). Finally, we plotted the frequency of measurements and the wind speed scale factor calculated for Holmes and Kuykendall (See Figure 3 below). The results for Kuykendall Hall show an adjustment factor of around 80%. The results for Holmes are suspect since the scale factor is so low, and because the wind direction variation exhibited erroneous data.

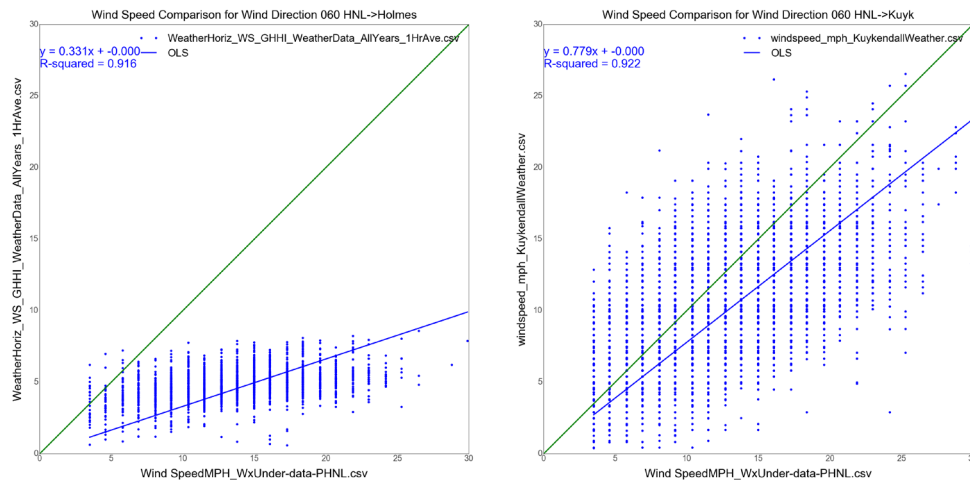


Figure 2. Scatter plots of wind speeds for 60° wind direction bin

Add/A.3 Weather Data from UHM Campus (Continued)

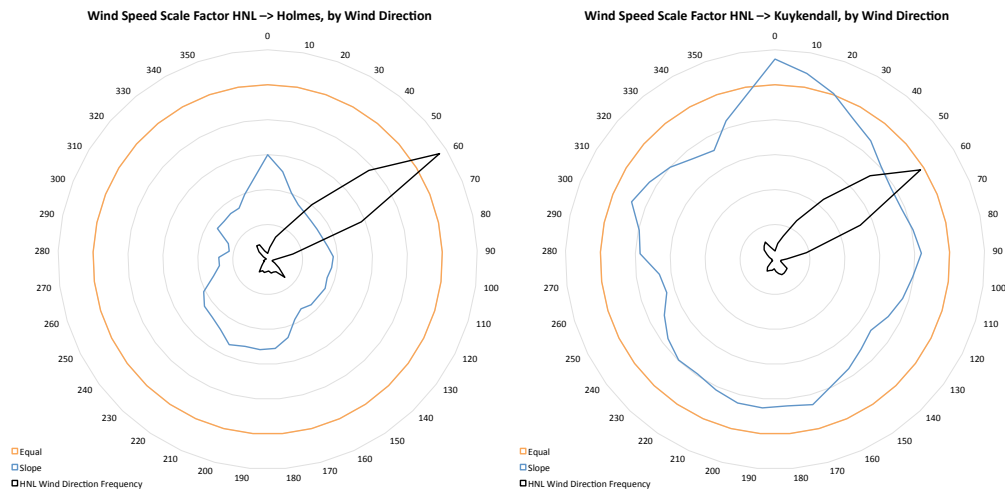


Figure 3. Wind speed adjustment factor and frequency by wind direction

c. Air Temperature

Last, we reviewed air temperature variation between HNL and UHM. As opposed to wind data, we expected to see more consistency between patterns of air temperature at HNL vs UHM. Similarly, we compared the full set of simultaneous measurements to see if the general relationship between wind speeds at each site exhibits a systematic relationship that can be used for adjustment.

We also anticipate that this relationship may be dependent upon the wind direction, so we examine the relationship by wind direction, in bins of 10°. For each bin, we plotted a scatterplot of simultaneous measurements of air temperature at UHM vs HNL (ie, measurements taken within an hour). We also calculated the line of best fit using OLS regression (see Figure 2 below). Finally, we plotted the frequency of measurements and the linear air temperature correction equation calculated for Holmes and Kuykendall (See Figure 4 below). The results for Kuykendall Hall show a lower slope than the relationship for Holmes. We also plot the predicted temperatures on campus HNL temperatures of 74°F and 81°F for Holmes Hall and Kuykendall Hall by wind direction.

Add/A.3 Weather Data from UHM Campus (Continued)

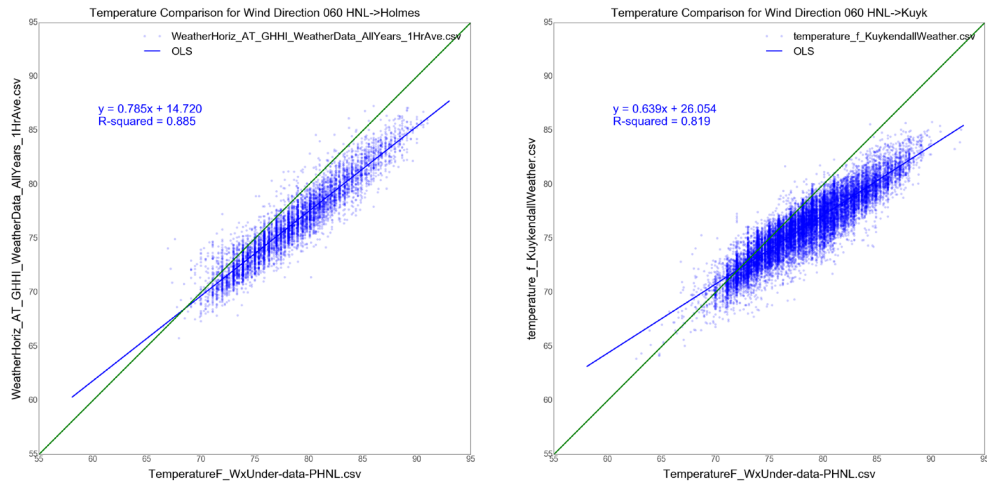


Figure 4. Scatter plots of air temperatures for 60° wind direction bin

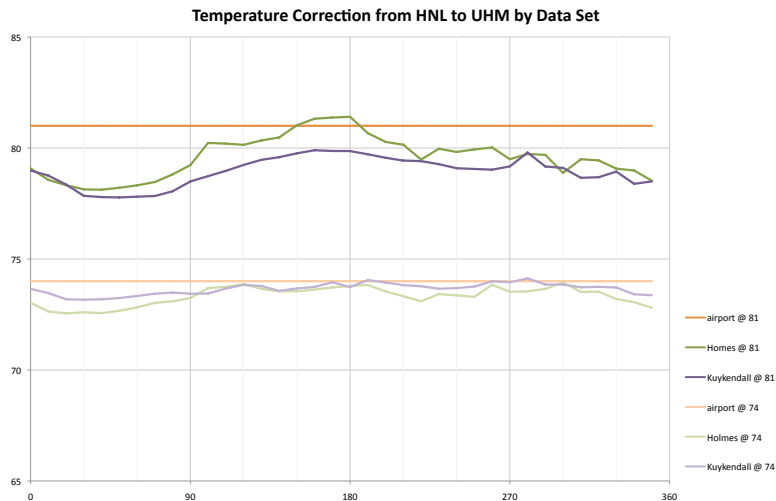


Figure 5. Air temperature adjustment factor by wind direction, showing more variation for the temperatures predicted by Holmes Hall data.

Note that during trade winds, the temperatures on site are generally lower than at the airport, especially for warmer weather. On the other hand, air temperatures are more similar between HNL and UHM for wind directions from the south.

Using the Holmes hall data, the adjusted UHM campus temperature variation will be greater than the adjustment derived from the Kuykendall data. We will average the correction equations for these two UHM datasets, unless we are provided reasons for relying upon one dataset more than another.

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Add/B. DAYLIGHTING AND SHADING STUDIES

1. EXECUTIVE SUMMARY

The first round of daylighting studies focused on optimizing solar control. The performance of different exterior shading strategies was evaluated in terms of the amount of useful daylight (percentage of the space that achieve between 30 and 300 FC with fractional credit for values below 30 FC) inside the space for each orientation. The Profile Angle is the angle between a vector normal to the window and the rays of the sun, measured perpendicular to the window plane.

Fixed, single overhang solutions were compared to other shading strategies such as fixed louvers, tilting louvers or automated louvers.

- For south facades, fixed or tilting louvers perform the best (fixed louvers outperform the single overhang as they produce a redirecting effect). The horizontal overhang is better at preventing excessive lighting near the window, but has less penetration in deeper spaces. Recommended Profile Angle is between 45 and 65 degrees.
- For east facades, fully automated louvers outperform all other options. Fixed strategies are less effective near the window because of low sun angles. Recommended Profile Angle is between 45 and 65 degrees.
- For west facades, fully automated louvers outperform all other options. Fixed strategies are less effective near the window because of low sun angles. Recommended Profile Angle is between 45 and 65 degrees.
- For north facades, a small horizontal overhang performs best. Larger overhangs only marginally reduce sun penetration at the expense of daylight deeper in the space. Recommended Profile Angle is 65 degrees.

This Addendum also includes a series of graphs showing actual hourly data over the whole year for:

- Horizontal overhang effectiveness (percentage of the window that is shaded) for different overhang depths for each orientation.
- Automated louver protocols: Schedules based on sun penetration for different orientations of operable louvers. Tilt only simulates with 5 positions, retractable has an Additional 6th position (fully open),
- Hourly Useful Daylight Performance (percentage of the space that achieve between 30 and 300 FC with fractional credit for values below 30 FC)
- Hourly excessive illuminance (percentage of the space that exceeds 300 FC.)

Add/B.1 Executive Summary (Continued)

The next round of daylighting studies analyzed visual comfort in the Hawaiian climate and how to prevent glare from direct views to the horizon and low altitude sky.

The sky conditions in Hawaii pose some unique challenges to meeting these demands. The latitude and local climate conditions lead to periods of very bright skies (even at the horizon) mixed with rapidly changing and sometimes quite dark skies. In order to maintain visual comfort inside the building the window wall needs a response that reduces the brightness of the view to the sky, but still allows enough daylight during darker sky conditions.

In cases where the view to the sky is obstructed by vegetation, topography and surrounding buildings (except those with large high reflectance surfaces that receive direct sun), a fixed horizontal overhang or fixed louvers that effectively block direct sun on the window works alone to create a visually comfortable interior.

In all other cases where there is a direct view to the horizon and low altitude sky some dynamic response is necessary. Two Preferred options:

- Option 1:: Automated Interior fabric roller shades. This is a compliment to fixed exterior overhangs that meet the profile angle requirements for the orientation. Fabric on East and West facades where a direct view out the window is unavoidable for people seated at desks should have an openness of 1% and a visible light transmittance > 5%. North and South facades, as well as East and West facades where desks are arranged facing perpendicular to the window should have an openness of 3% and visible light transmittance > 10%.
- Option 2:: Automated exterior louvers. Louvers should be light in color and matte rather than specular or glossy. They should be capable of adjusting the profile angle for light penetration between 10 (mostly closed) and 45 degrees (1:1 ratio between louver spacing and louver depth).

This Addendum also includes a series of graphs showing actual hourly data over the whole year for Automated shade protocols by orientation (when the shades would be deployed), human response renderings, falsecolor luminance maps (shows the rendered view on a color scale to communicate surface brightness) and image contour maps (contour map shows changes in elevation, these show changes in illuminance levels throughout the space, showing illuminance levels in footcandles).

Add/B DAYLIGHTING AND SHADING STUDIES**2. MODEL ASSUMPTIONS**

We modeled and ran simulations using Radiance, a research grade lighting simulation tool developed by Lawrence Berkeley Laboratory that is based on the physics of light and material properties.

Geometry is based on existing classrooms in Kuykendall Hall. Window size was optimized to maximize daylight (50% window to wall ratio). The space is assumed to be located on the third floor, surrounded by medium density 3-4 story buildings and landscape.

Geometry: Sill 3.66' high
 Head 10.5' high
 Ceiling: 13' high
 Depth of room: 28'

Materials and finishes are based on assumptions that match the UHM Building Design and Performance Standards.

Visual Light Reflectances (VLR):

Floor 20%
Walls 50%
Ceiling 80%
Shades 14% VLT
Glazing 64% VLT
Site 15%
Trees 8%
Overhang 50%

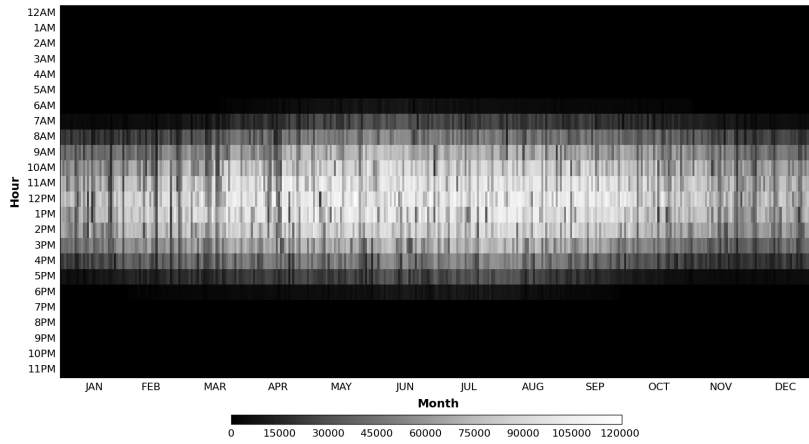
Sky and Climate Data: Weather data is the TMY2 dataset from the Honolulu airport, The TMY3 dataset appears to have hourly values for some columns shifted in certain months, so does not appear to be reliable. The final analysis should be repeated with the UHM weather data if it is substantially different.

Clear sky data is generated using stats from the TMY3 dataset and is in good agreement with the TMY2 direct normal values.

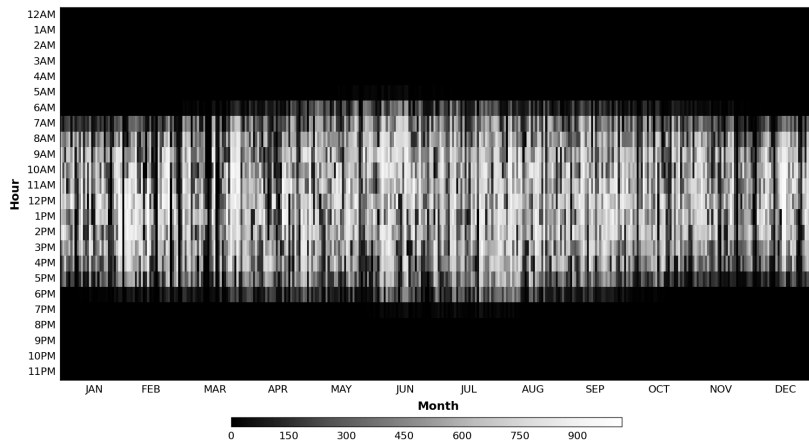
VLR - visible light reflectance, VLT - visible light transmittance

Add/B.2 Model Assumptions (Continued)

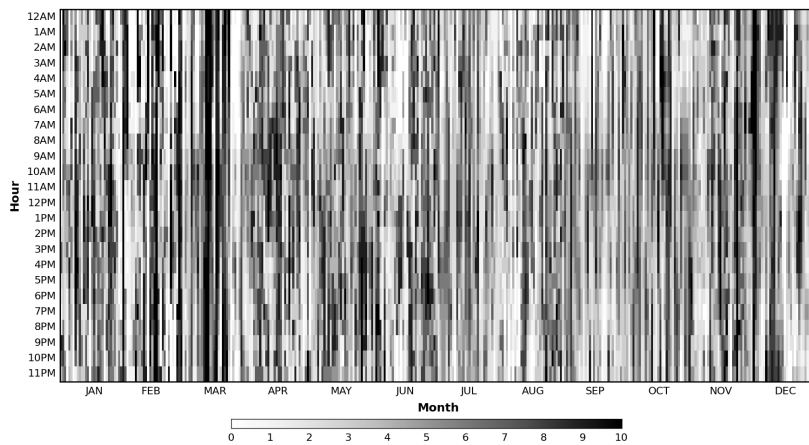
Global Horizontal Illuminance



Direct Normal Radiation

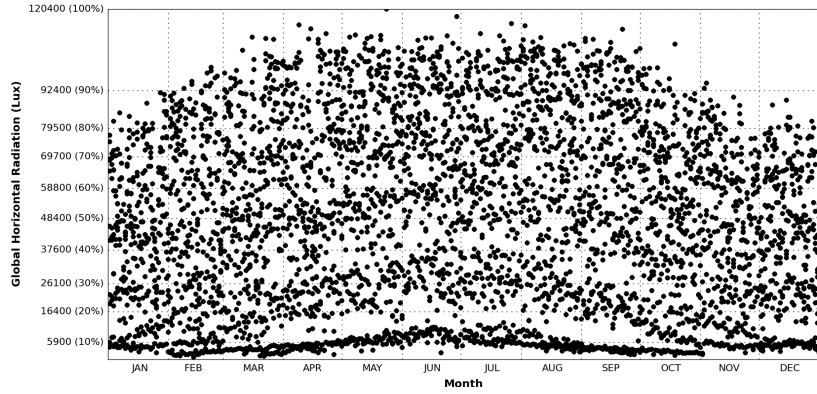


Sky Cover

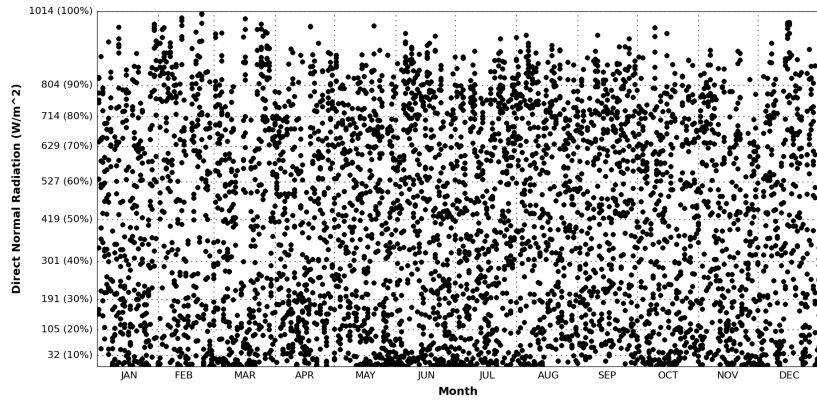


Add/B.2 Model Assumptions (Continued)

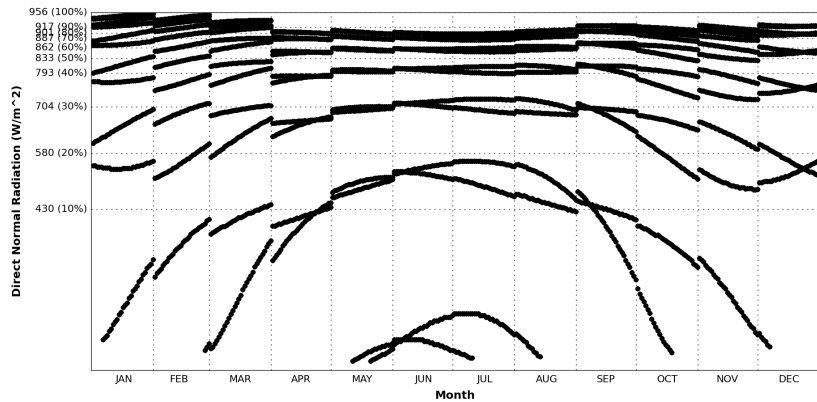
Global Horizontal Illuminance



Direct Normal Radiation



Clear sky Direct Normal Radiation



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Add/B DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

3.1/ SUMMARY OF RESULTS.....19

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3.5/ HOURLY EXCESSIVE ILLUMINANCE.....49

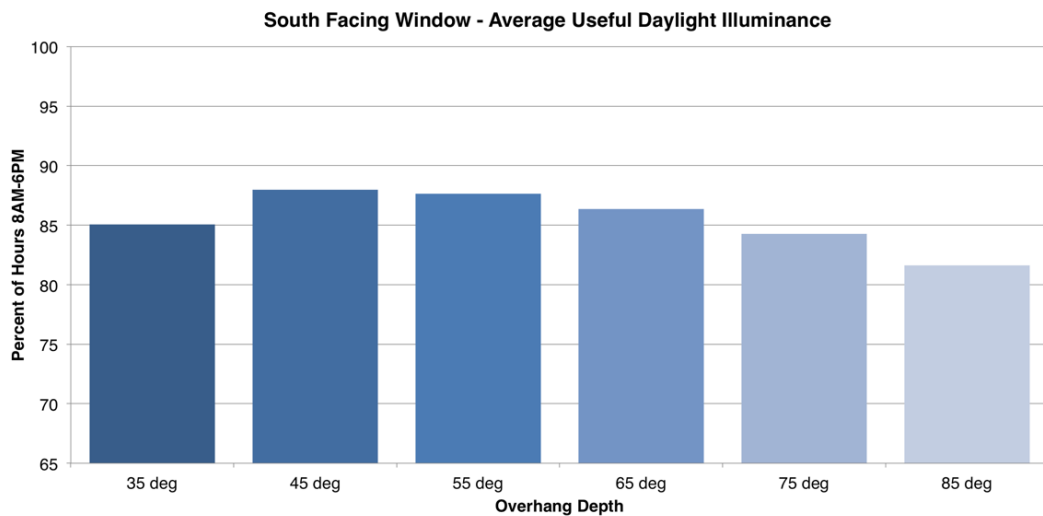
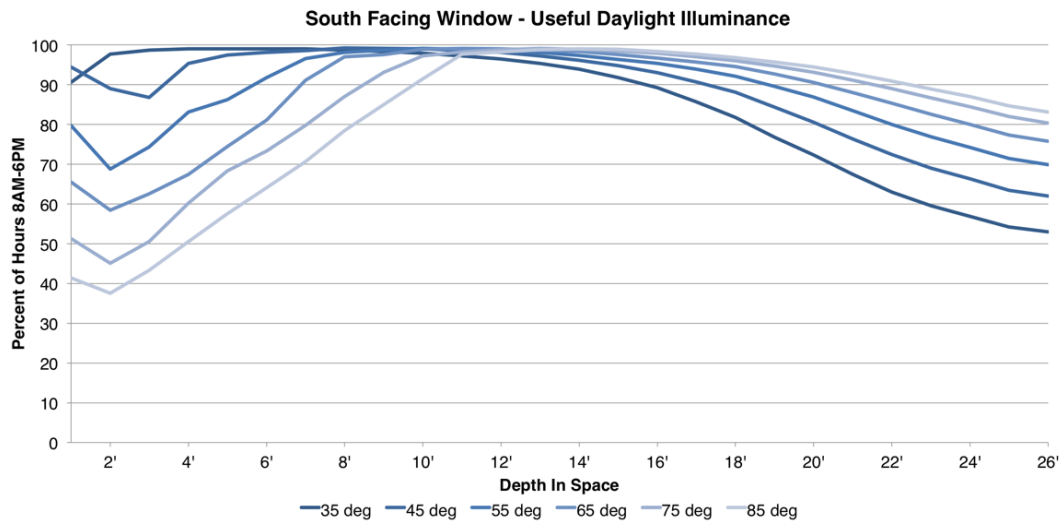
B. DAYLIGHTING AND SHADING

Add/B. DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

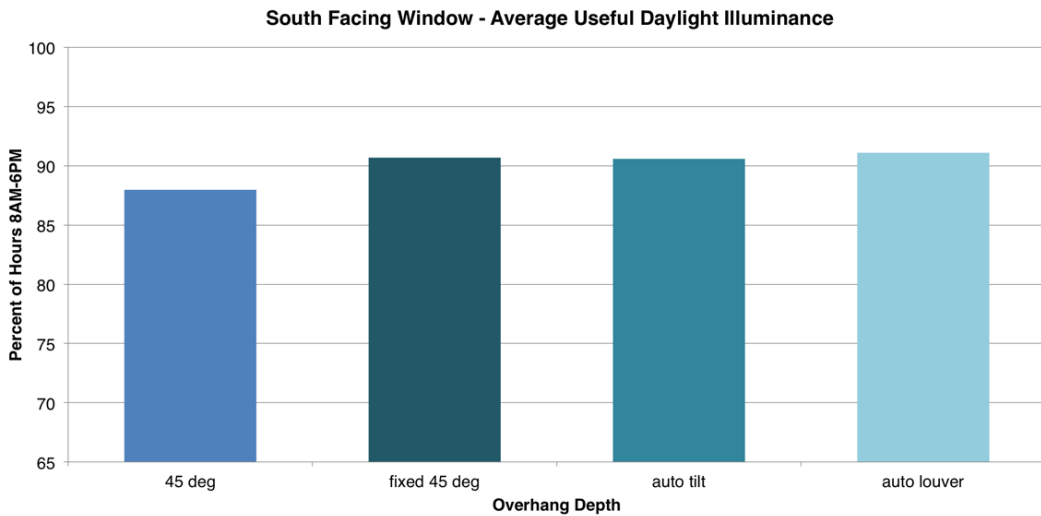
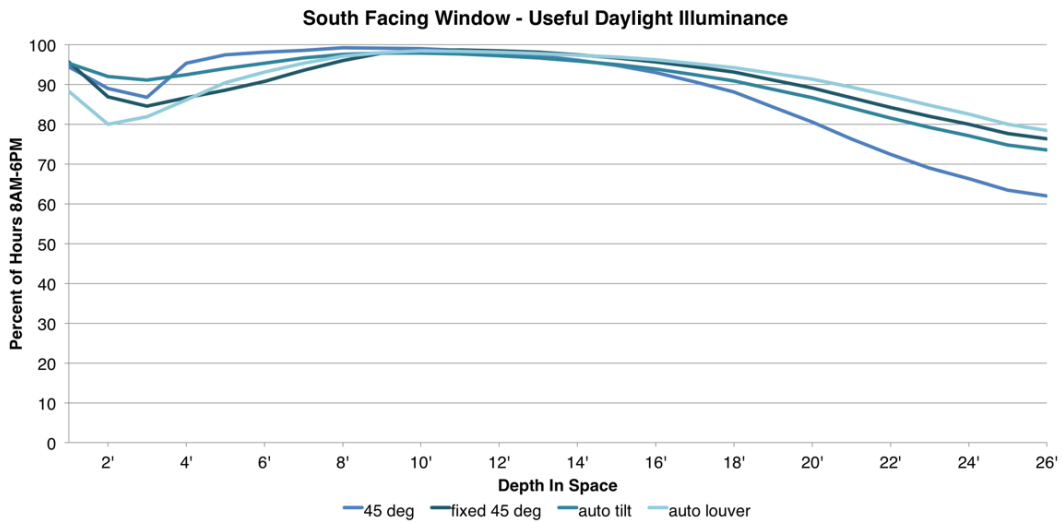
3.1. SUMMARY OF RESULTS

3.1.1 South Facing



Graphs show the percentage of hours a point receives between 30 and 300 footcandles, with fractional credit for values below 30FC. Graphs on this page show average and point by point performance across the room of different horizontal overhang depths. Graphs on the next page show average and point by point performance for the optimal horizontal overhang compared with smaller fixed louvers, tilting louvers and retractable tilting louvers.

Add/B. 3.1.1 Summary of Results:: South Facing (Continued)



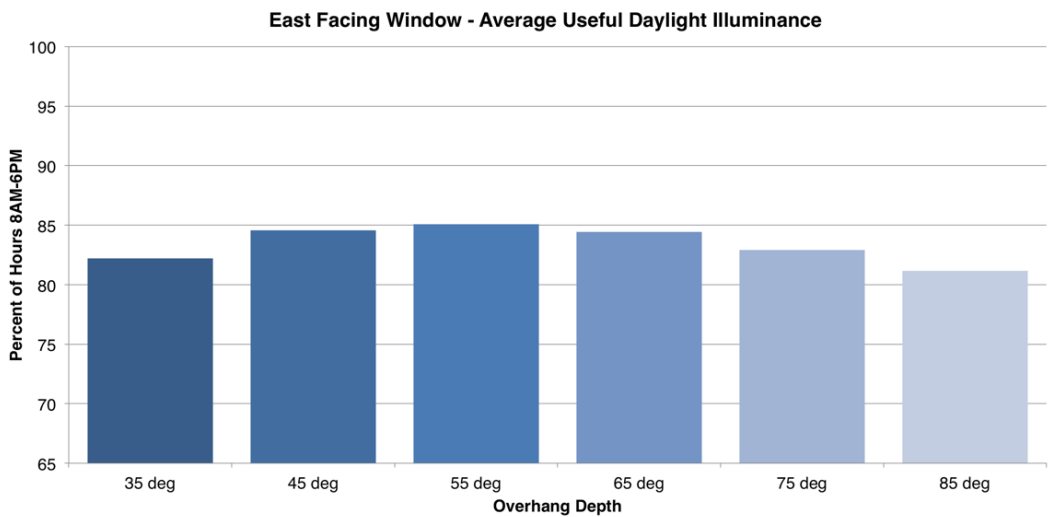
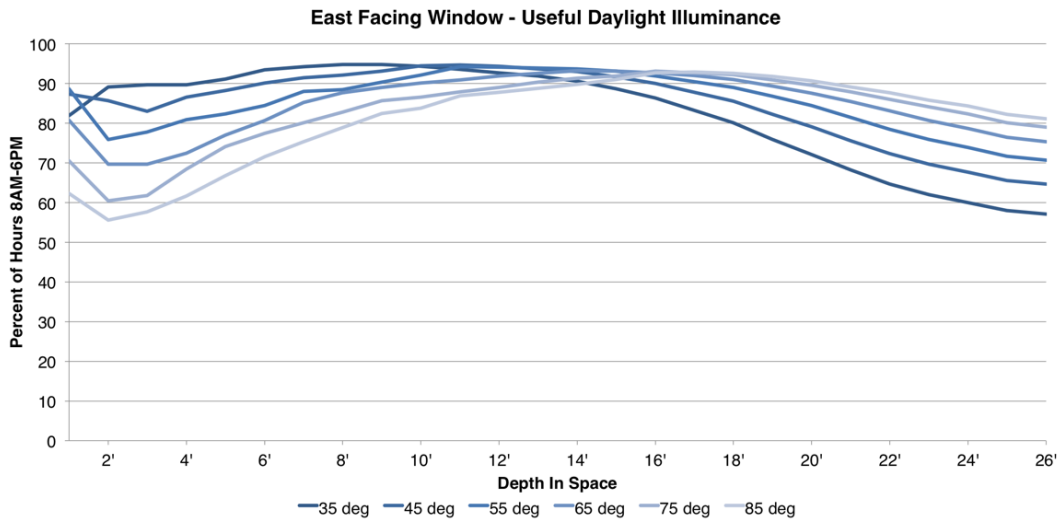
For south facades, fixed or tilting louvers perform the best (fixed louvers outperform the single overhang as they produce a redirecting effect). The horizontal overhang is better at preventing excessive lighting near the window, but has less penetration in deeper spaces.

Add/B. DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

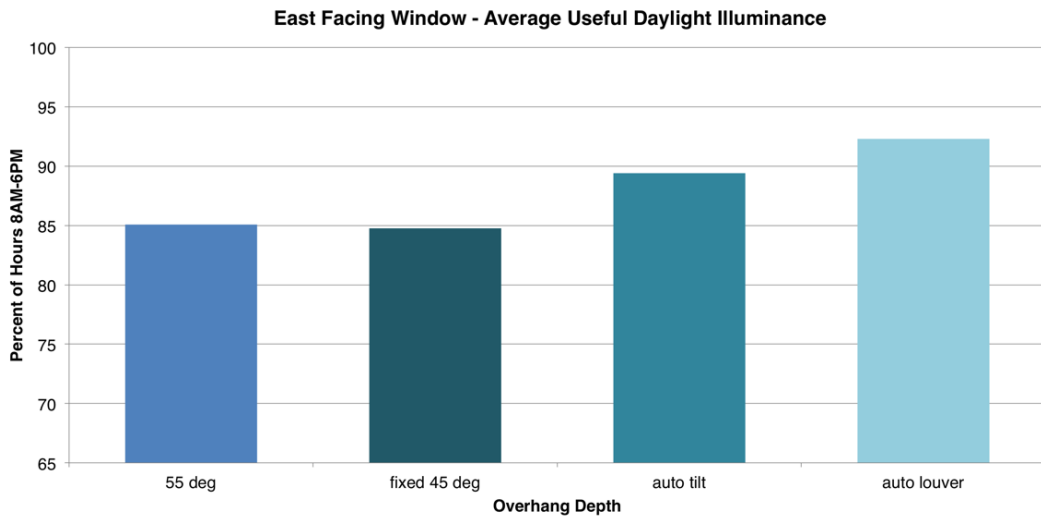
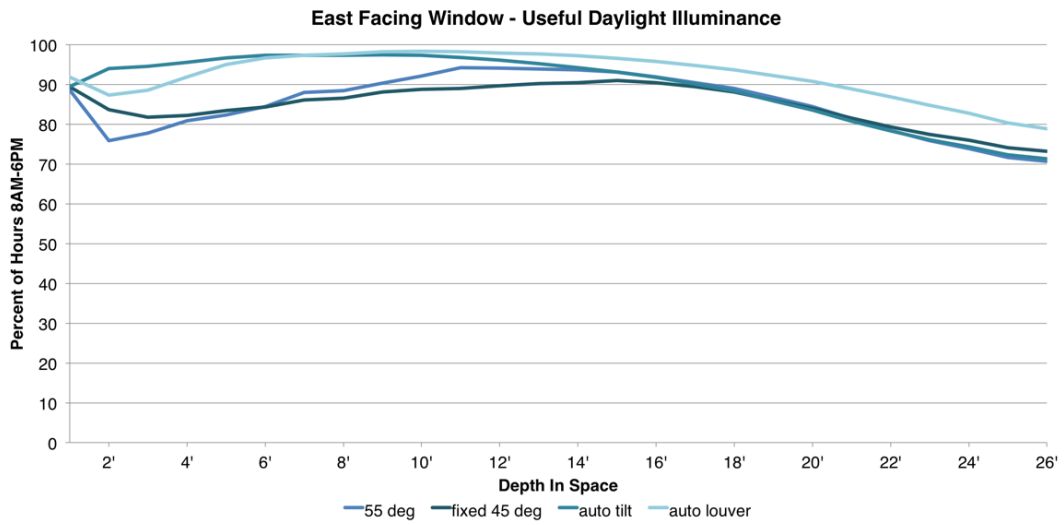
3.1. SUMMARY OF RESULTS

3.1.2 East Facing



Graphs show the percentage of hours a point receives between 30 and 300 footcandles, with fractional credit for values below 30FC. Graphs on this page show average and point by point performance across the room of different horizontal overhang depths. Graphs on the next page show average and point by point performance for the optimal horizontal overhang compared with smaller fixed louvers, tilting louvers and retractable tilting louvers.

Add/B. 3.1.2 Summary of Results:: East Facing (Continued)



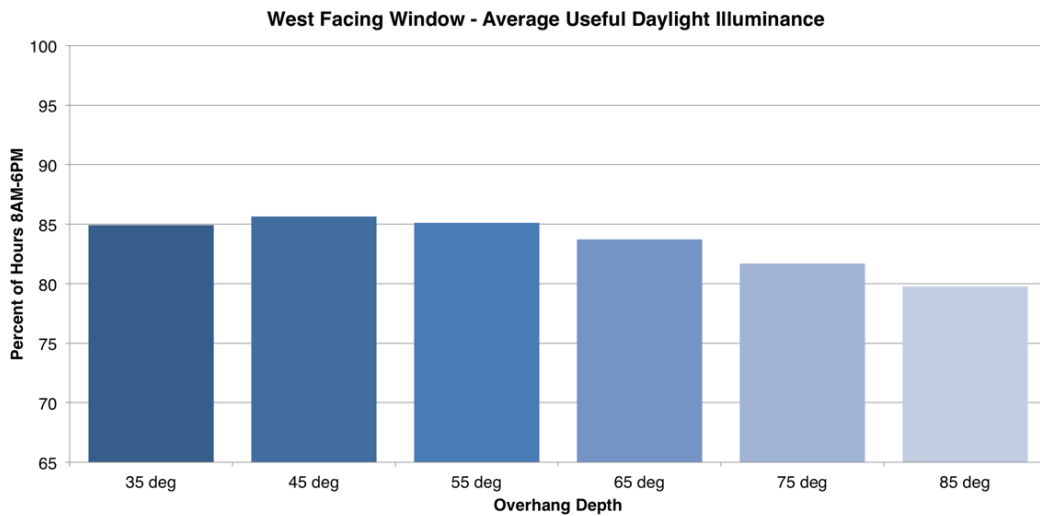
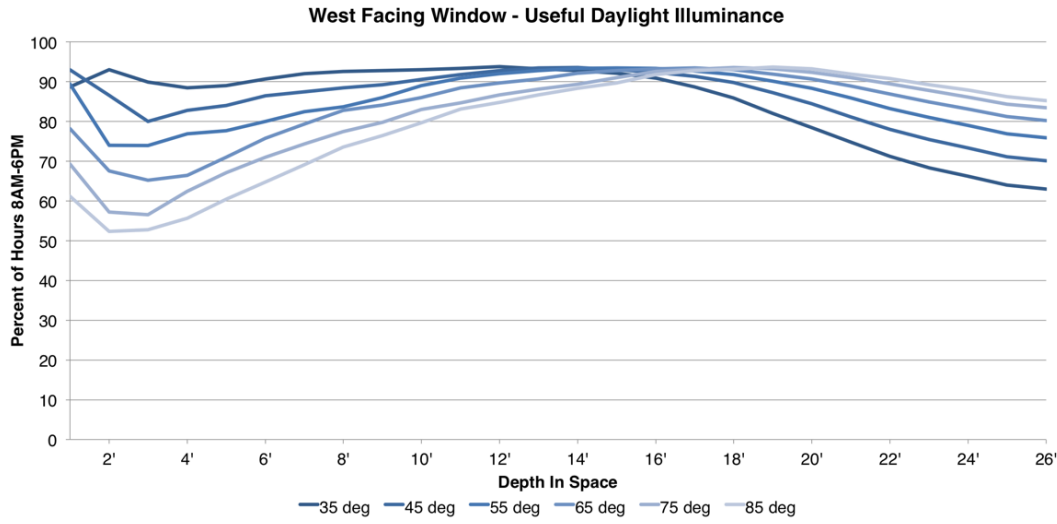
For east facades, fully automated louvers outperform all other options. Fixed strategies are less effective near the window because of low sun angles.

Add/B. DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

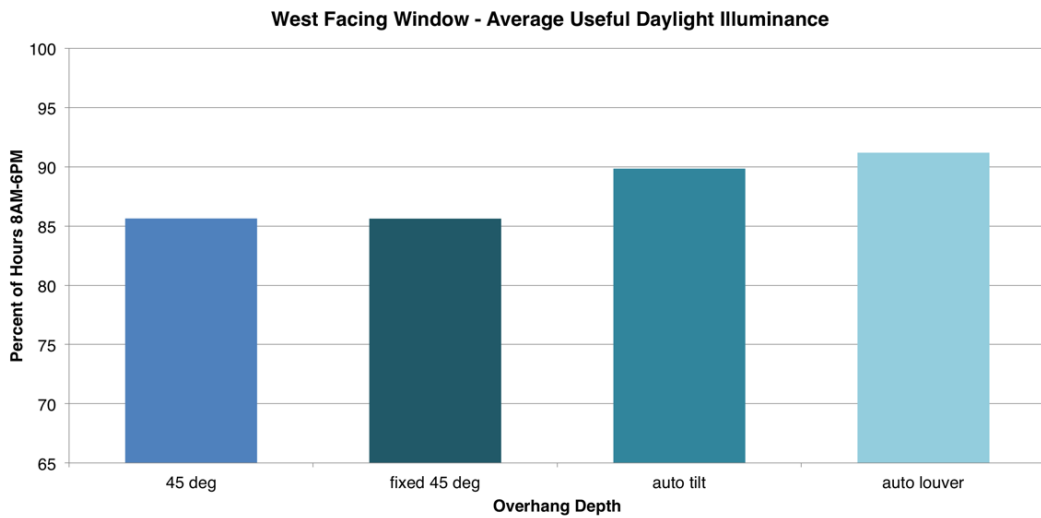
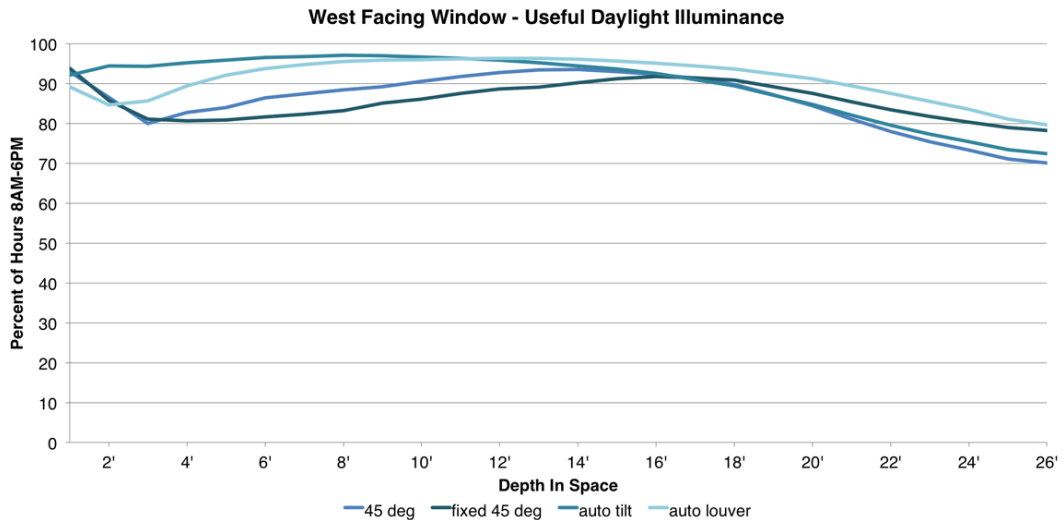
3.1. SUMMARY OF RESULTS

3.1.3 West Facing



Graphs show the percentage of hours a point receives between 30 and 300 footcandles, with fractional credit for values below 30FC. Graphs on this page show average and point by point performance across the room of different horizontal overhang depths. Graphs on the next page show average and point by point performance for the optimal horizontal overhang compared with smaller fixed louvers, tilting louvers and retractable tilting louvers.

Add/B. 3.1.3 Summary of Results:: West Facing (Continued)



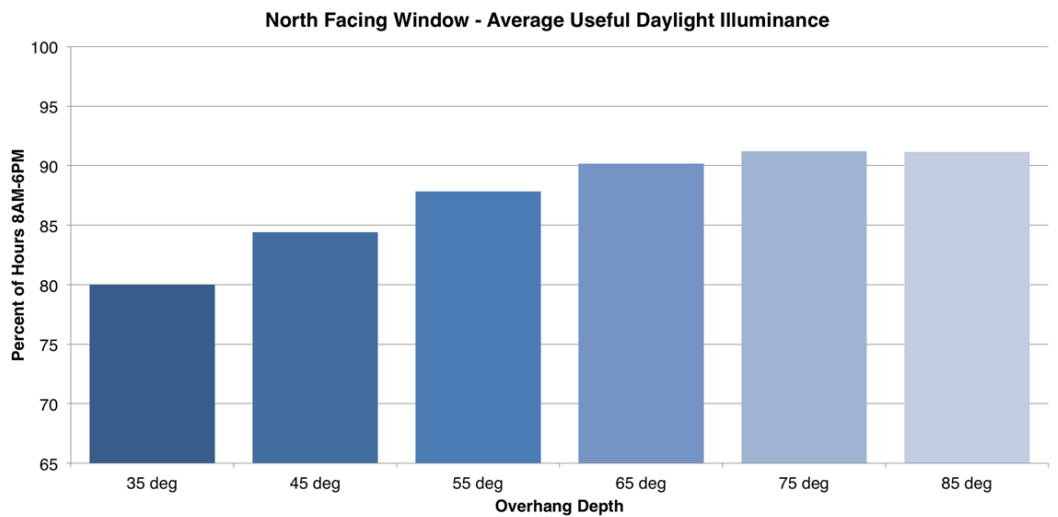
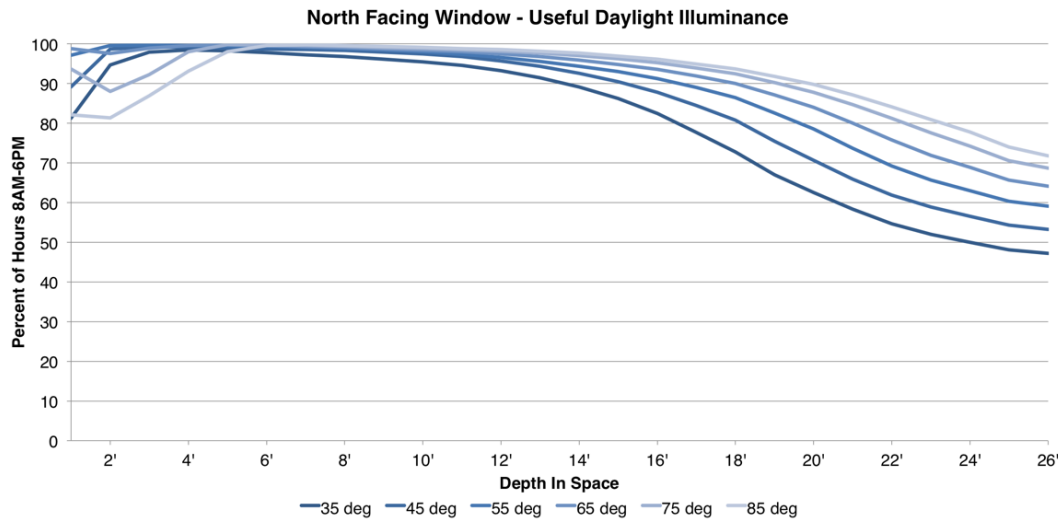
For west facades, fully automated louvers outperform all other options. Fixed strategies are less effective near the window because of low sun angles.

Add/B. DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

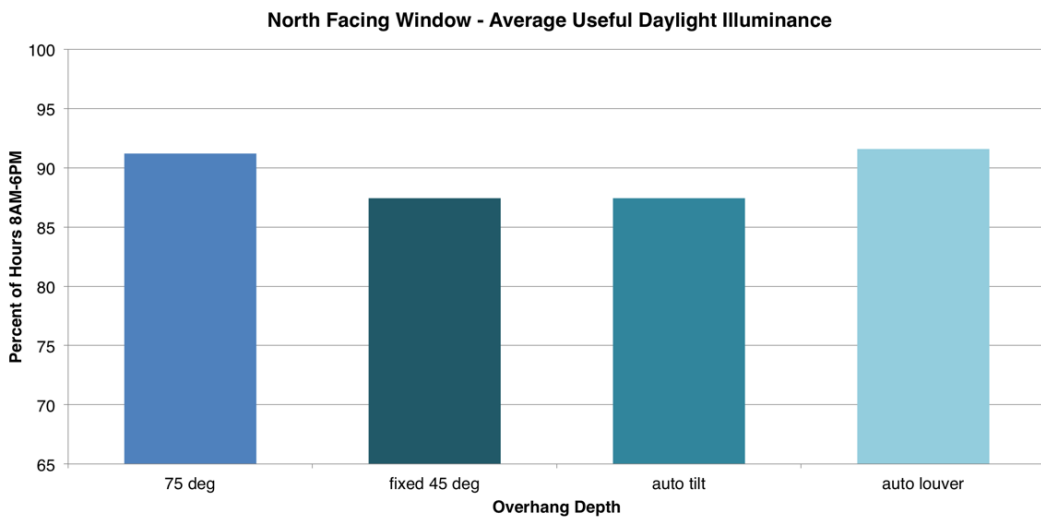
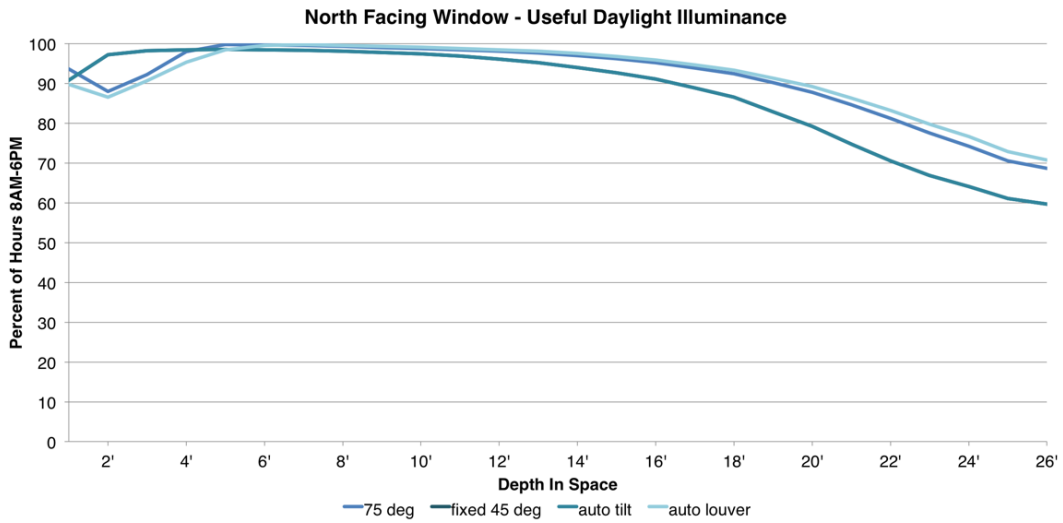
3.1. SUMMARY OF RESULTS

3.1.4 North Facing



Graphs show the percentage of hours a point receives between 30 and 300 footcandles, with fractional credit for values below 30FC. Graphs on this page show average and point by point performance across the room of different horizontal overhang depths. Graphs on the next page show average and point by point performance for the optimal horizontal overhang compared with smaller fixed louvers, tilting louvers and retractable tilting louvers.

Add/B. 3.1.4 Summary of Results:: North Facing (Continued)



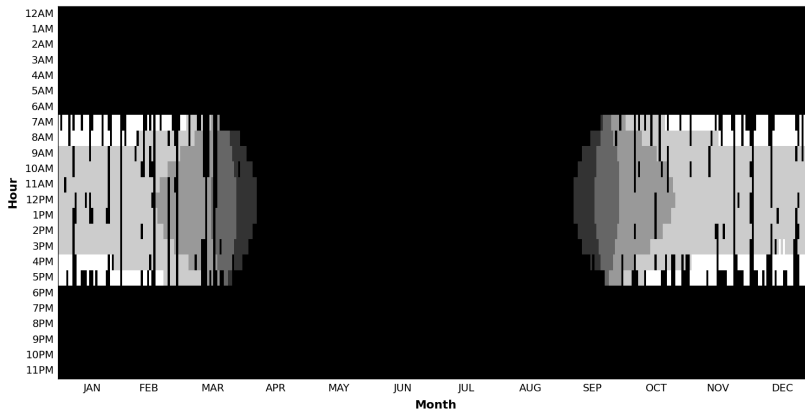
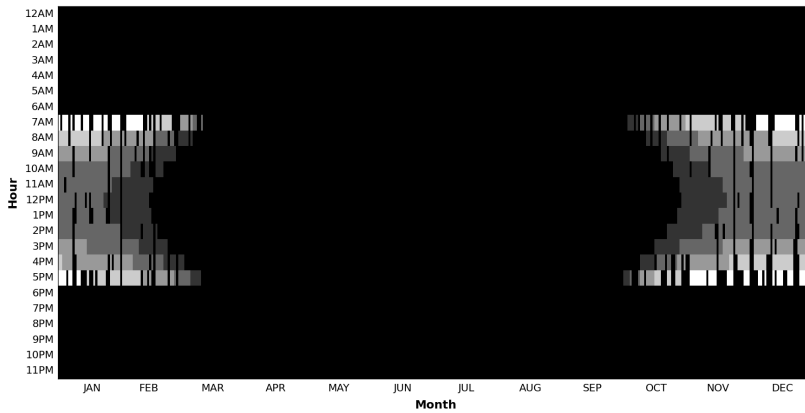
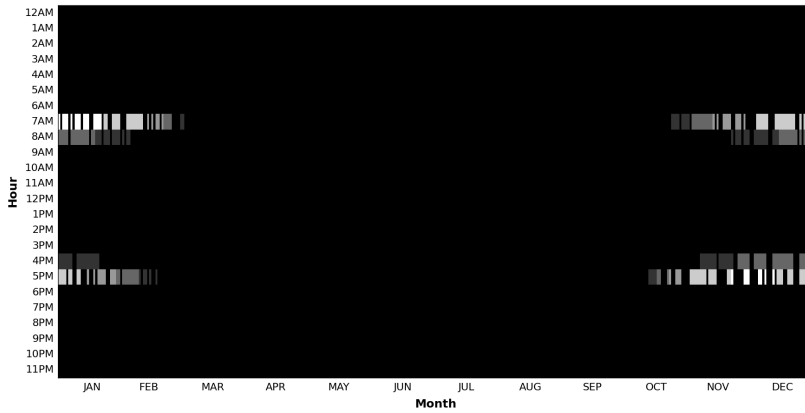
For north facades, a small horizontal overhang performs best. Larger overhangs only marginally reduce sun penetration at the expense of daylight deeper in the space.

Add/B. DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

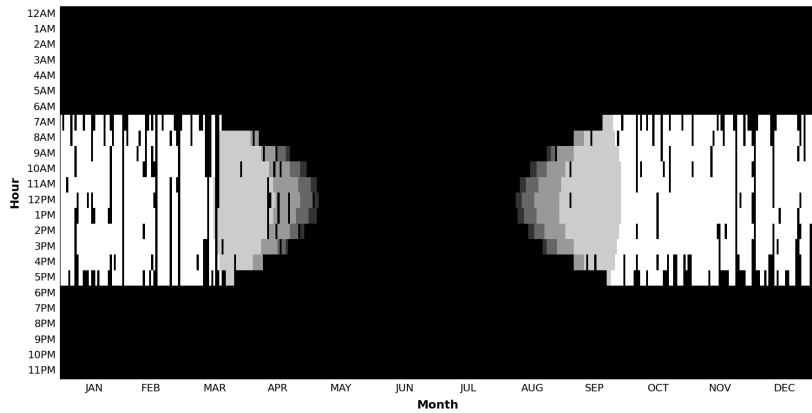
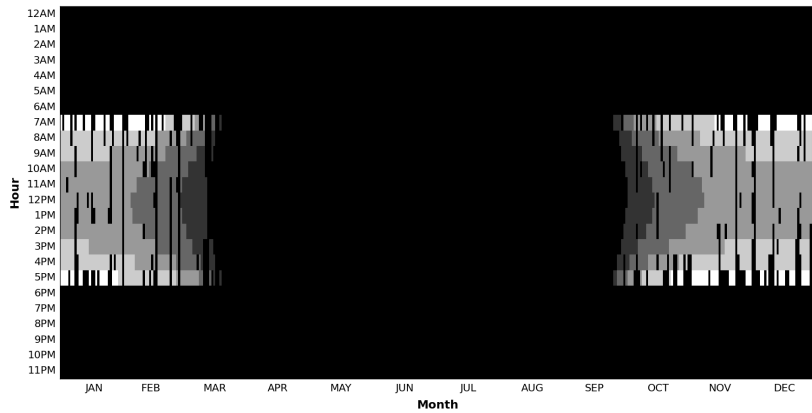
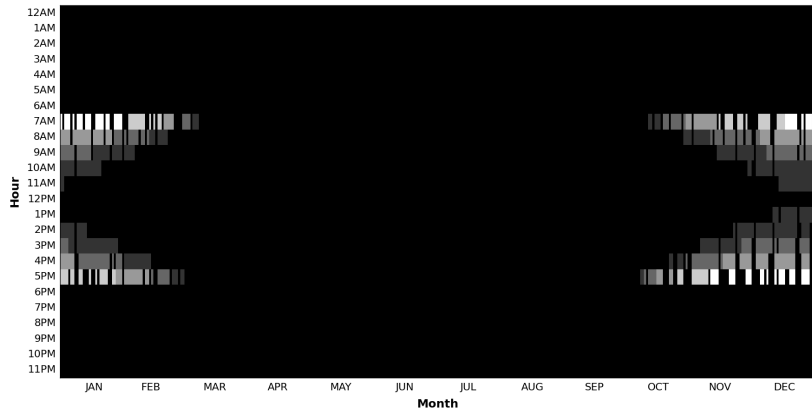
3.2. HORIZONTAL OVERHANG EFFECTIVENESS

3.2.1 South Facade



Add/B. 3.2.1 Horizontal Overhang Effectiveness:: South Facade(Continued)

Hourly graphs below show the percentage of the window that is shaded for various depths of horizontal overhangs.

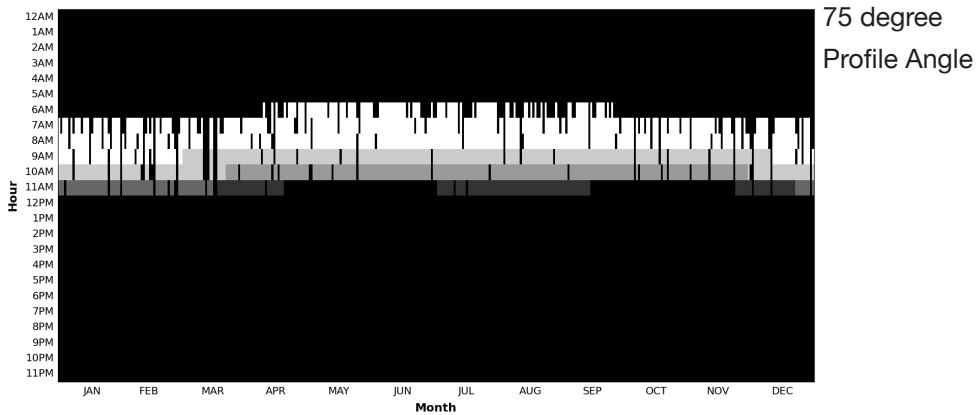
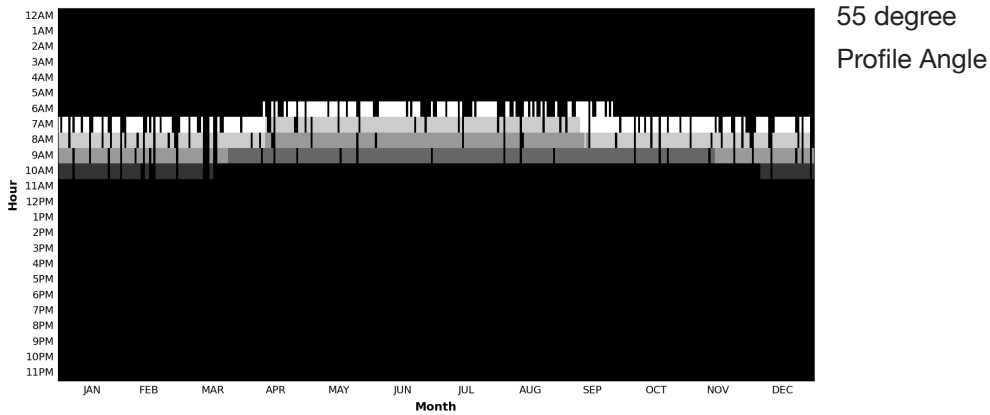
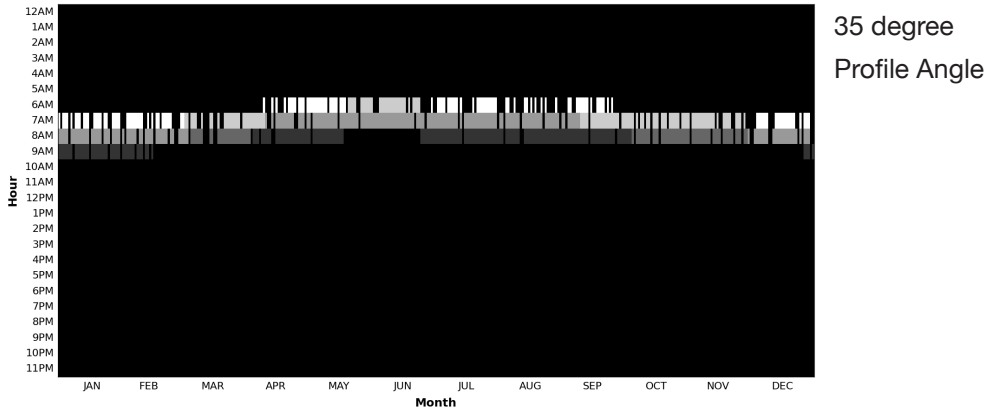


Add/B. DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

3.2. HORIZONTAL OVERHANG EFFECTIVENESS

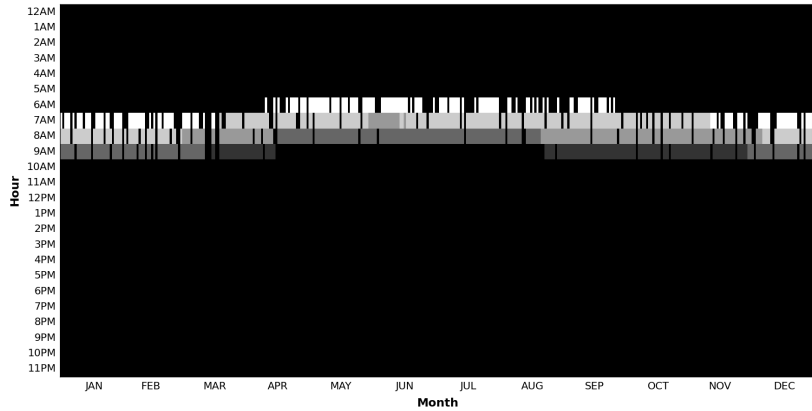
3.2.2 East Facade



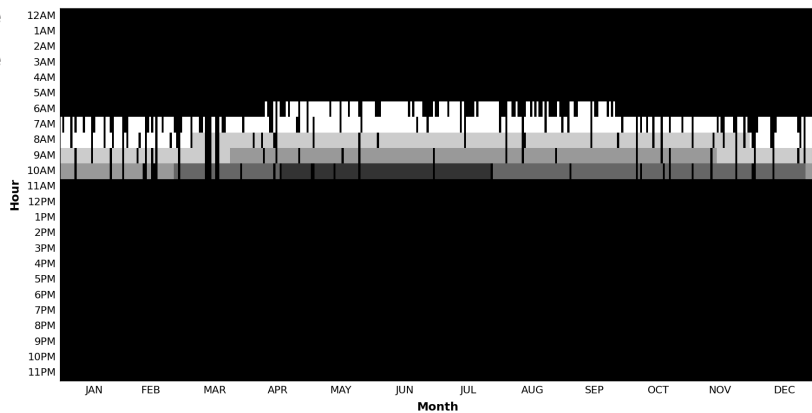
Add/B. 3.2.2 Horizontal Overhang Effectiveness:: East Facade(Continued)

Hourly graphs below show the percentage of the window that is shaded for various depths of horizontal overhangs.

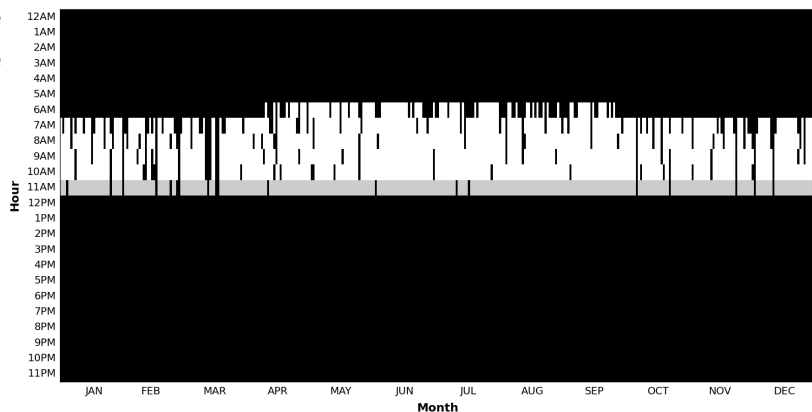
45 degree
Profile Angle



65 degree
Profile Angle



85 degree
Profile Angle

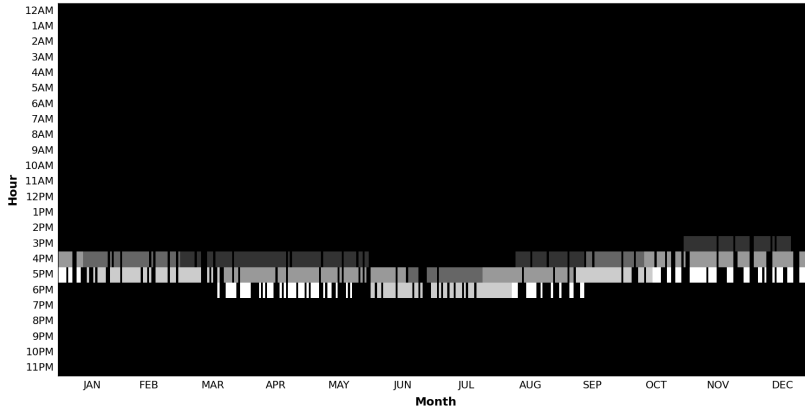


Add/B. DAYLIGHTING AND SHADING STUDIES

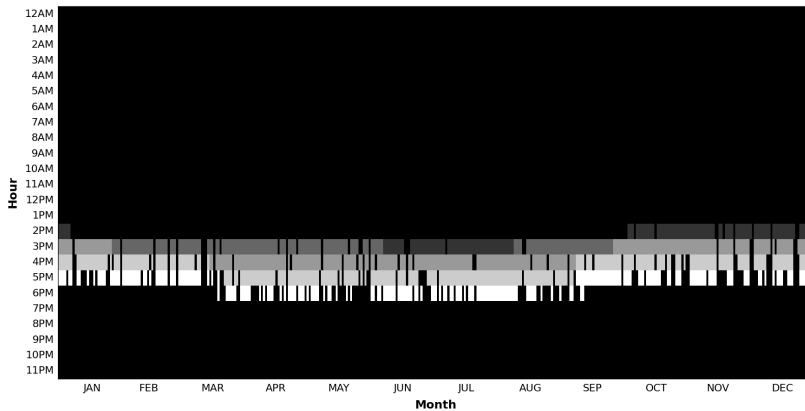
3. OPTIMIZING SOLAR CONTROL

3.2. HORIZONTAL OVERHANG EFFECTIVENESS

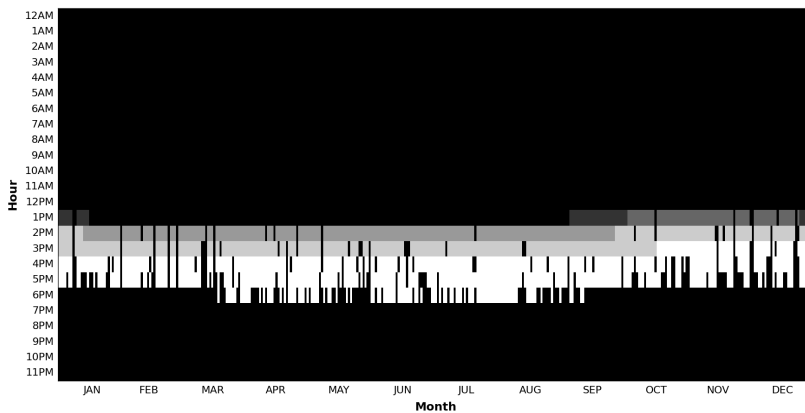
3.2.3 West Facade



35 degree
Profile Angle



55 degree
Profile Angle



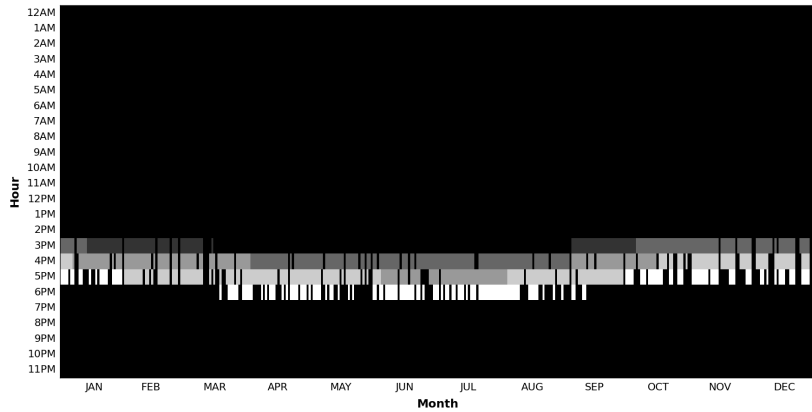
75 degree
Profile Angle



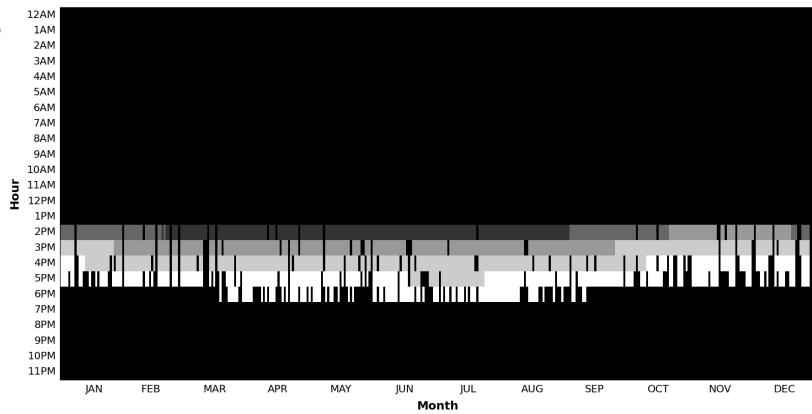
Add/B. 3.2.3 Horizontal Overhang Effectiveness:: West Facade(Continued)

Hourly graphs below show the percentage of the window that is shaded for various depths of horizontal overhangs.

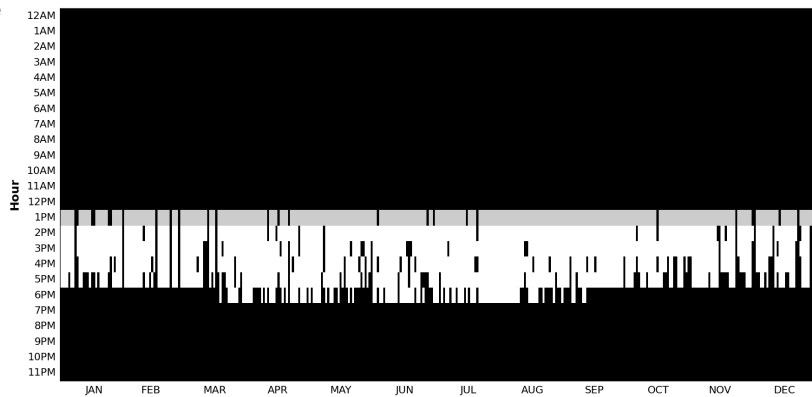
45 degree
Profile Angle



65 degree
Profile Angle



85 degree
Profile Angle

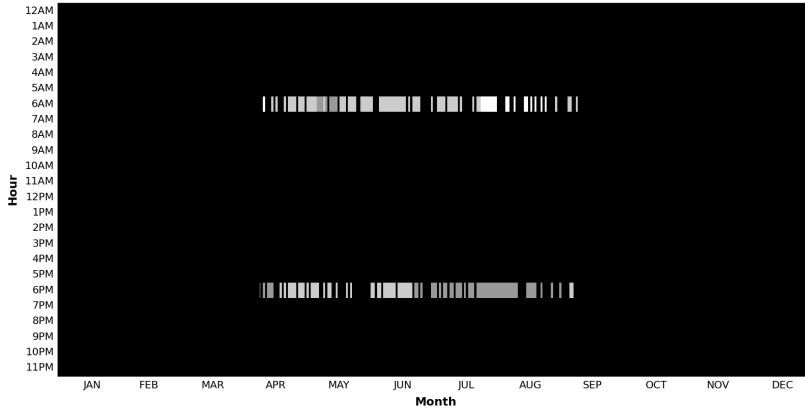


Add/B. DAYLIGHTING AND SHADING STUDIES

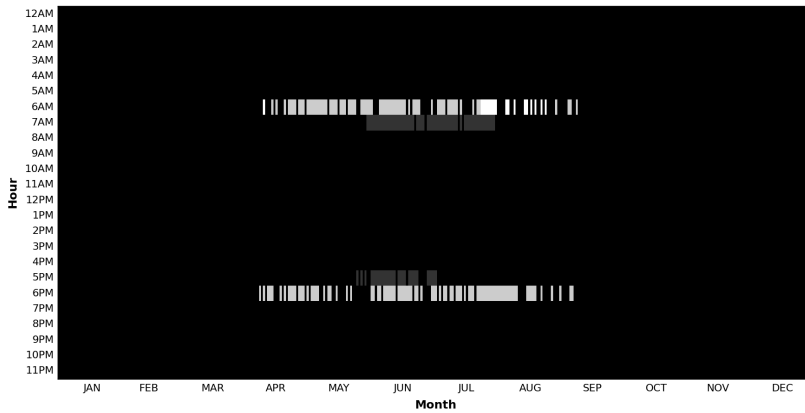
3. OPTIMIZING SOLAR CONTROL

3.2. HORIZONTAL OVERHANG EFFECTIVENESS

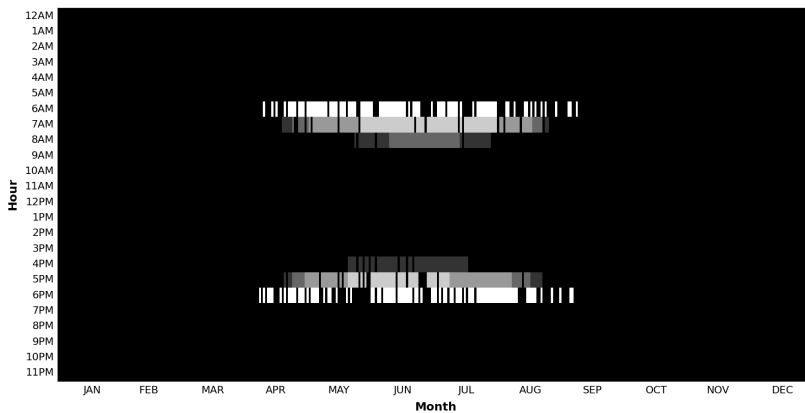
3.2.4 North Facade



35 degree
Profile Angle



55 degree
Profile Angle



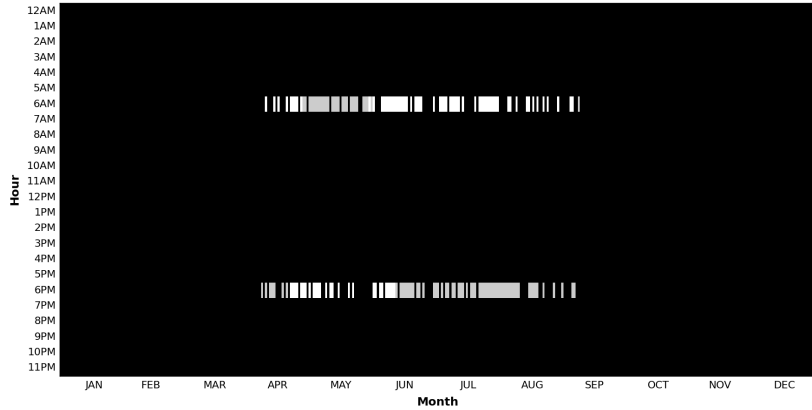
75 degree
Profile Angle



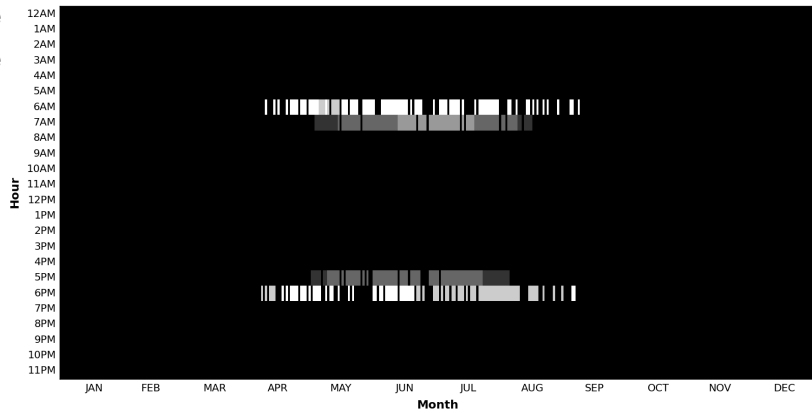
Add/B. 3.2.4 Horizontal Overhang Effectiveness:: North Facade(Continued)

Hourly graphs below show the percentage of the window that is shaded for various depths of horizontal overhangs.

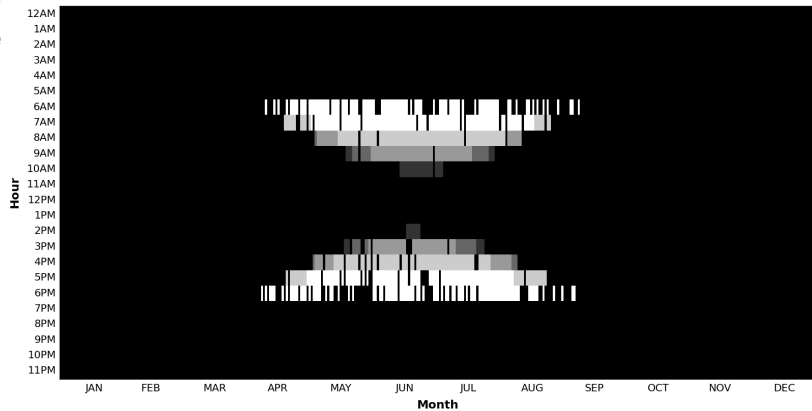
45 degree
Profile Angle



65 degree
Profile Angle



85 degree
Profile Angle

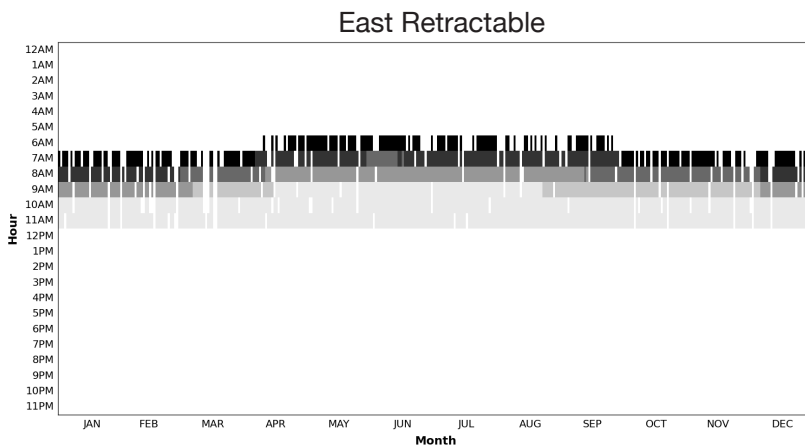
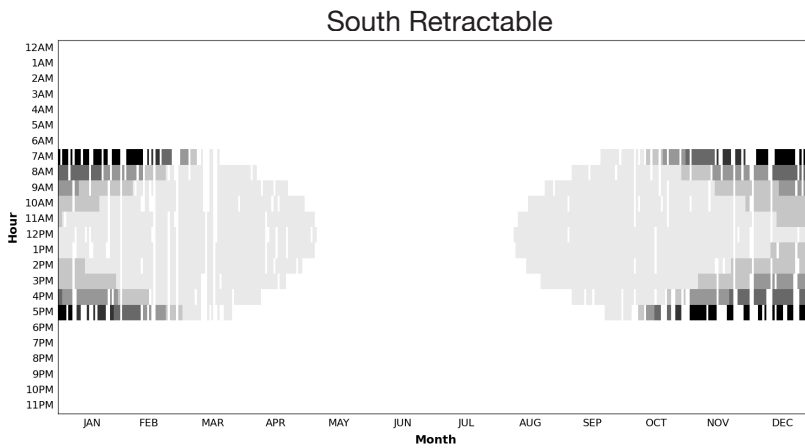


Add/B. DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

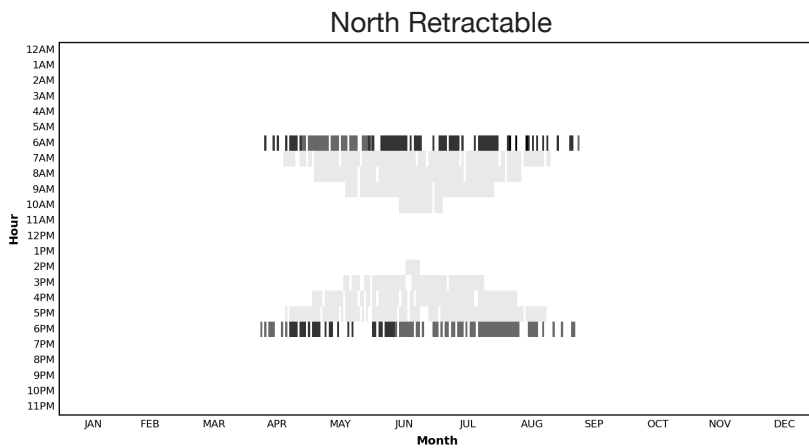
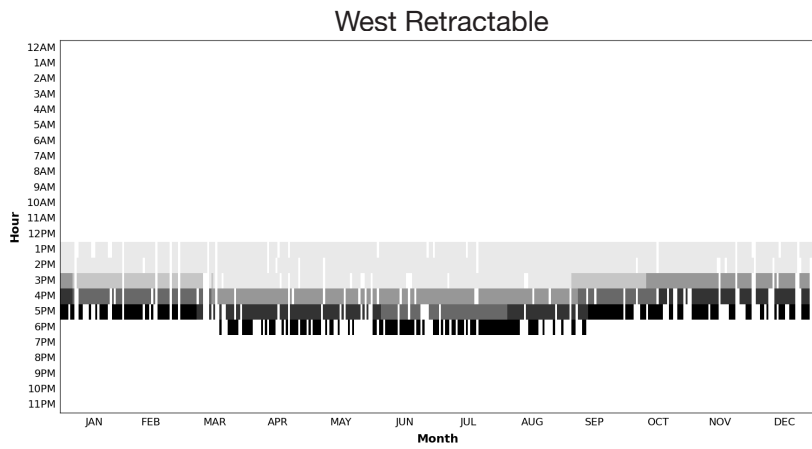
3.3. AUTOMATED LOUVER PROTOCOLS

3.3.1 Retractable



Add/B. 3.3.1 Automated Louver Protocols:: Retractable (Continued)

Schedules based on sun penetration for different orientations of operable louvers. Tilt only simulates with 5 positions, retractable has an Additional 6th position (fully open),



Closed Open

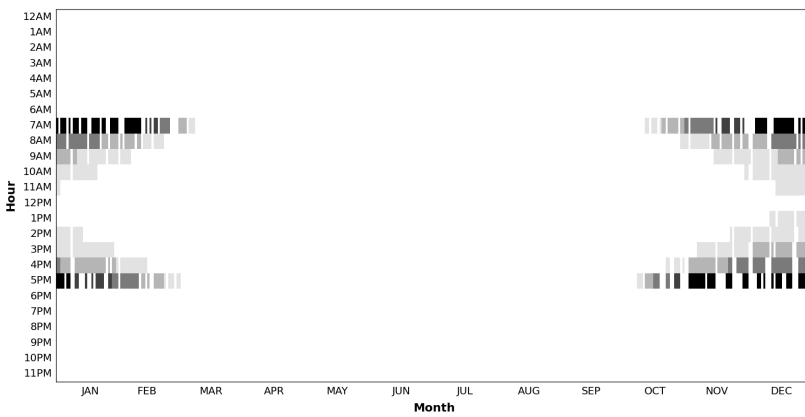
Add/B. DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

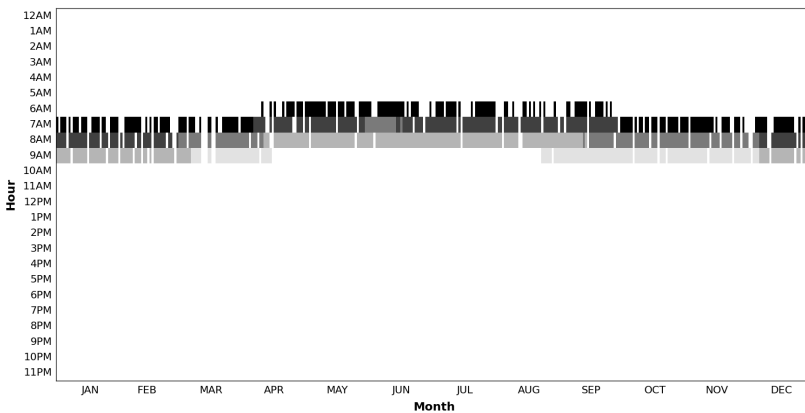
3.3. AUTOMATED LOUVER PROTOCOLS

3.3.2 Tilt Only

South Tilt Only

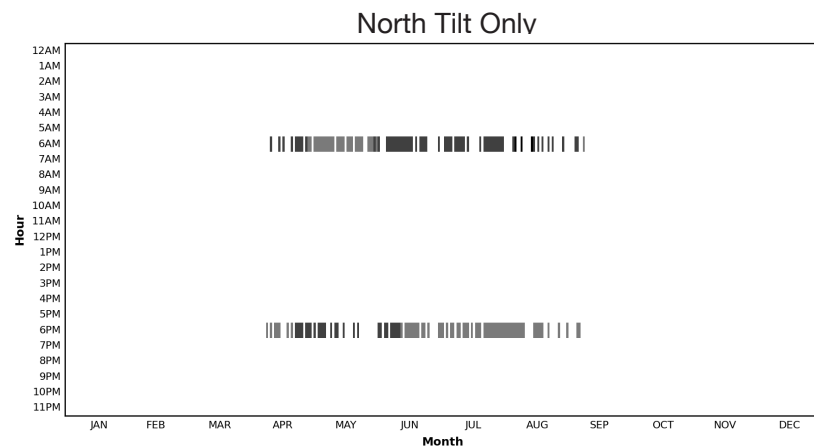
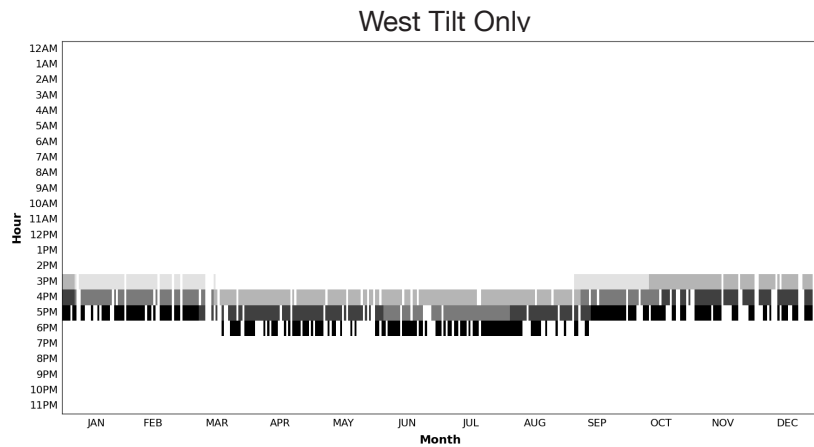


East Tilt Only



Add/B. 3.3.2 Automated Louver Protocols:: Tilt Only (Continued)

Schedules based on sun penetration for different orientations of operable louvers. Tilt only simulates with 5 positions, retractable has an Additional 6th position (fully open),



Closed Open

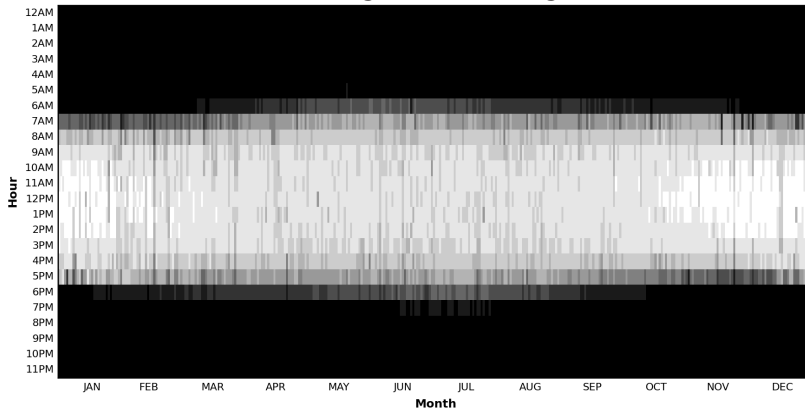
Add/B. DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

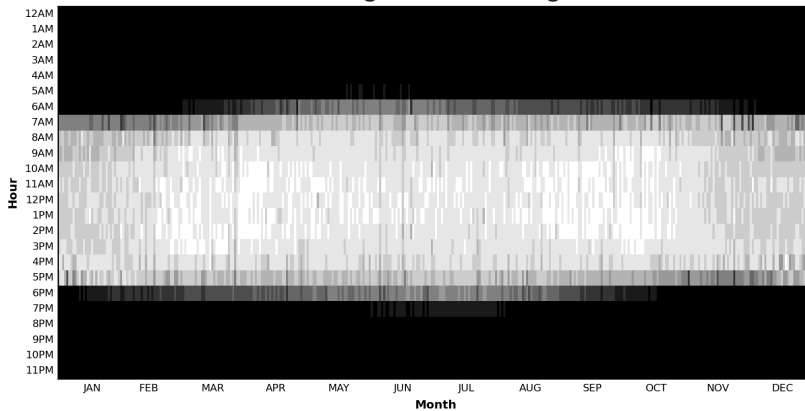
3.4. HOURLY USEFUL DAYLIGHT ILLUMINANCE

3.4.1 South Facade

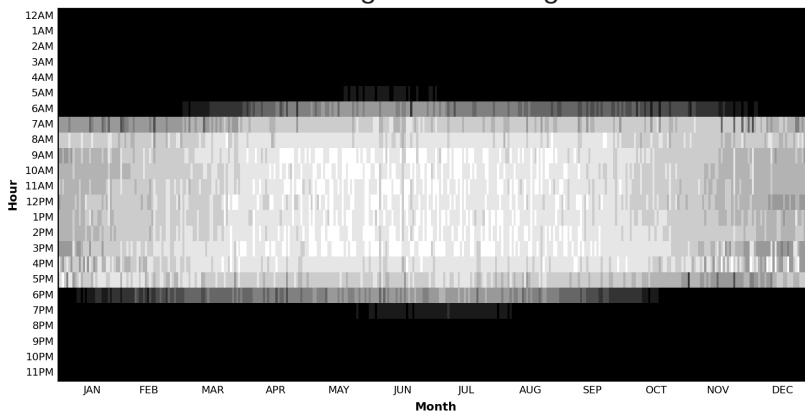
35 Degree Profile Angle



55 Degree Profile Angle



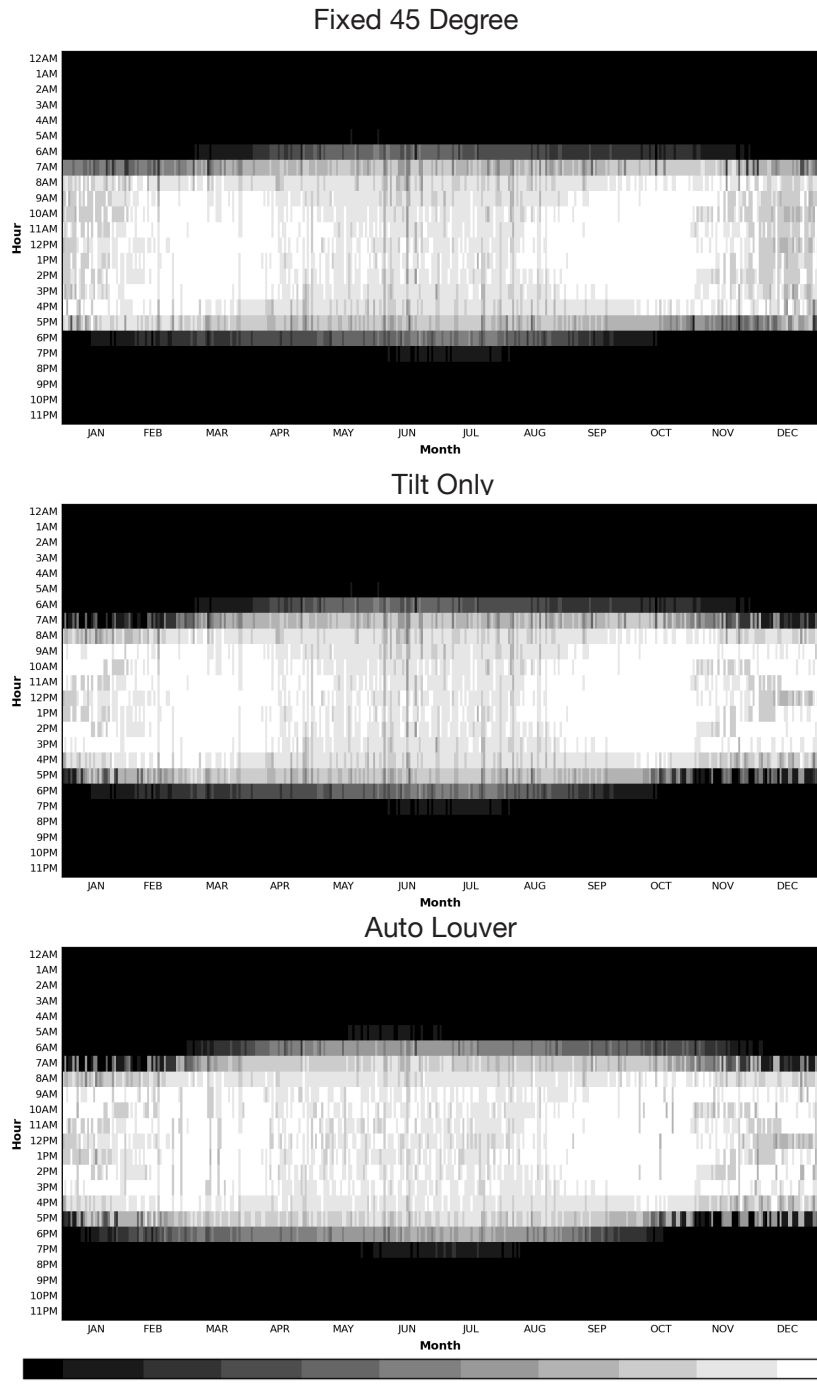
75 Degree Profile Angle



Percent Useful Illumination

Add/B. 3.4.1 Hourly Useful Daylight Illuminance:: South Facade (Continued)

These Hourly graphs below show the percentage of the space that Achieve between 30 and 300 FC with fractional credit for values below 30 FC.



Percent Useful Illumination

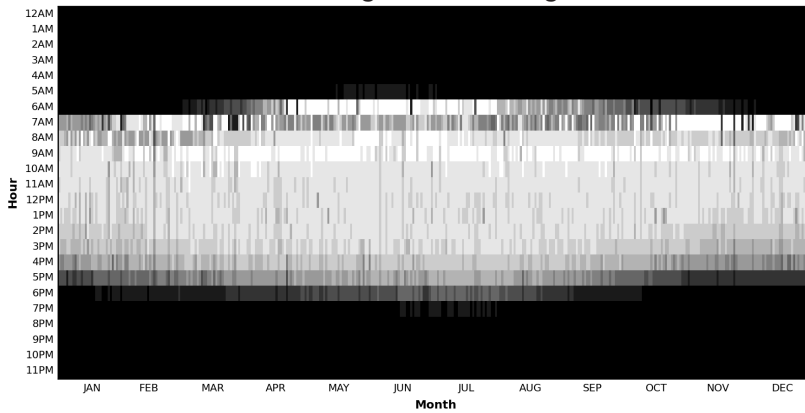
Add/B. DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

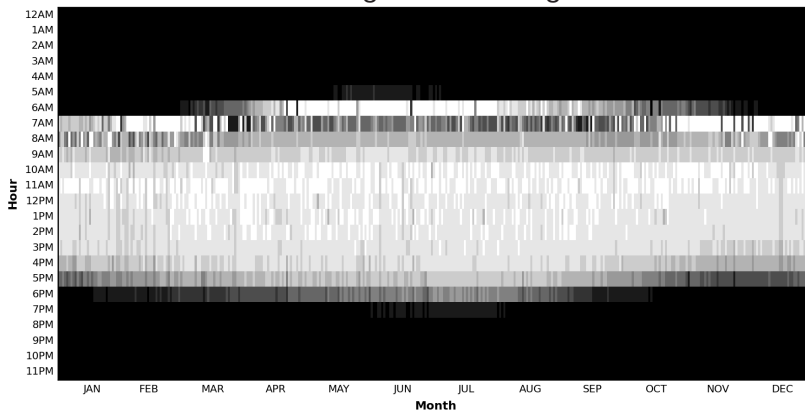
3.4. HOURLY USEFUL DAYLIGHT ILLUMINANCE

3.4.2 East Facade

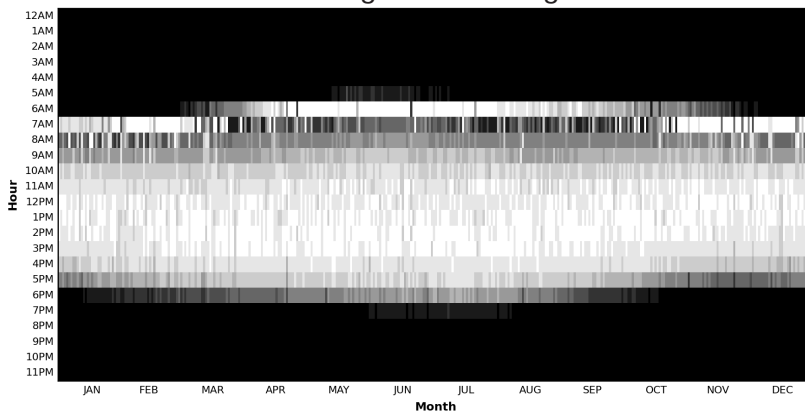
35 Degree Profile Angle



55 Degree Profile Angle



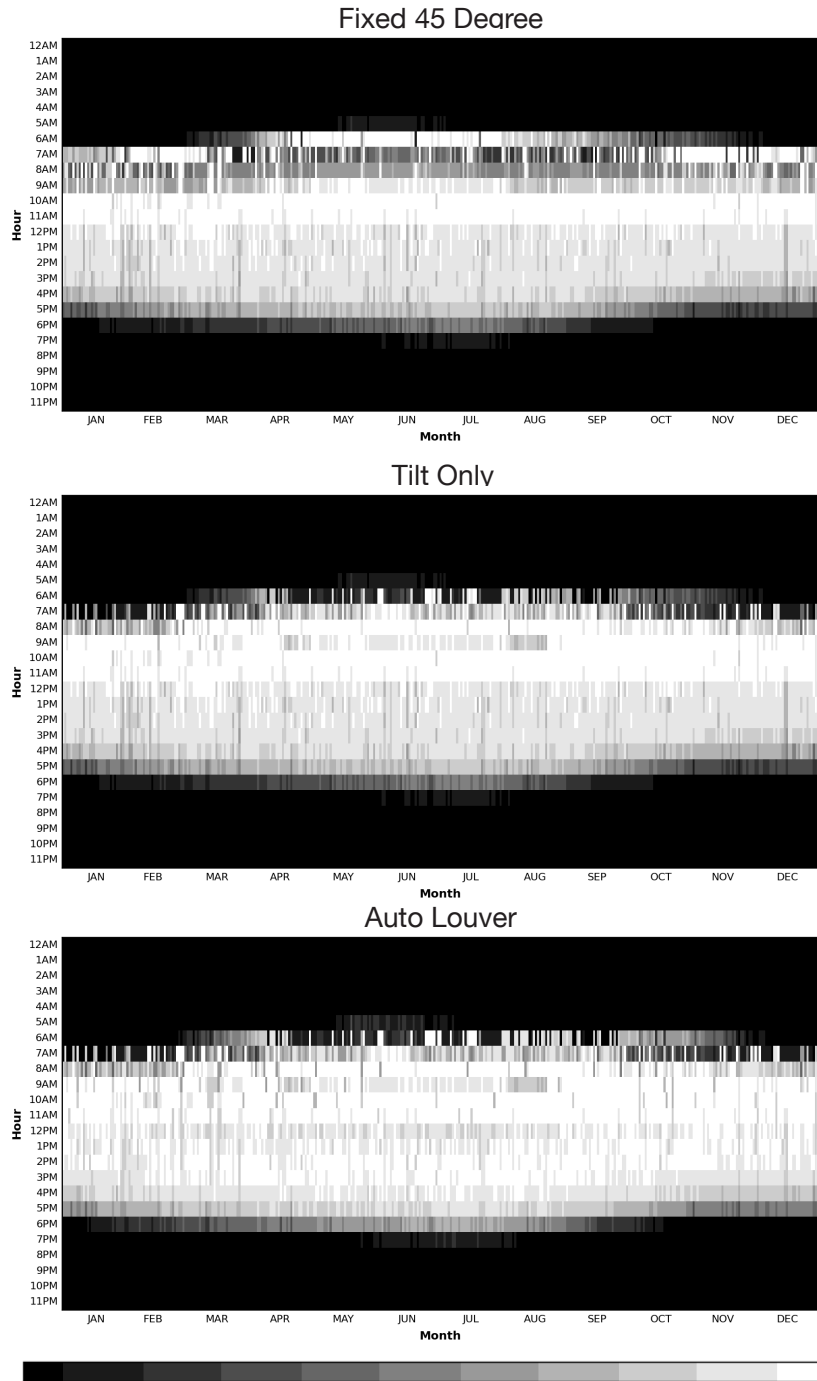
75 Degree Profile Angle



Percent Useful Illumination

Add/B. 3.4.2 Hourly Useful Daylight Illuminance:: East Facade (Continued)

These Hourly graphs below show the percentage of the space that Achieve between 30 and 300 FC with fractional credit for values below 30 FC.



Percent Useful Illumination

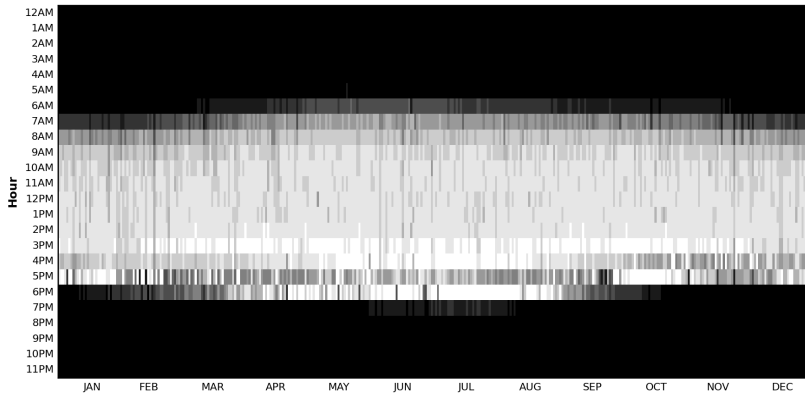
Add/B. DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

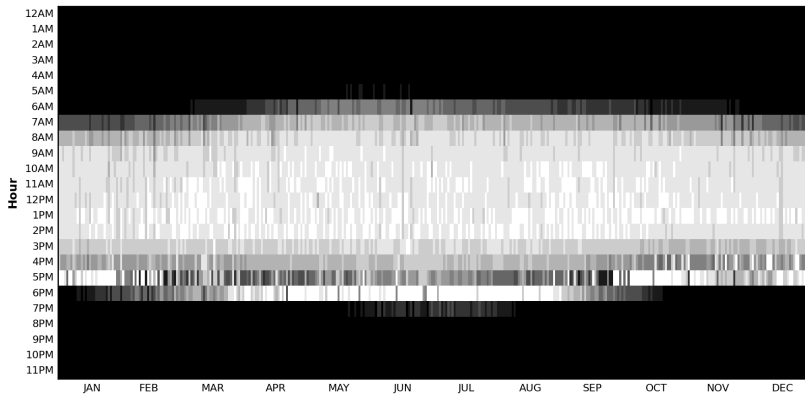
3.4. HOURLY USEFUL DAYLIGHT ILLUMINANCE

3.4.3 West Facade

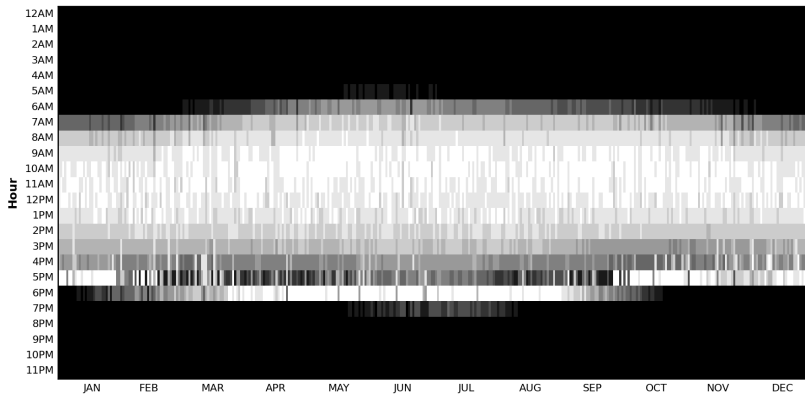
35 Degree Profile Angle



55 Degree Profile Angle



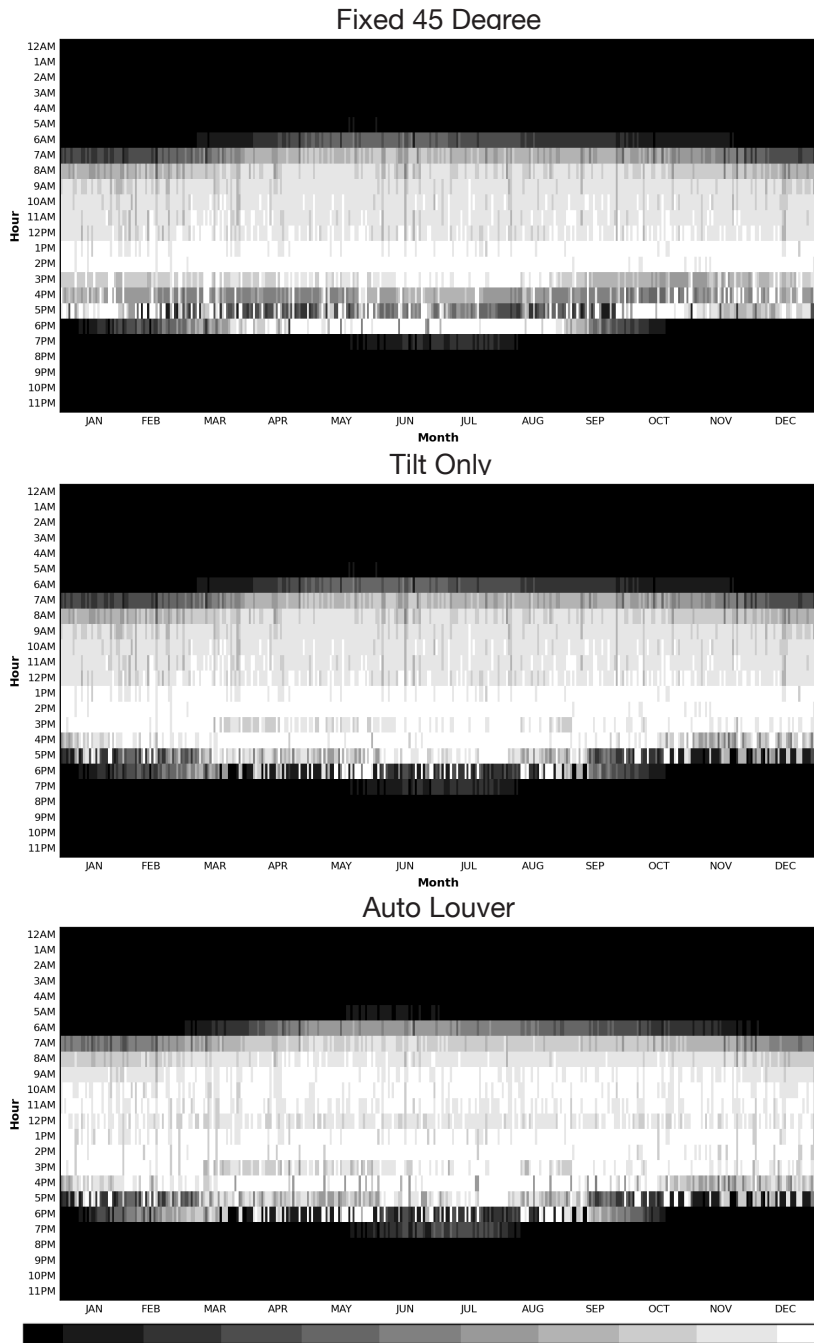
75 Degree Profile Angle



Percent Useful Illumination

Add/B. 3.4.3 Hourly Useful Daylight Illuminance:: West Facade (Continued)

These Hourly graphs below show the percentage of the space that Achieve between 30 and 300 FC with fractional credit for values below 30 FC.



Percent Useful Illumination

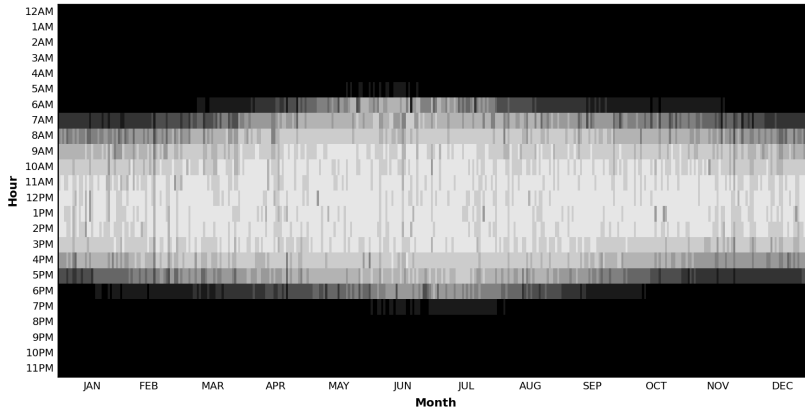
Add/B. DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

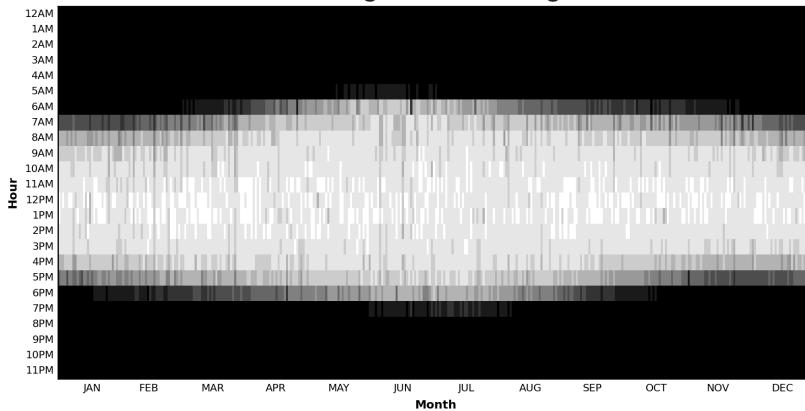
3.4. HOURLY USEFUL DAYLIGHT ILLUMINANCE

3.4.4 North Facade

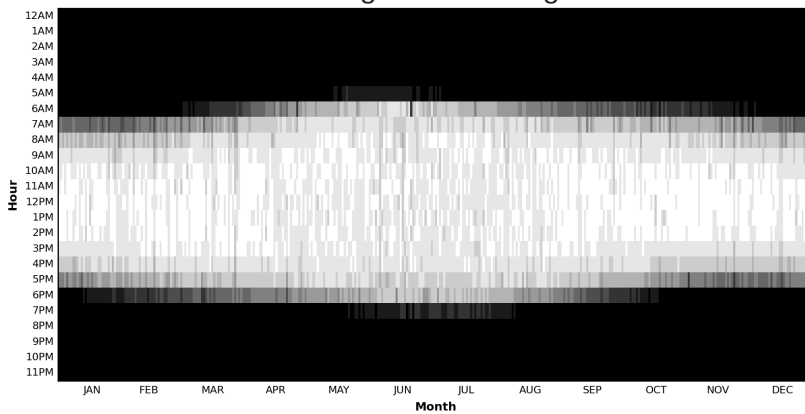
35 Degree Profile Angle



55 Degree Profile Angle



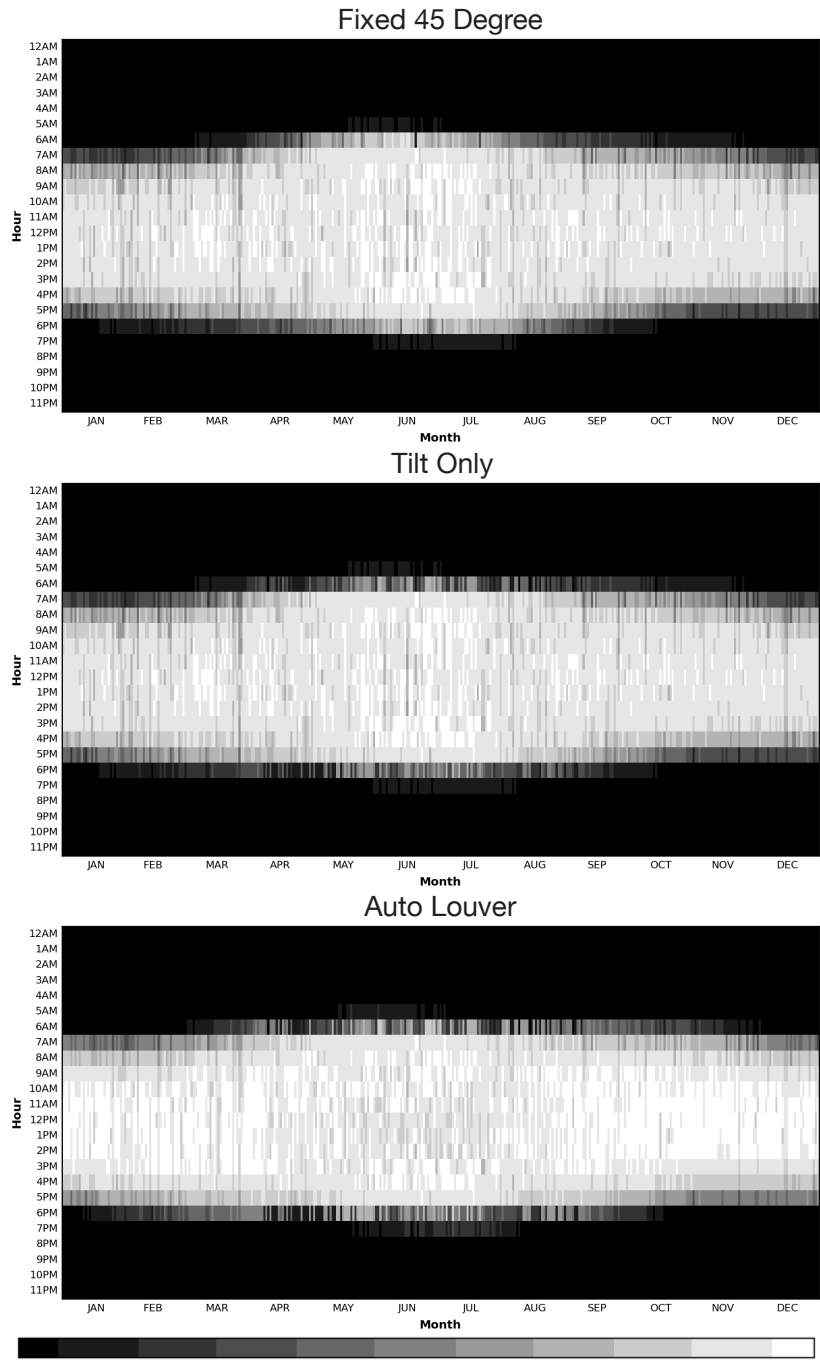
75 Degree Profile Angle



Percent Useful Illumination

Add/B. 3.4.4 Hourly Useful Daylight Illuminance:: North Facade (Continued)

These Hourly graphs below show the percentage of the space that Achieve between 30 and 300 FC with fractional credit for values below 30 FC.



Percent Useful Illumination

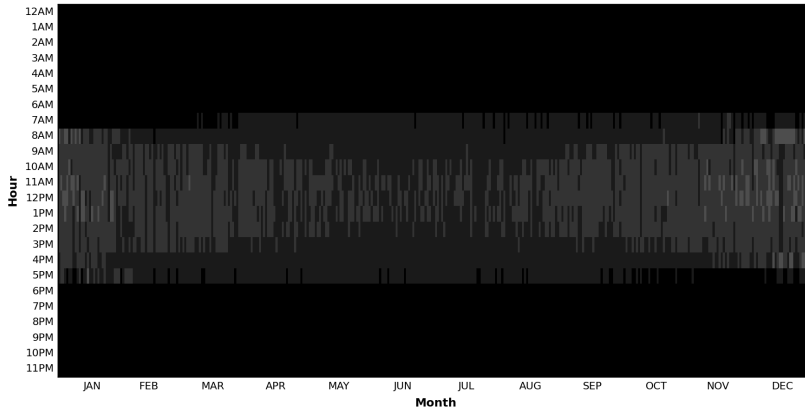
Add/B. DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

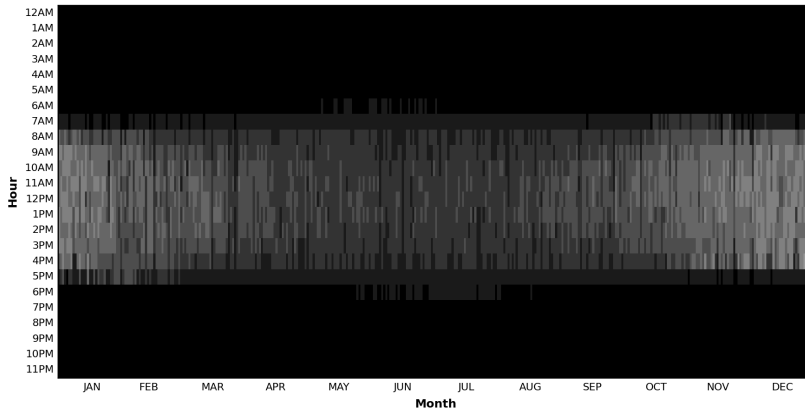
3.5. HOURLY EXCESSIVE ILLUMINANCE

3.5.1 South Facade

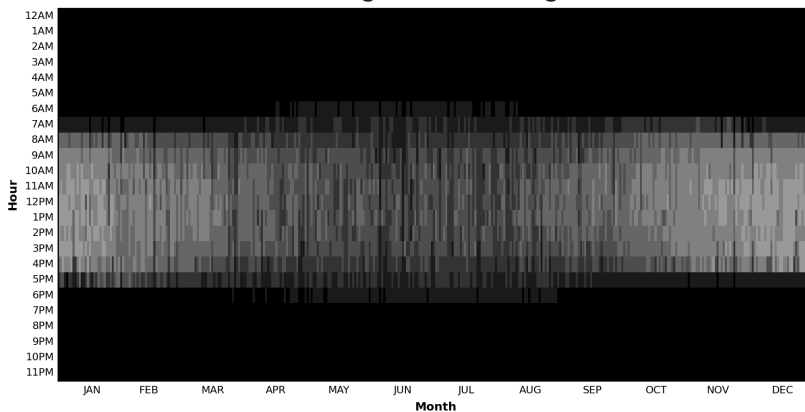
35 Degree Profile Angle



55 Degree Profile Angle



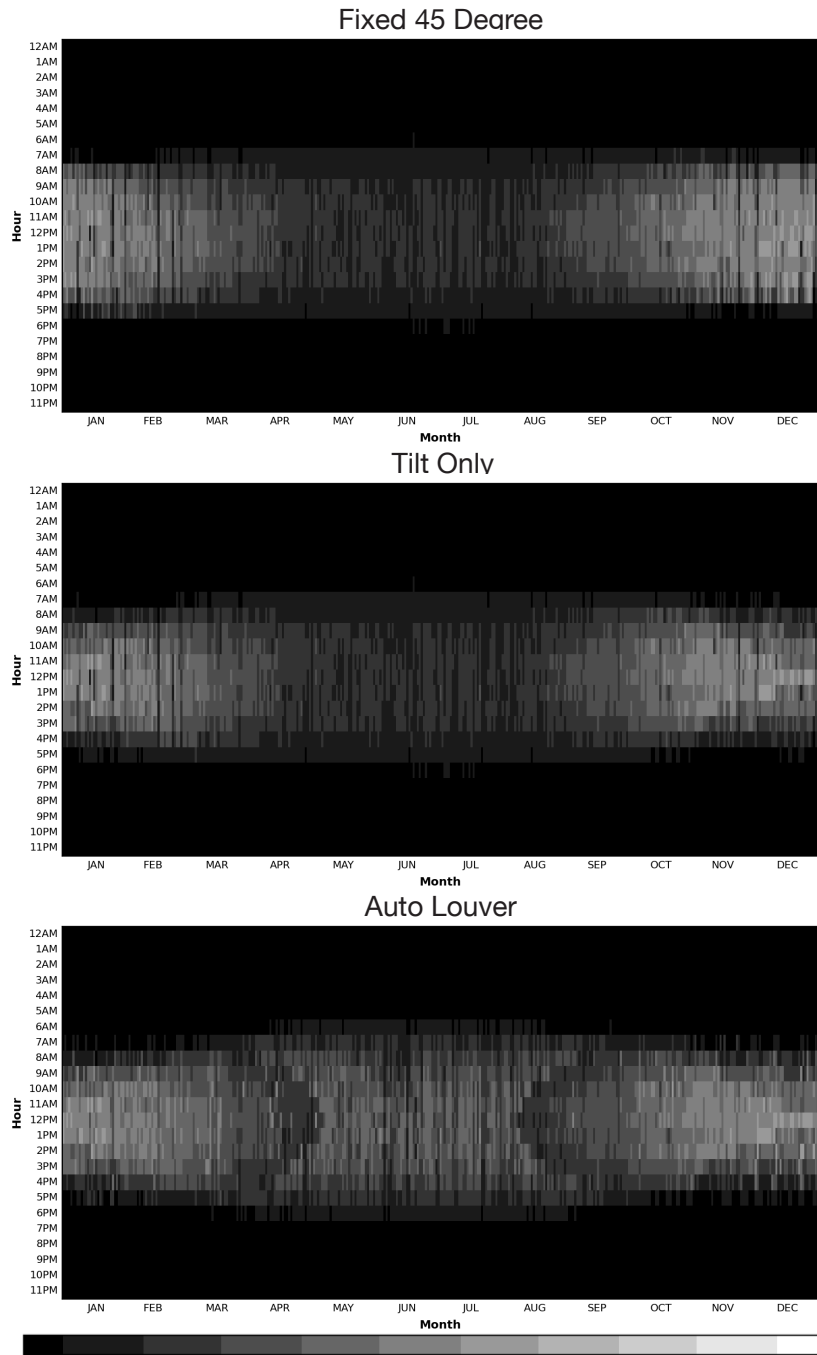
75 Degree Profile Angle



Percent Excessive Illumination

Add/B. 3.5.1 Hourly Excessive Illuminance:: South Facade (Continued)

These Hourly graphs below show the percentage of the space that exceeds 300 FC.



Percent Excessive Illumination

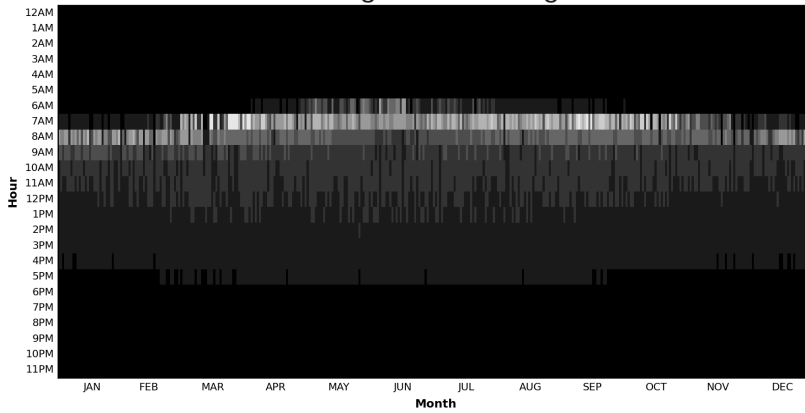
Add/B. DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

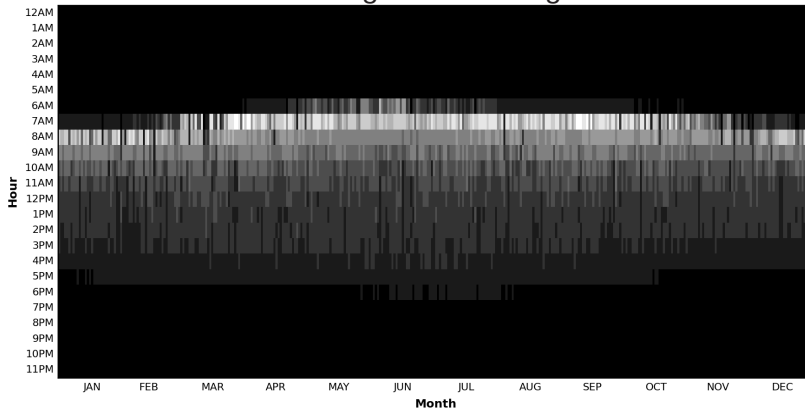
3.5. HOURLY EXCESSIVE ILLUMINANCE

3.5.2 East Facade

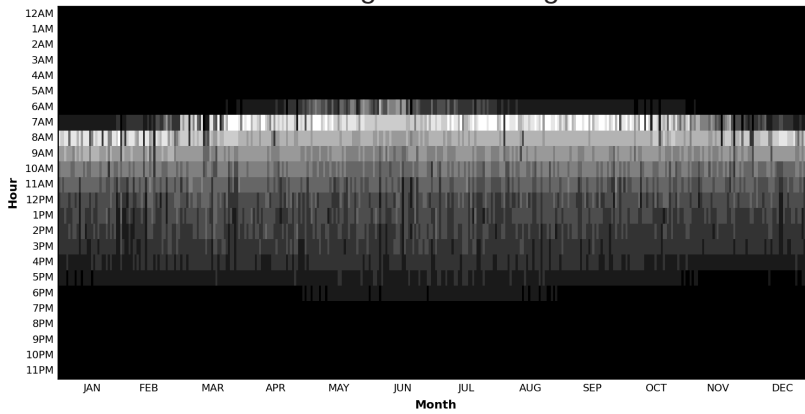
35 Degree Profile Angle



55 Degree Profile Angle



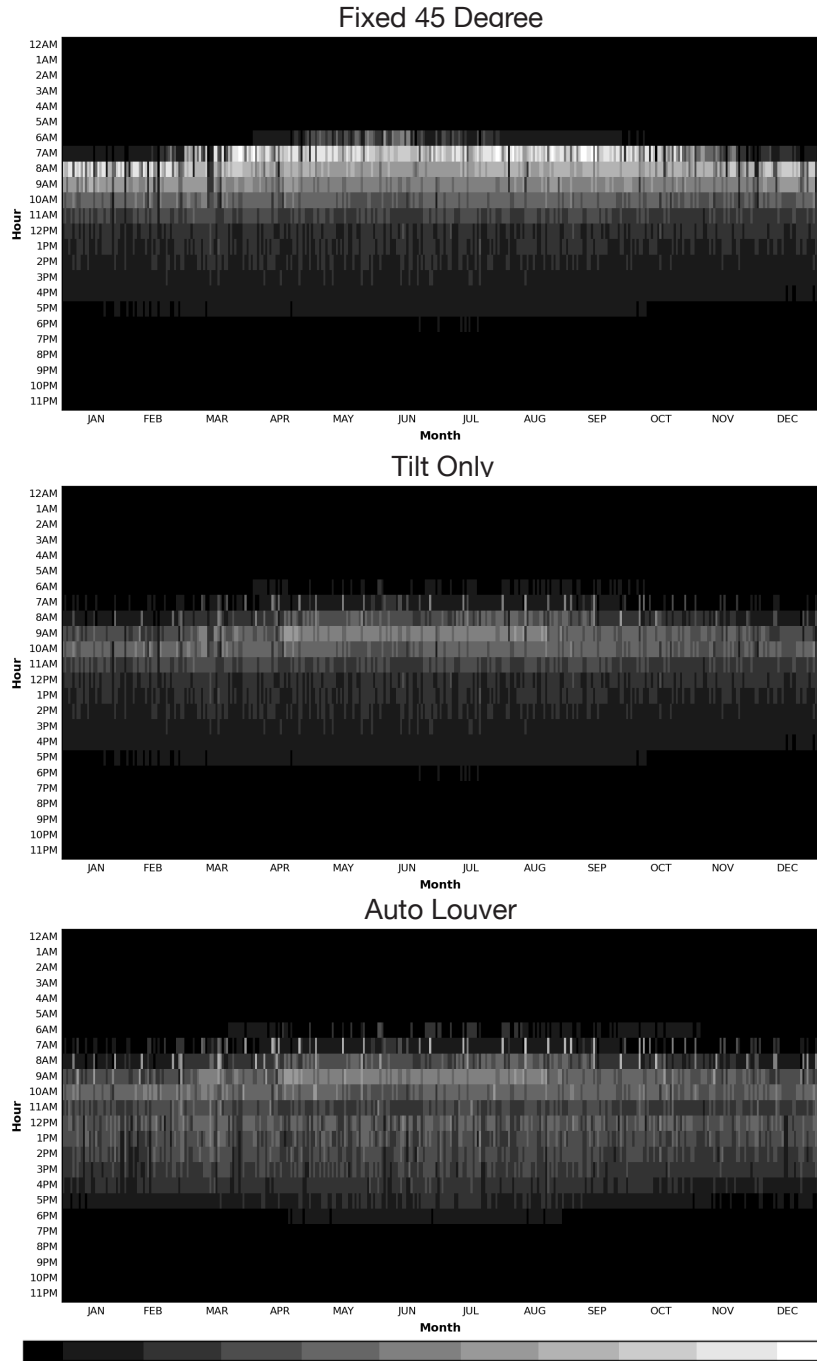
75 Degree Profile Angle



Percent Excessive Illumination

Add/B. 3. 5.2 Hourly Excessive Illuminance:: East Facade (Continued)

These Hourly graphs below show the percentage of the space that exceeds 300 FC.



Percent Excessive Illumination

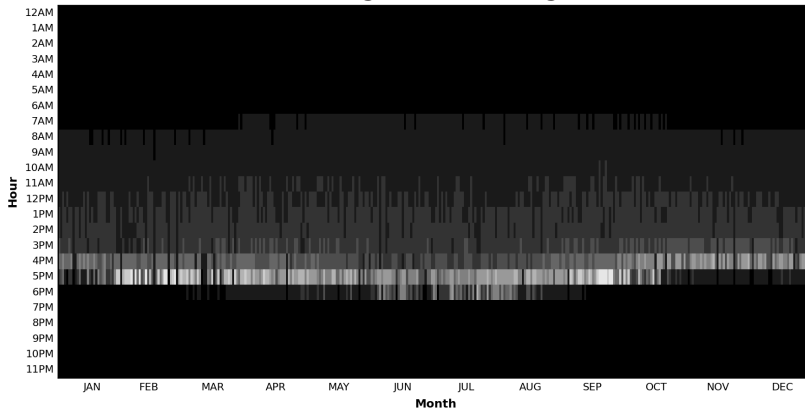
Add/B. DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

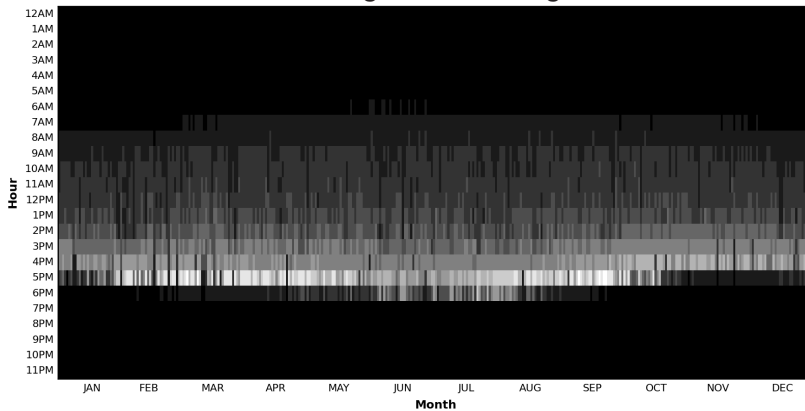
3.5. HOURLY EXCESSIVE ILLUMINANCE

3.5.3 West Facade

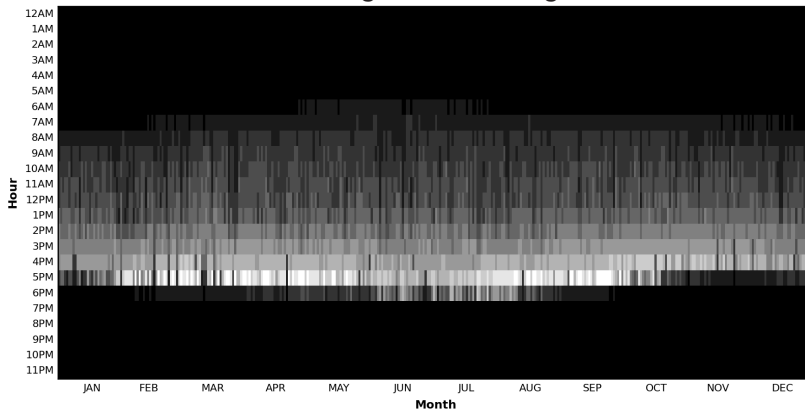
35 Degree Profile Angle



55 Degree Profile Angle



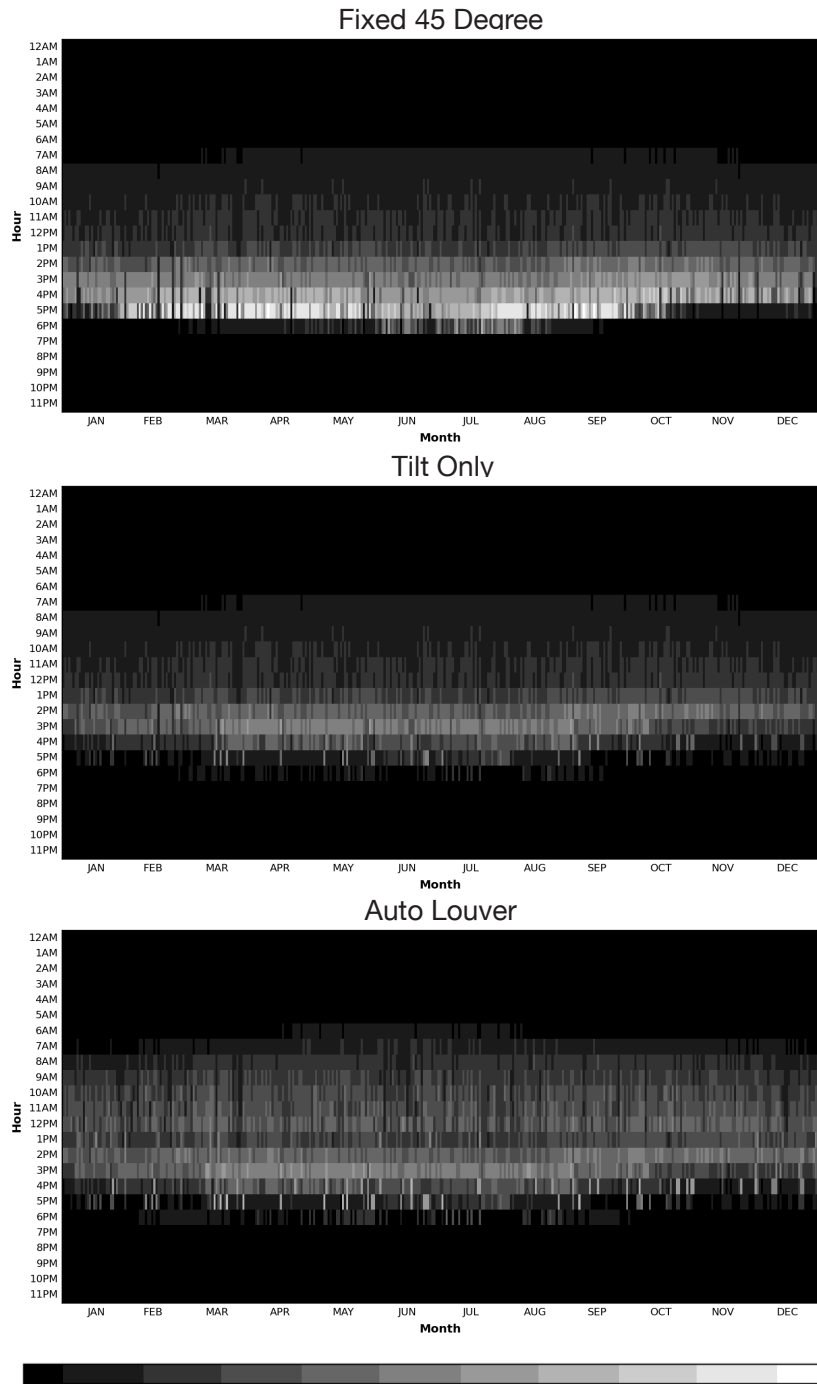
75 Degree Profile Angle



Percent Excessive Illumination

Add/B. 3.5.3 Hourly Excessive Illuminance:: West Facade (Continued)

These Hourly graphs below show the percentage of the space that exceeds 300 FC.



Percent Excessive Illumination

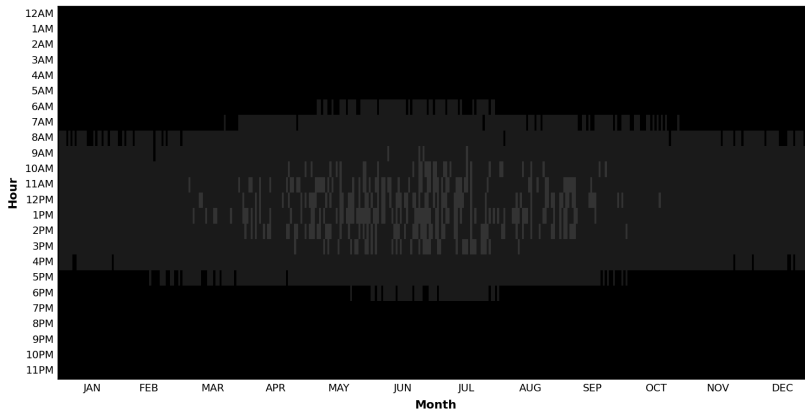
Add/B. DAYLIGHTING AND SHADING STUDIES

3. OPTIMIZING SOLAR CONTROL

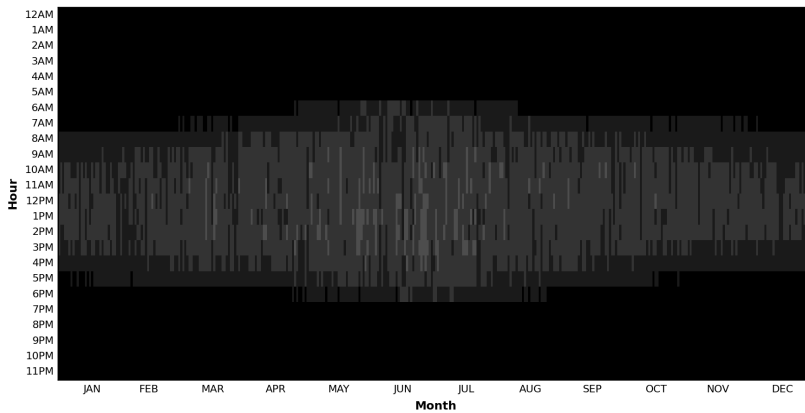
3.5. HOURLY EXCESSIVE ILLUMINANCE

3.5.4 North Facade

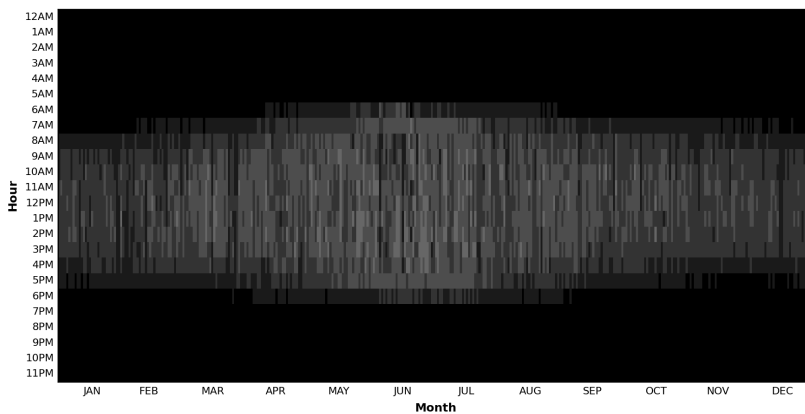
35 Degree Profile Angle



55 Degree Profile Angle



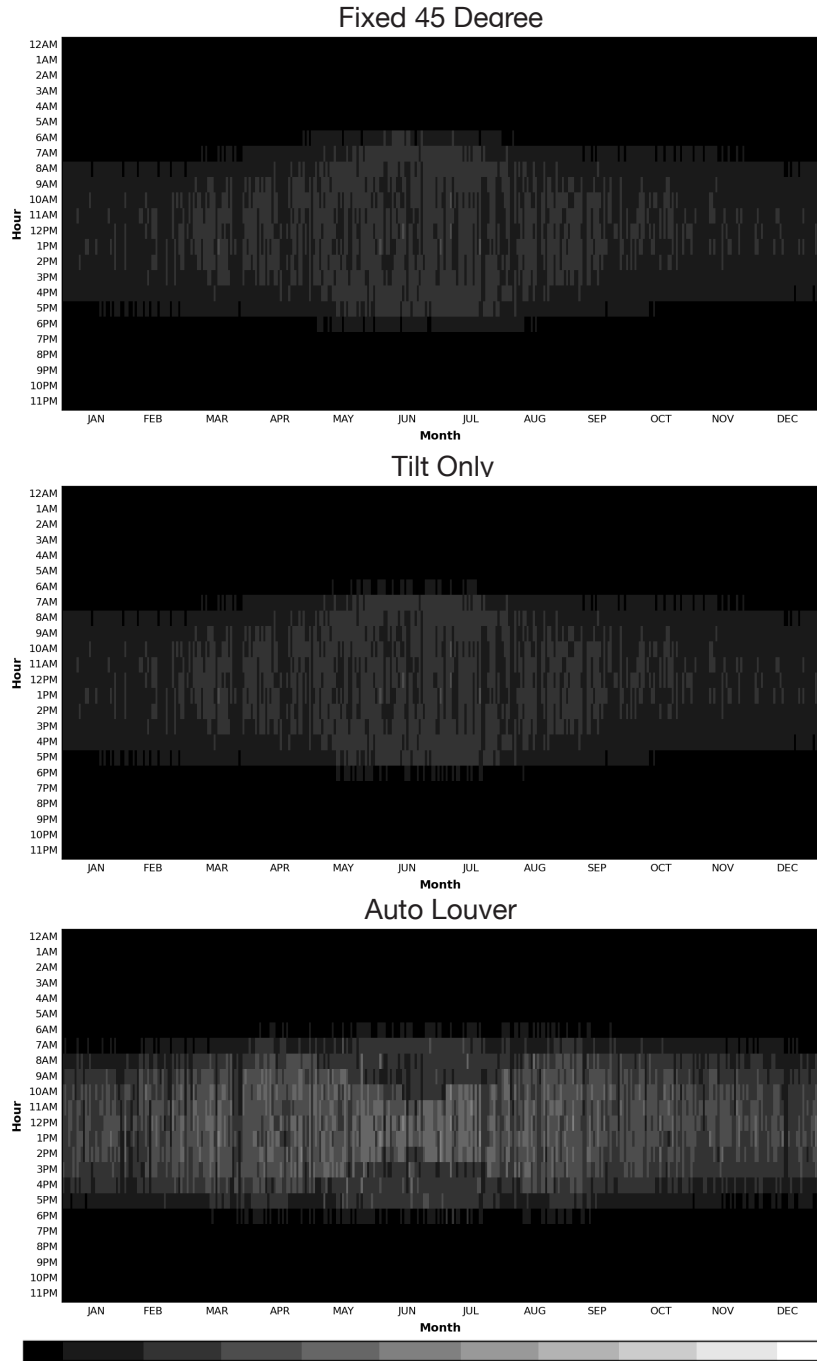
75 Degree Profile Angle



Percent Excessive Illumination

Add/B. 3.5.4 Hourly Excessive Illuminance:: North Facade (Continued)

These Hourly graphs below show the percentage of the space that exceeds 300 FC.



Percent Excessive Illumination

[BLANK]

Add/B. DAYLIGHTING AND SHADING STUDIES

4. DAYLIGHTING AND VISUAL COMFORT ANALYSIS

4.1/ SUMMARY OF RESULTS.....19

4.2/ AUTOMATED SHADE PROTOCOLS.....49

4.3/ HUMAN RESPONSE RENDERINGS.....49

4.4/ FALSECOLOR LUMINANCE49

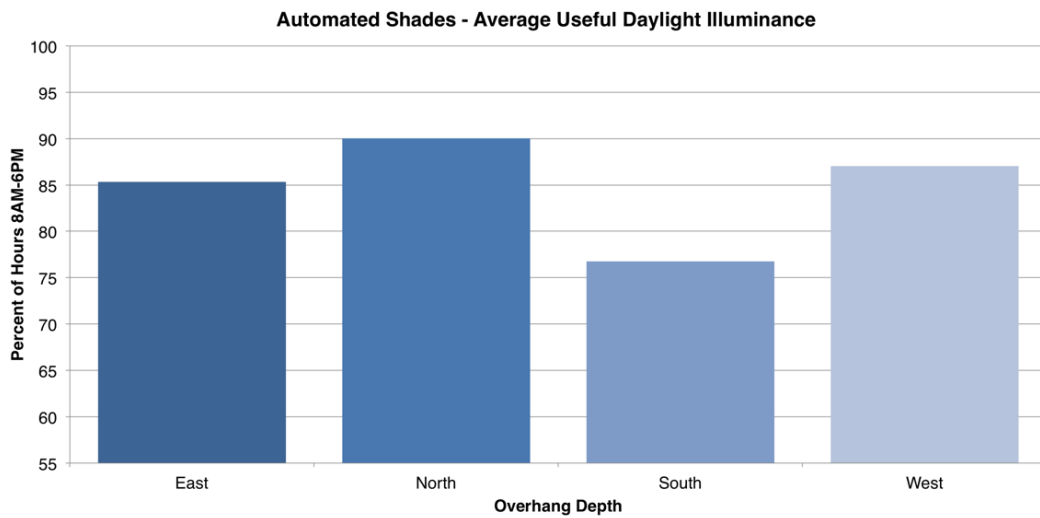
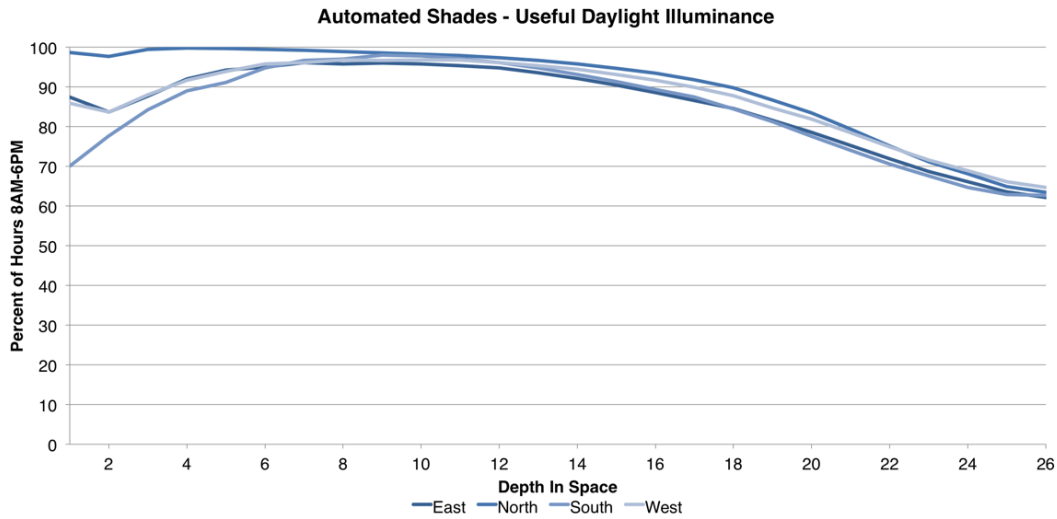
B. DAYLIGHTING AND SHADING

Add/B. DAYLIGHTING AND SHADING STUDIES

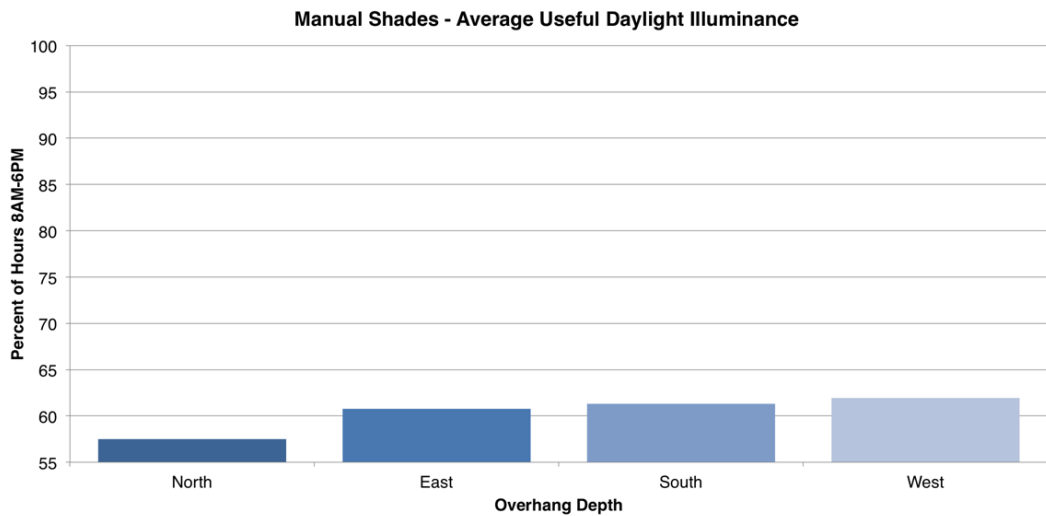
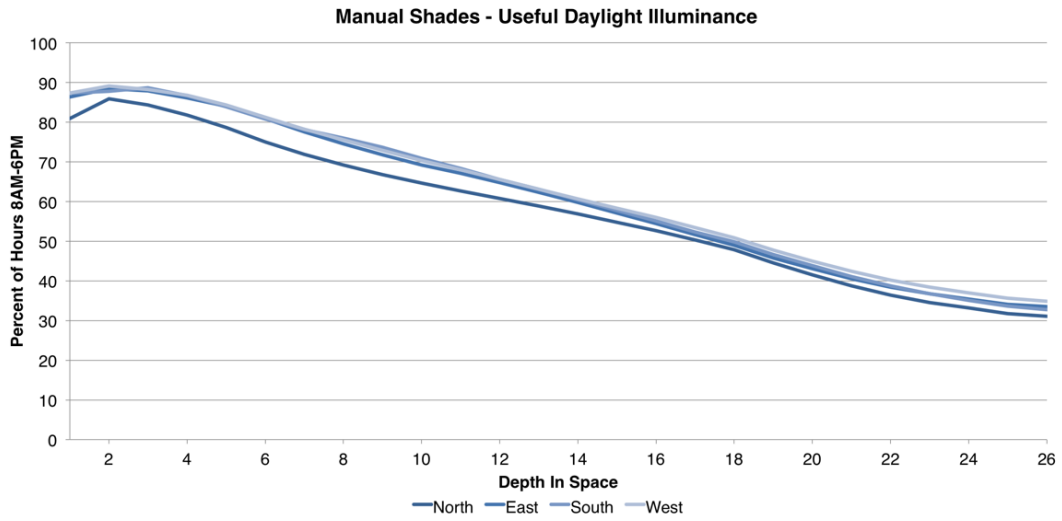
4. DAYLIGHTING AND VISUAL COMFORT ANALYSIS

4.1. SUMMARY OF RESULTS

**Roller Shades with 65 Degree Overhang::
Manual vs/ Automated**



**Add/B. 4.1. Summary of Results:: Roller Shades with 65 Degree Overhang::
Manual vs/ Automated (Continued)**



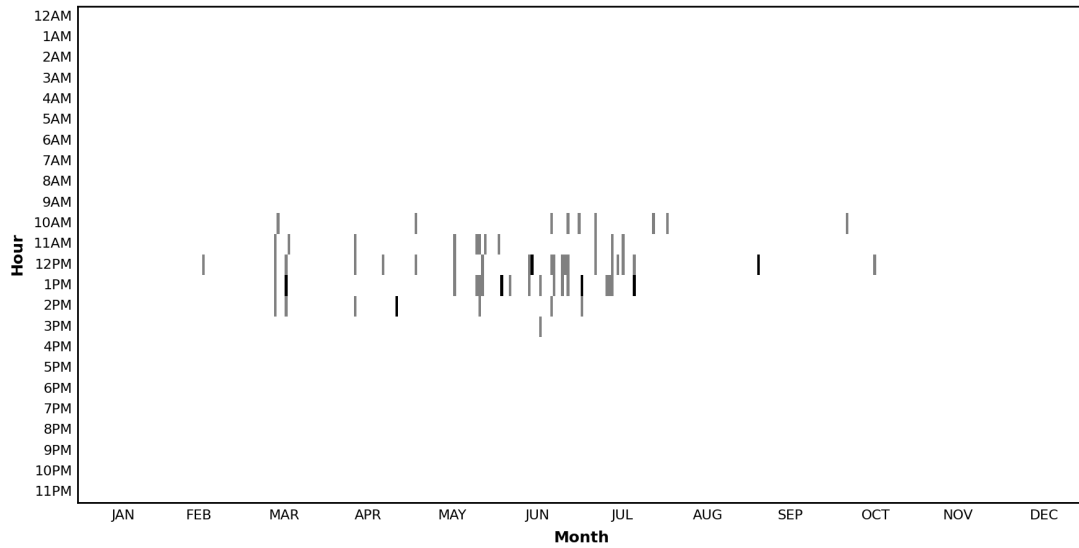
Add/B. DAYLIGHTING AND SHADING STUDIES

4. DAYLIGHTING AND VISUAL COMFORT ANALYSIS

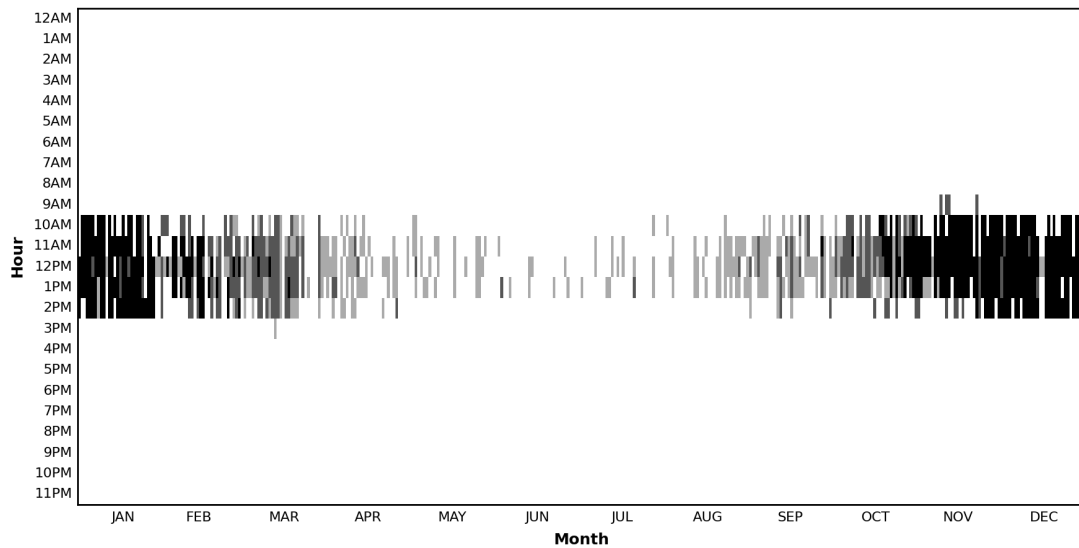
4.2. AUTOMATED SHADE PROTOCOLS BY ORIENTATION

65 Degree Overhang

North

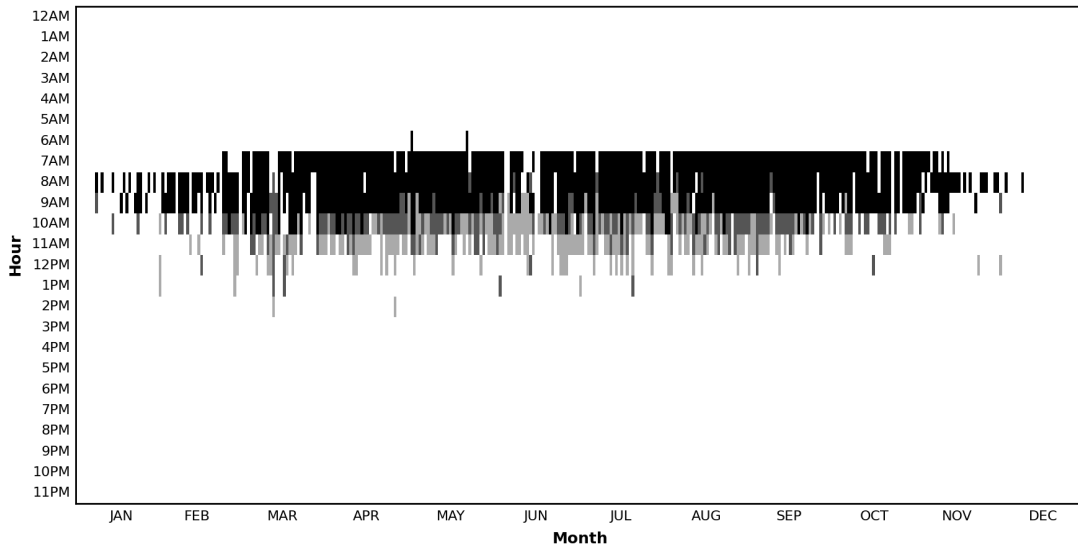


South

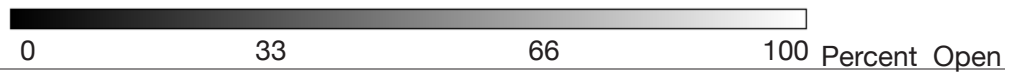
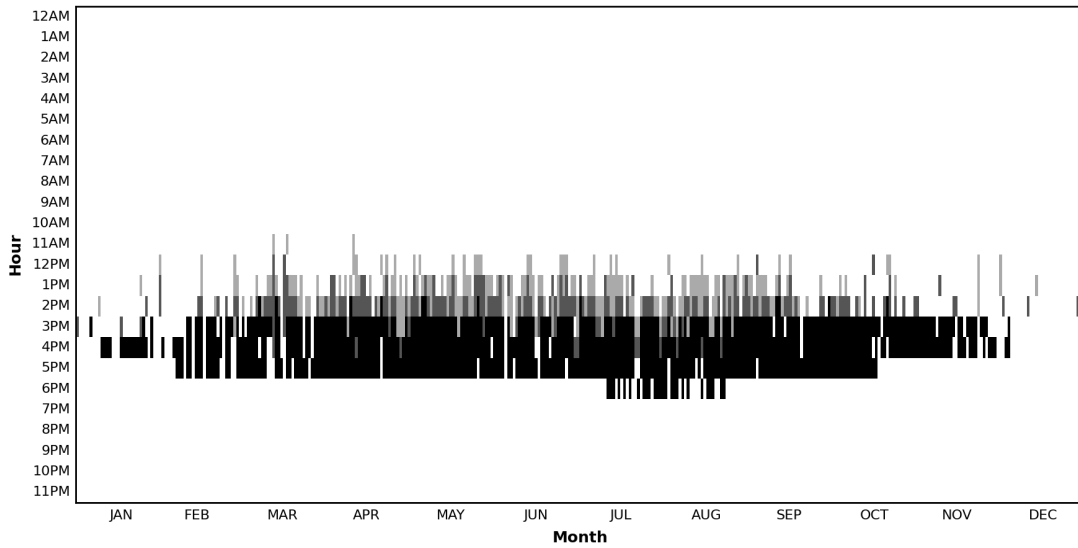


**Add/B. 4.2 Automated Shade Protocols By Orientation:: 65 Degree Overhang
(Continued)**

East



West



Add/B. DAYLIGHTING AND SHADING STUDIES

4. DAYLIGHTING AND VISUAL COMFORT ANALYSIS

4.3. HUMAN RESPONSE RENDERINGS

65 Typical Classroom Facing West



With Shades Lowered for sky brightness



Typical Sunny Sky March 2 pm

**Add/B. 4.3 Human Response Renderings:: Typical Classroom Facing West
(Continued)**

The perspective view is processed with an algorithm that mimics human visual acuity, and is tone mapped to simulate the saturation, exposure, and possible veiling glare a human eye would see.



Without shades



Typical Sunny Sky March 2 pm

Add/B. DAYLIGHTING AND SHADING STUDIES

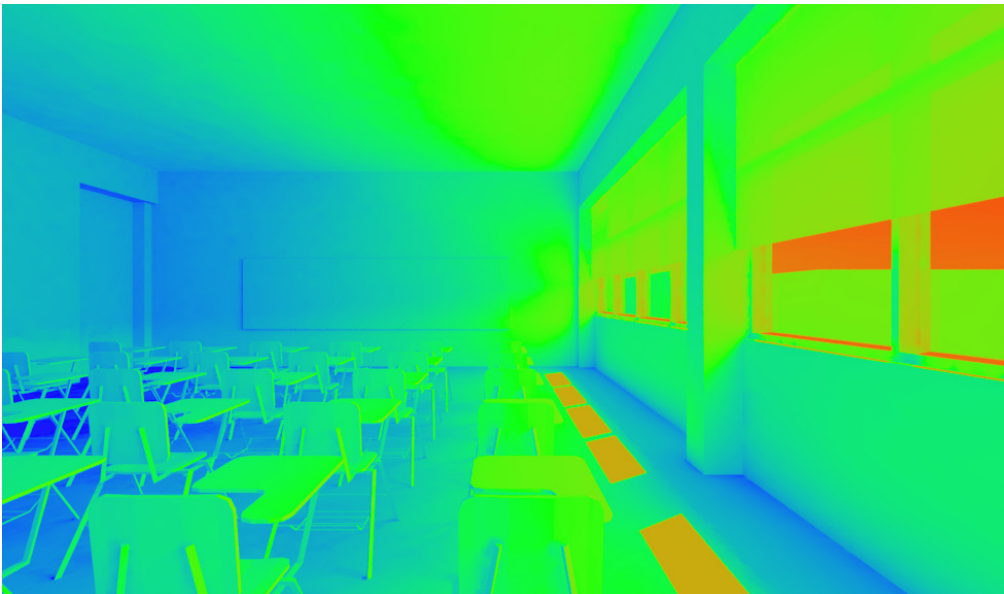
4. DAYLIGHTING AND VISUAL COMFORT ANALYSIS

4.4. FALSECOLOR LUMINANCE

Typical Classroom Facing West



With Shades Lowered for sky brightness



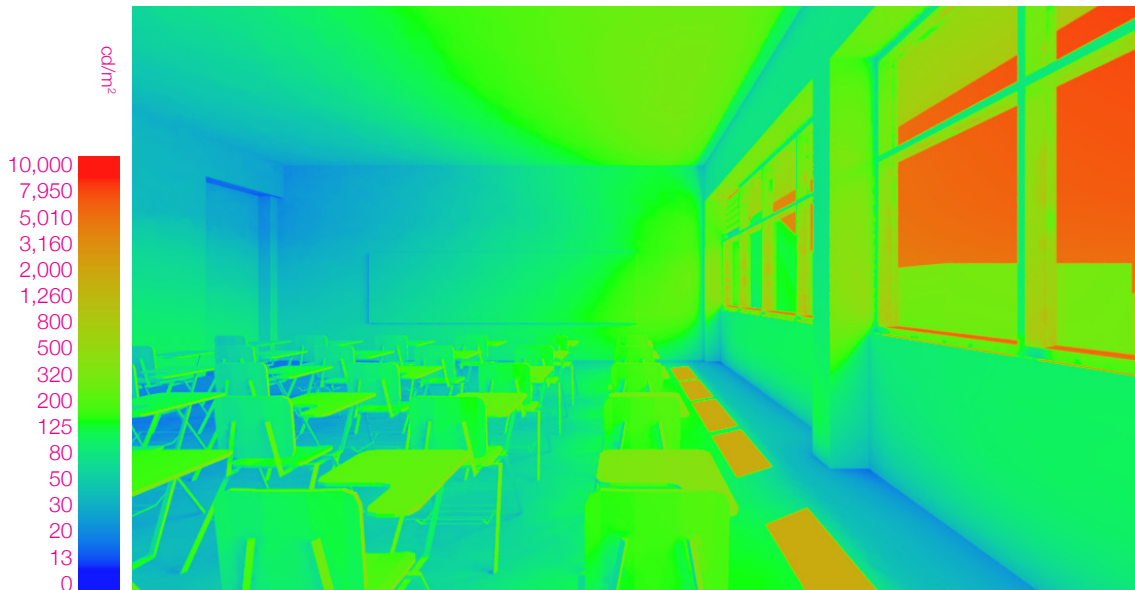
Typical Sunny Sky March 2 pm

Add/B. 4.4 Falsecolor Luminance:: Typical Classroom Facing West (Continued)

The falsecolor luminance map shows the rendered view on a color scale to communicate surface brightness. The scale is set to approximate the range of values an occupant can comfortably handle while in a daylighted space. As a point-in-time metric (rather than annualized data), this is a useful tool to identify potential glare sources and the experiential quality of the luminous environment. These luminance maps are shown in candelas per square meter (cd/m²), also known as nits. As reference, a new LCD computer monitor has a peak brightness of approximately 300 cd/m².



Without shades



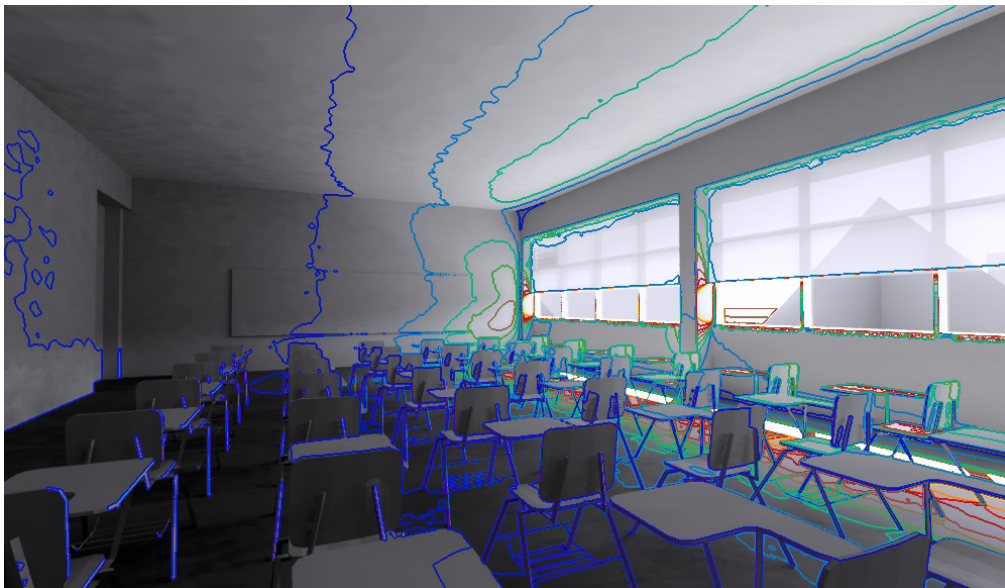
Typical Sunny Sky March 2 pm

Add/B. DAYLIGHTING AND SHADING STUDIES

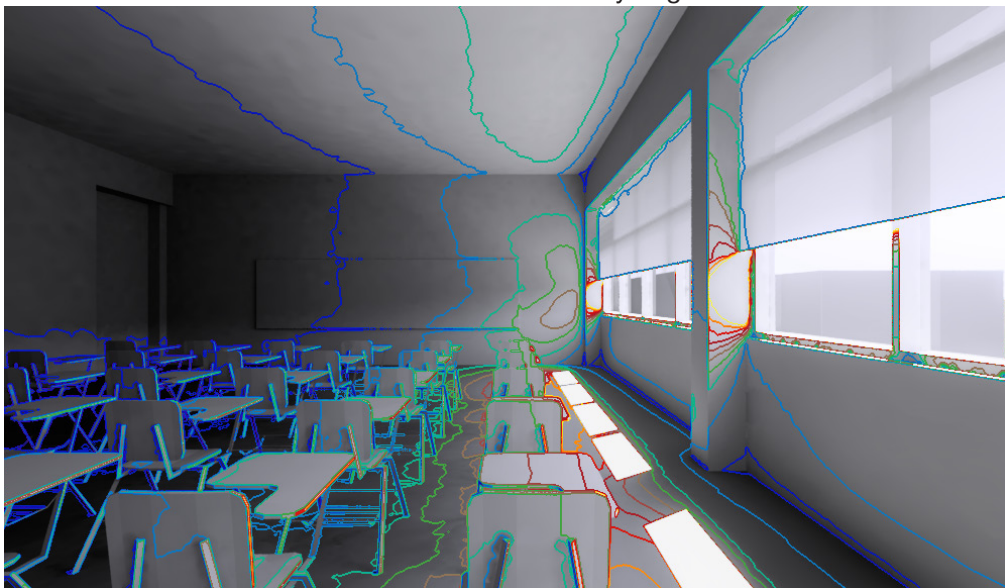
4. DAYLIGHTING AND VISUAL COMFORT ANALYSIS

4.4. FALSECOLOR LUMINANCE

Typical Classroom Facing West



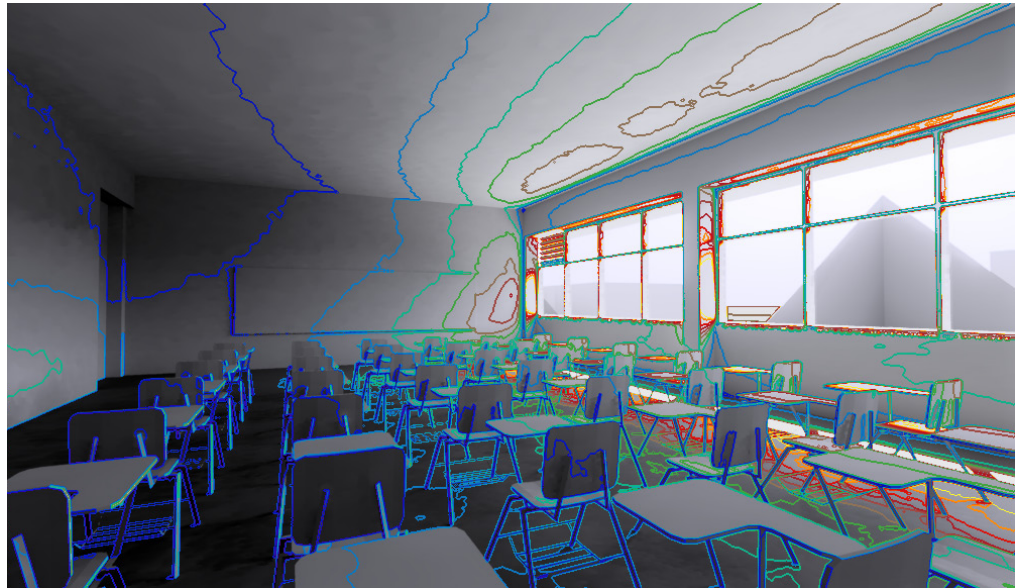
With Shades Lowered for sky brightness



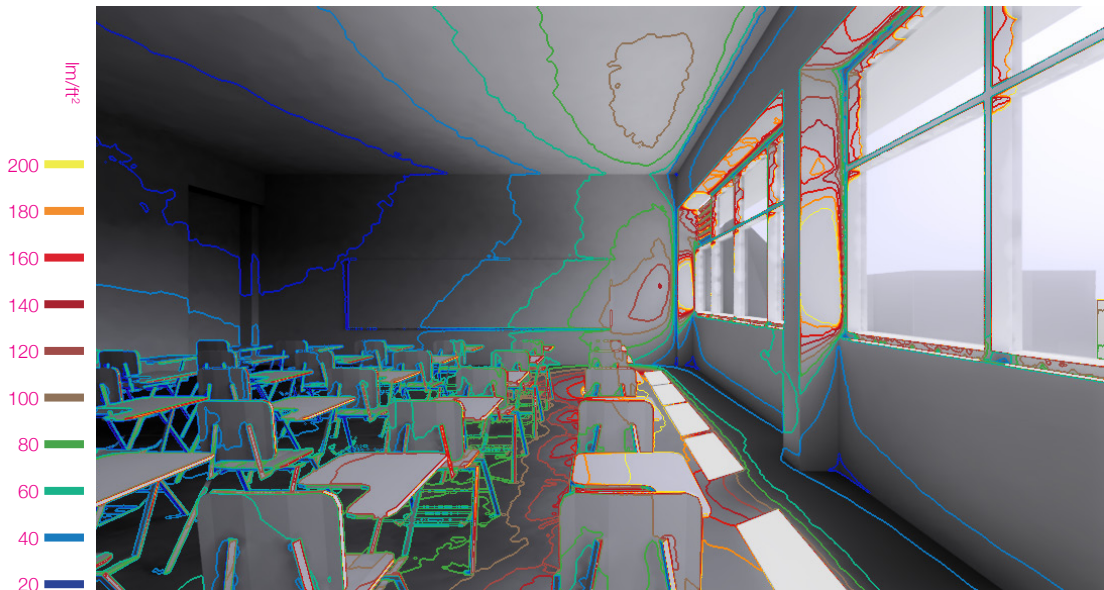
Typical Sunny Sky March 2 pm

Add/B. 4.4 Falsecolor Luminance:: Typical Classroom Facing West (Continued)

The illuminance levels are shown as contour lines in perspective views. These contour lines show illuminance levels in footcandles, and as a contour map shows changes in elevation, these show changes in illuminance levels throughout the space. As opposed to luminance which measures surface brightness, illuminance measures how much light is falling on a surface.



Without shades



Typical Sunny Sky March 2 pm

[BLANK]

Add/C. HVAC AND THERMAL COMFORT STUDIES

1. EXECUTIVE SUMMARY

To understand occupant comfort, we initially assume there are no HVAC systems and study only the passive ability of the building to provide comfort. These models predict the number of occupied hours that occupants will feel comfortable without mechanical conditioning (HVAC autonomy).

Human comfort depends on a host of conditions. In this study, occupant comfort is calculated as defined by the ASHRAE 55 Adaptive Thermal Comfort Standard. Indoor operative temperatures range between 65.8°F - 86.1°F (18.78°C - 30.1°C). This assumes that occupants will wear clothing appropriate to the weather. Furthermore, air movement is assumed to be less than 40 fpm, as this is the threshold for comfort cooling due to air movement.

We use two typical south facing classrooms as the base case, and assume the most basic usual envelope for existing buildings on campus. Observing the comfort load factors for each space, we determined the priorities to improve thermal comfort which include increasing natural ventilation, reducing internal heat from lighting, reducing the heat gain or loss through glazing areas, and increasing the thermal mass effect. From these, we could identify how much comfort can be improved relying only on passive strategies and building design decisions. By parametrically modeling envelope improvements in an Additive fashion we could quantify the relative effect of each measure.

In summary, the factors associated with decreased comfort in this analysis are the solar radiation through the windows and internal loads (heat released to the space by the occupants as well as from lighting and equipment).

The analysis also indicates that ventilation and thermal mass (interior floor and wall conduction) improve building thermal performance and thus improving comfort and reducing future HVAC loads. Ventilation introducing outside air when heat is building up in the space due to high internal loads or solar radiation, can prevent overheating. Thermal mass in the floor, such as a concrete slab contributes to comfortable

Add/C.1 HVAC and Thermal Comfort Studies:: Executive Summary (Continued)

conditions by absorbing heat during the day and releasing it at night.

We identified a series of customized suite of improvements that directly Address the potential for overheating and correspond to typical UHM retrofit project scopes, including future deferred maintenance projects on the UHM campus. These suite models were then run for each orientation and then for offices and laboratories. The studies present the following cumulative scenarios:

- Typical Existing: Base case with assumptions for envelope features and internal loads usually found in existing campus buildings.
- Typical with Improved Windows: If a retrofit project is approved, window improvement opportunities should be considered by the design team in an effort to pursue holistic interventions that Achieve the largest performance benefits. These improvements include good glazing, exterior shading and window operability.
- Minimum Suite: reducing the internal loads by using efficient lighting and daylight controls is the most critical retrofit need in existing UHM buildings.
- Improved Suite: roofs are upgraded to fulfill the prescriptive IECC 2015 requirements.
- Code Suite: prescriptive IECC 2015 requirements for walls are also included. This suite represents the most ambitious and realistic retrofit interventions in existing buildings, affecting all exterior envelope surfaces and lighting loads.
- Ideal: these models represent ideal assumptions for new buildings, and include exposing thermal mass to all interior surfaces.
- Ideal with Smart Ventilation: these models assume that two Additional air changes per hour (ACH) are introduced as needed (either by natural ventilation or fan

Add/C.1 HVAC and Thermal Comfort Studies:: Executive Summary (Continued)

assistance) to the Ideal Suite described above.

In this executive summary, the results have been averaged for all four orientations, and summarized by building type. Tables describing the hours of overheating for both the whole year and occupied hours only, with and without ceiling fans are included. In Addition, hourly graphs representing degrees from comfort for the top floor spaces for all hours of the year are presented, summarizing graphically the effect of the improvement strategies. These results have been used to validate and inform the metrics included as requirements in the UHM Building Design and Performance Standards.

Observing the thermal comfort results, the main recommendations for classroom and offices are::

- Ceiling fans (to provide air motion) and operable windows are critical (as they allow the adaptive comfort model and bring in 1ACH of outside air beyond breathing requirements).
- For all orientations, good glazing and shading, in Addition to efficient lighting with controls (both occupancy and daylight) should be part of every retrofit project, if possible.
- New buildings should be designed to include as much thermal mass and ventilation as possible (ideally, to achieve 2 or 3 ACH minimum).
- Design teams that do not have the capacity to replicate the studies presented in this section are encouraged to include the model assumptions that Achieve the highest building performance results as part of the specifications for their projects (prescriptive recommendations in the UHM BDP Standards).

Even if laboratory buildings do not have the same potential to be passively conditioned as the other building types, introducing the envelope improvements and reductions in internal loads would still have a significant impact on building performance.

This Addendum also includes the detailed results from every simulation, with graphs for operative temperatures and degrees from comfort for each hour of the year, cumulative bin summaries for comfort results and comfort load factors for both top and bottom floors, for each building type and orientation. Design teams are encouraged to selectively look at the results that are relevant to their project and provide their own

Add/C.1 HVAC and Thermal Comfort Studies:: Executive Summary (Continued)

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Add/C.1 HVAC and Thermal Comfort Studies:: Executive Summary (Continued)**a. Thermal Comfort and HVAC Autonomy:: Classroom Results**

On average, for all orientations, classrooms in existing UHM buildings (Typical Existing) need HVAC conditioning during all occupied hours. By improving the windows, bringing in a minimum amount of outside air (1ACH) and installing ceiling fans (Typical with Window Improvements), occupants in these spaces would feel too warm during 49% of the time in floors with no roof exposure and 68% in the top floors.

Controlling the time the lights are on and effectively reducing the lighting loads during daytime hours, in Addition to the strategies mentioned above (Minimum Suite), improves comfort conditions so that these spaces would only need HVAC conditioning during 26% of the occupied times on average for both floors.

Adding IECC 2015 prescriptive requirements for the roof (Improved Suite), improves comfort conditions in the top floor so that and HVAC system would be needed during 20% of the occupied hours. Similarly, upgrading the walls to IECC 2015 prescriptive requirements (Code Suite), would make the lower classrooms and the classrooms on the top floors need HVAC conditioning during 21% and 15% of the occupied time respectively.

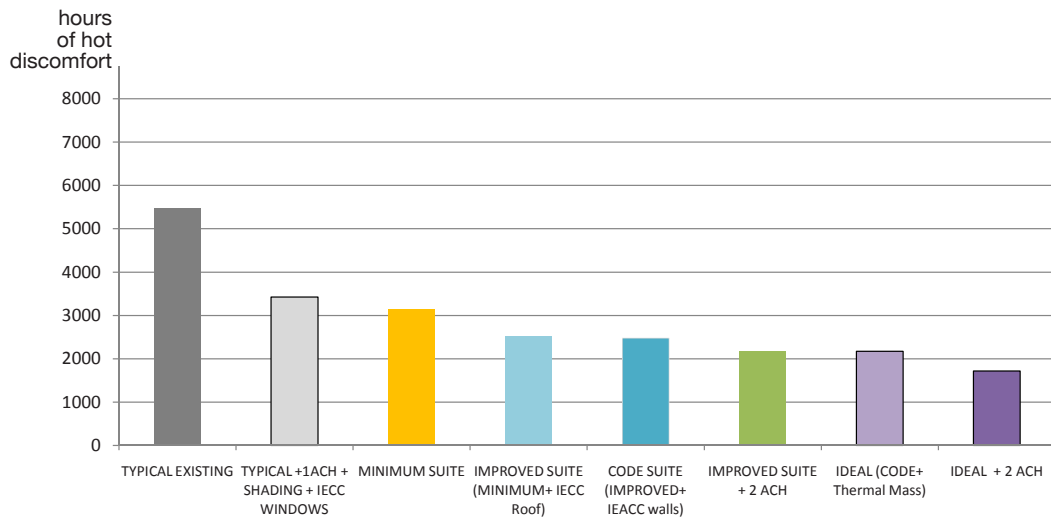
Exposed thermal mass in all interior surfaces (Ideal Suite) would reduce the need for HVAC conditioning to 7% of the occupied hours in both spaces, or 5% if Additional outside air is introduced to the classrooms. This essentially means that, in this climate, the HVAC system only needs to be available during extreme heat wave periods in buildings with the features considered in these studies.

It is important to note that if ceiling fans are not installed, only the well insulated spaces with thermal mass and increased ventilation (Ideal Suite) would reduce hot discomfort and the need for HVAC conditioning beyond 77% of the occupied hours.

Also, as described in the weather data analysis section of this Addendum, these models were run using TMY3 data, which deliberately avoids extreme conditions. In order to evaluate the validity of this study under more severe weather conditions, such as the periods of high humidity, high temperature and very low wind speeds (August 2015) that are expected to increase in frequency due to climate change,

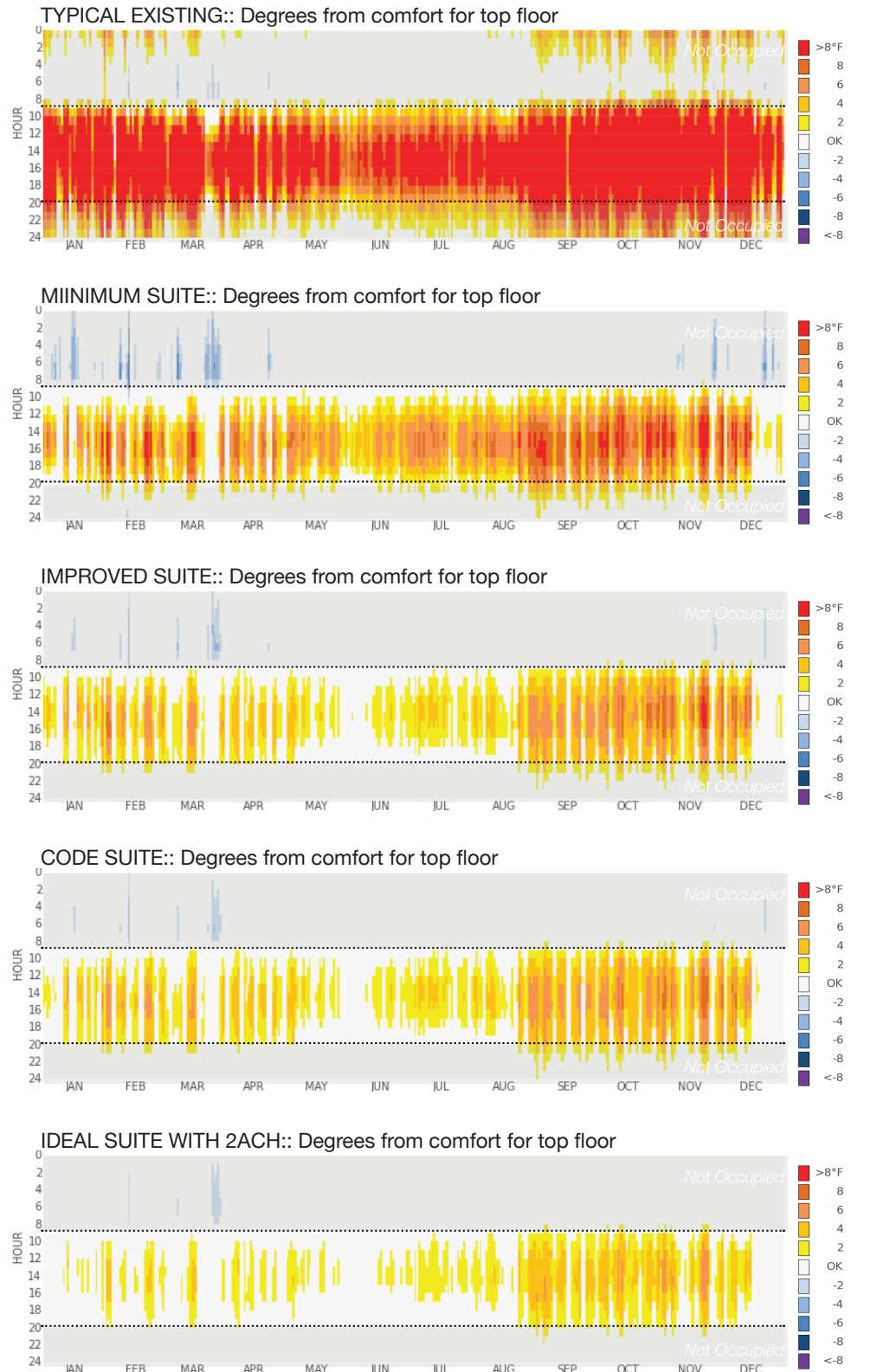
Add/C.1 HVAC and Thermal Comfort Studies:: Executive Summary (Continued)

CLASSROOM RESULTS:: SUMMARY



Scenario	Floor	Condition	Bottom Floor			Top Floor		
			hours	% of the whole year	% of occupied time	hours	% of the whole year	% of occupied time
TYPICAL EXISTING		too warm	5943	68%	100%	5490	63%	100%
		w/ ceiling fans	4353.3	50%	100%	4070	48%	100%
A-3 TYPICAL +1ACH + SHADING + IECC WINDOWS		too warm	3059.5	35%	100%	3422	39%	100%
		w/ ceiling fans	1323.3	15%	49%	1847	21%	68%
B-3 MINIMUM SUITE		too warm	2615.3	30%	97%	3144	36%	100%
		w/ ceiling fans	673	8%	25%	726	8%	27%
C-1 IMPROVED SUITE (MINIMUM+ IECC Roof)		too warm	2561.8	29%	95%	2523	29%	93%
		w/ ceiling fans	690	8%	26%	534	6%	20%
C-2 CODE SUITE (IMPROVED+ IEACC walls)		too warm	2504.5	29%	93%	2473	28%	92%
		w/ ceiling fans	569	6%	21%	407	5%	15%
D-2 IMPROVED SUITE + 2 ACH		too warm	2207.3	25%	82%	2165	25%	80%
		w/ ceiling fans	464	5%	17%	327	4%	12%
E-1 IDEAL (CODE+ Thermal Mass)		too warm	2077.3	24%	77%	2171	25%	80%
		w/ ceiling fans	176	2%	7%	183	2%	7%
E-1 IDEAL + 2 ACH		too warm	1605.5	18%	59%	1717	20%	64%
		w/ ceiling fans	127	1%	5%	126	1%	5%

Add/C.1 HVAC and Thermal Comfort Studies:: Executive Summary (Continued)



Add/C.1 HVAC and Thermal Comfort Studies:: Executive Summary (Continued)

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Add/C.1 HVAC and Thermal Comfort Studies:: Executive Summary (Continued)***b. Thermal Comfort and HVAC Autonomy:: Office Results***

The main difference between classroom and office models is the internal load assumptions and ventilation rates. On the one hand, classroom spaces assume a much higher occupancy than the ASHRAE 90.1 assumptions for office spaces. However, ASHRAE 62.1 defines the requirements for minimum fresh air ventilation rates as the sum of a “per floor area” and a “per person” airflow rate. Thus, the more people in a space, the more fresh air is introduced in the model. As a consequence, office models show more discomfort hours (twice as many overall).

On average, for all orientations, offices in existing UHM buildings (Typical Existing) would need HVAC conditioning during all the occupied hours. By improving the windows, bringing in a minimum amount of outside air (1ACH) and installing ceiling fans (Typical with Window Improvements), occupants in these spaces would feel uncomfortable during 86% of the time in floors with no roof exposure and but still feel too warm during all occupied hours in the top floors.

Controlling the time the lights are on and effectively reducing the lighting loads during daytime hours, in Addition to the strategies mentioned above (Minimum Suite), improves comfort conditions so that these spaces would only need HVAC conditioning during 43% of the occupied times on lower floors and 83% in upper floors.

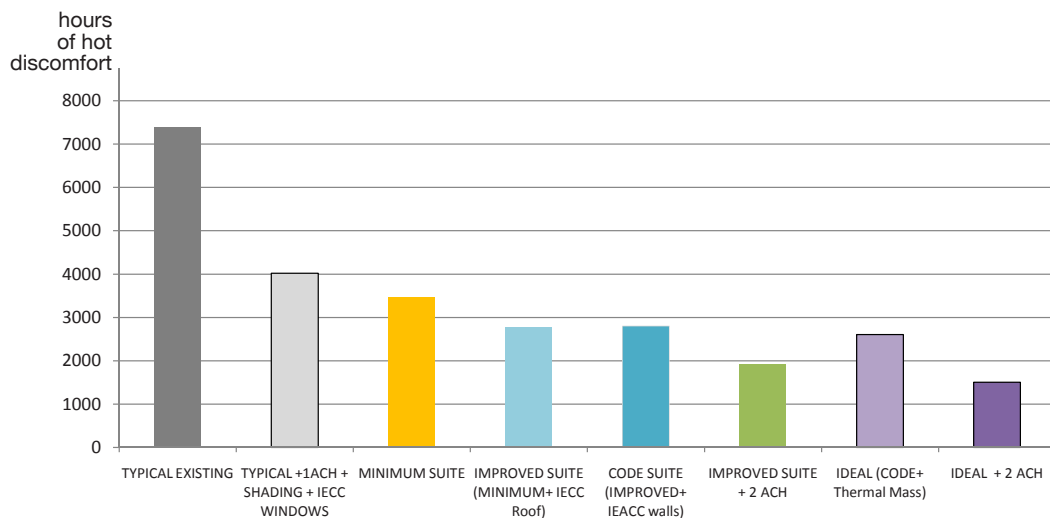
Adding IECC 2015 prescriptive requirements for the roof (Improved Suite), improves comfort conditions in the top floor so that and HVAC system would be needed during 37% of the occupied hours (making the interior conditions much more similar to ones in the lower floors). Similarly, upgrading the walls to IECC 2015 prescriptive requirements (Code Suite), would make the lower classrooms and the classrooms on the top floors need HVAC conditioning during 34% and 29% of the occupied time respectively.

Exposed thermal mass in all interior surfaces (Ideal Suite) would reduce the need for HVAC conditioning to 18% of the occupied hours in both spaces. However, Adding more ventilation makes the office models perform more similarly to the classroom models, Achievingreducing the overheating hours to 4% of the occupied hours. This essentially means that, same as for the classroom spaces

Add/C.1 HVAC and Thermal Comfort Studies:: Executive Summary (Continued)

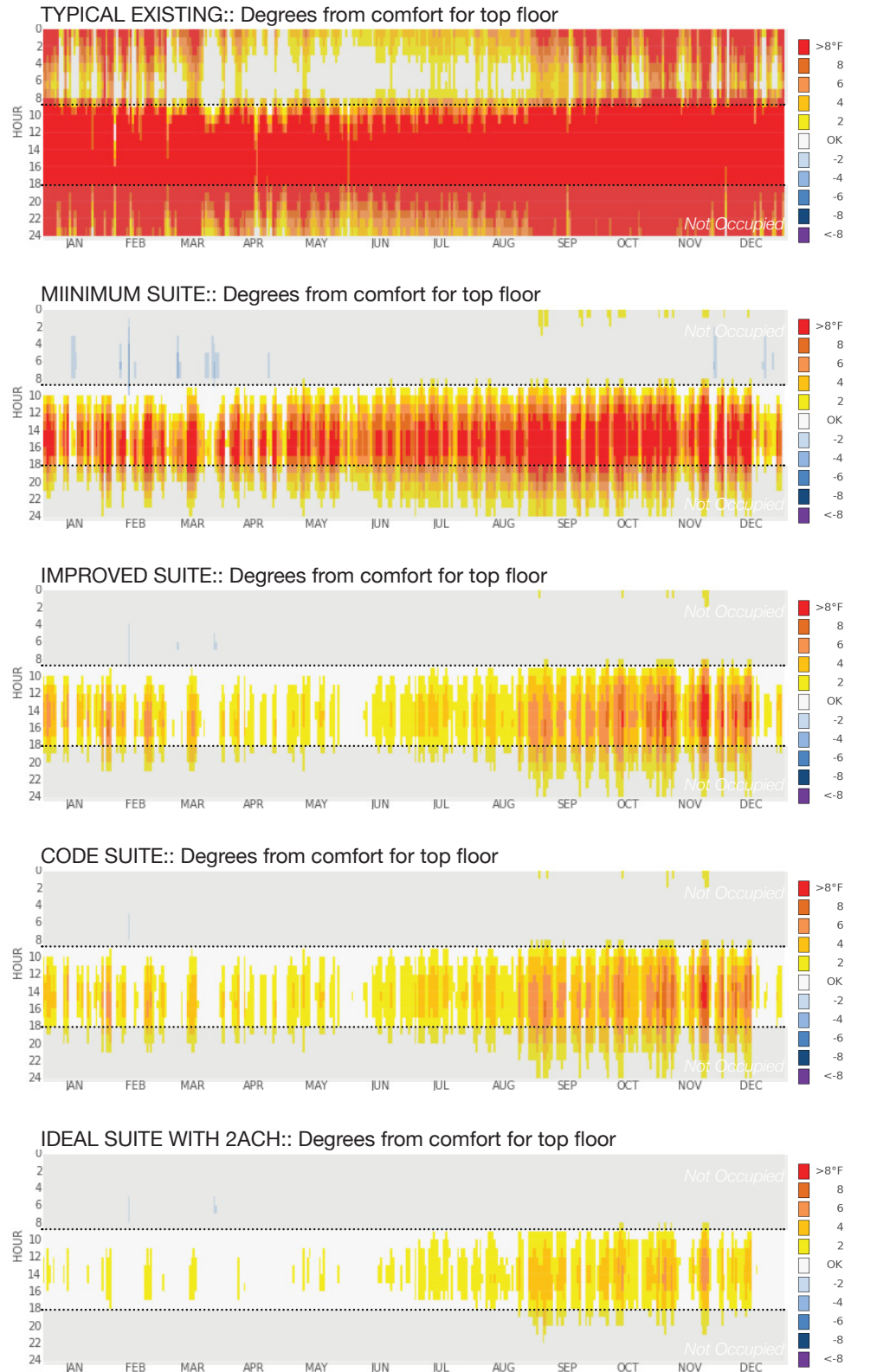
in this climate, the HVAC system only needs to be available during extreme heat wave periods in buildings with the features considered in these studies.

It is important to note that if ceiling fans are not installed, only the well insulated spaces with thermal mass and increased ventilation (Ideal Suite) would reduce hot discomfort and the need for HVAC conditioning during the occupied hours.



Scenario	Floor	Condition	Bottom Floor			Top Floor		
			hours	% of the whole year	% of occupied time	hours	% of the whole year	% of occupied time
TYPICAL EXISTING	Bottom Floor	too warm	7986.5	91%	100%	7393	84%	100%
		w/ ceiling fans	6865.3	78%	100%	6038	69%	100%
A-3 TYPICAL +1ACH + SHADING + IECC WINDOWS	Bottom Floor	too warm	3862.5	44%	100%	4020	46%	100%
		w/ ceiling fans	1750.3	20%	86%	2295	26%	100%
B-3 MINIMUM SUITE	Bottom Floor	too warm	2921	33%	100%	3460	39%	100%
		w/ ceiling fans	864	10%	43%	1681	19%	83%
C-1 IMPROVED SUITE (MINIMUM+ IECC Roof)	Bottom Floor	too warm	2759.3	31%	100%	2780	32%	100%
		w/ ceiling fans	832.5	10%	41%	757	9%	37%
C-2 CODE SUITE (IMPROVED+ IEACC walls)	Bottom Floor	too warm	2759.5	32%	100%	2799	32%	100%
		w/ ceiling fans	697	8%	34%	594	7%	29%
D-2 IMPROVED SUITE + 2 ACH	Bottom Floor	too warm	1911.5	22%	94%	1922	22%	95%
		w/ ceiling fans	360	4%	18%	291	3%	14%
E-1 IDEAL (CODE+ Thermal Mass)	Bottom Floor	too warm	2475.8	28%	100%	2607	30%	100%
		w/ ceiling fans	362	4%	18%	372	4%	18%
E-1 IDEAL + 2 ACH	Bottom Floor	too warm	1364.8	16%	67%	1504	17%	74%
		w/ ceiling fans	73	1%	4%	77.8	1%	4%

Add/C.1 HVAC and Thermal Comfort Studies:: Executive Summary (Continued)



Add/C.1 HVAC and Thermal Comfort Studies:: Executive Summary (Continued)

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Add/C.1 HVAC and Thermal Comfort Studies:: Executive Summary (Continued)***c. Thermal Comfort and HVAC Autonomy:: Laboratory Results***

Laboratories operate in a tighter range of acceptable interior conditions, which requires controlling and potentially conditioning the air that comes into the building whenever the outdoor conditions do not fall within that acceptable range. In Addition, the internal loads in laboratory spaces are significantly higher than in other building types, especially for equipment but also for lighting. As described in the Labs 21 Best Practices guidelines, zoning the equipment efficiently is a good way to reduce the impact of the heat released from laboratory equipment on the interior conditions and thus the HVAC energy use. Also, a careful design of the ventilation rates, adapting them to differences in interior conditions and occupancy, provides the most benefits in terms of overall laboratory building performance.

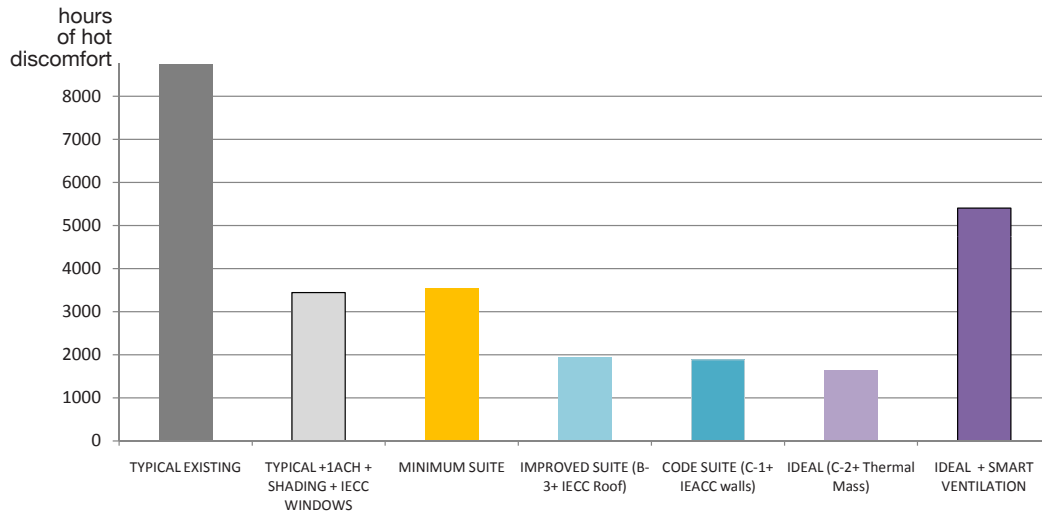
Our results confirm that laboratories need HVAC conditioning during all occupied hours, independently of the envelope improvements introduced in the building. Not only that, ceiling fans do not provide the advantages noticed in other building types, and the adaptive comfort model is not applicable in these spaces.

However, even if thermal comfort and HVAC autonomy are not as critical as for other building types, these parametric studies were repeated with an HVAC conditioning system to predict total building energy use. These results show that envelope improvements have a measurable impact on optimizing building energy performance.

In the hourly graphs showing the degrees from comfort over the year for each suite model, we observe that with controlling the internal loads, improving the windows (shading+glazing) and bringing in more air than just the breathing requirements (Minimum Suite), interior conditions during the unoccupied times are widely improved. Furthermore the results from the model with IECC 2015 prescriptive envelope, thermal mass and smart ventilation (which means half as low ventilation rates during occupied hours and four times lower rates during unoccupied hours) show that even if the amount of overheating **hours** increases compared to the other models with higher constant ventilation rates, the **conditions** are not as extreme. This means that the space would be able to be conditioned with a significantly smaller HVAC system.

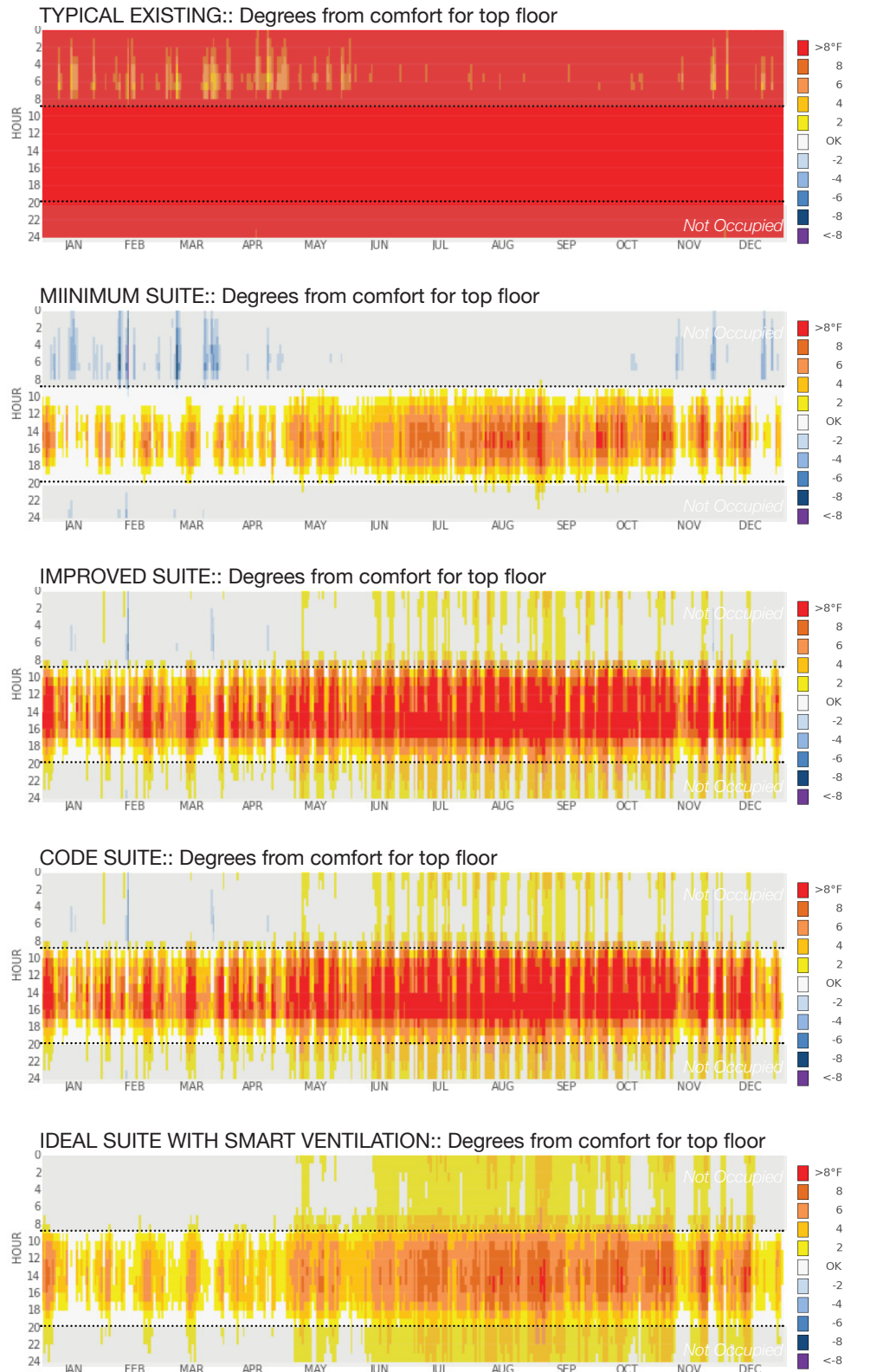
Add/C.1 HVAC and Thermal Comfort Studies:: Executive Summary (Continued)

LABORATORY RESULTS:: SUMMARY



Scenario	Status	Bottom Floor			Top Floor		
		hours	% of the whole year	% of occupied time	hours	% of the whole year	% of occupied time
TYPICAL EXISTING	too warm	8758	100%	100%	8739	100%	100%
A-3 TYPICAL +1ACH + SHADING + IECC WINDOWS	too warm	3262.5	37%	100%	3443	39%	100%
B-3 MINIMUM SUITE	too warm	1996.5	23%	100%	3538	40%	100%
C-1 IMPROVED SUITE (MINIMUM+ IECC Roof)	too warm	1972.5	23%	100%	1950	22%	100%
C-2 CODE SUITE (IMPROVED+ IEACC walls)	too warm	1891.5	22%	100%	1885	22%	100%
E-1 IDEAL (CODE+ Thermal Mass)	too warm	1556	18%	100%	1639	19%	100%
E-2 IDEAL + SMART VENTILATION	too warm	5380	61%	100%	5406	62%	100%

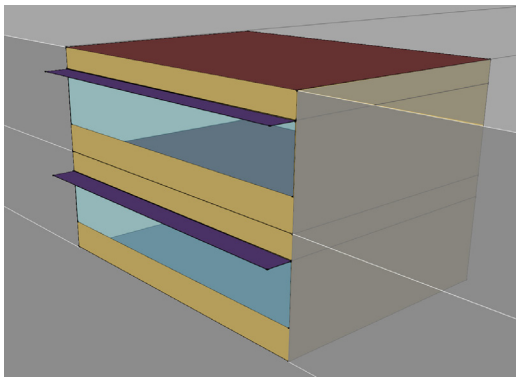
Add/C.1 HVAC and Thermal Comfort Studies:: Executive Summary (Continued)



Add/C. HVAC AND THERMAL COMFORT STUDIES**2. MODEL ASSUMPTIONS**

We modeled the building using EnergyPlus, a research-grade simulation platform that accounts for sub-hourly building envelope heat flows through conduction, convection, and radiation. The model contains envelope geometry, shading devices (overhangs), and orientation, as well as assumptions about ventilation strategy, construction assemblies, and internal gains. Typical meteorological year (TMY) weather data for Honolulu International Airport (the closest representative data set), were used for the analysis.

The analysis consisted of annual hour-by-hour simulations using the EnergyPlus software to identify the potential strategies to improve the energy performance of a typical existing classroom. The geometry and classroom layout was based on rooms 302 and 402 currently located in Kuykendall Hall. They represent classroom units within a larger building, located on the third floor and the fourth floor, to understand the impact of roof exposure, and with adiabatic interior walls. Window sizes were modified according to the findings and recommendations from the daylighting models to maximize interior lighting levels. Internal loads based on a medium sized classroom according to the UHM Space Planning guidelines were considered. In terms of schedules, an 8am to 8pm occupancy was modeled, with light power density and receptacle use per ASHRAE 90.1 Appendix G. We also modeled that the building provides fresh air for breathing as required per code.



Weather file::

Honolulu International Airport (USA_HI_Honolulu.Intl.AP.911820_TMY3.epw), IECC climate zone 1A

All models: 50% Window to wall Ratio, as per daylighting model recommendations to maximize interior lighting levels.

Typical Models: No insulation in opaque envelope: walls (assembly $U=0.410$ Btu/h-ft²-F), roof (assembly $U=0.393$ Btu/h-ft²-F). Single pane windows ($U= 1.017$, $SHGC=0.819$, $VT=0.881$). No shading (exterior or interior). Interior walls: (1) 5/8" gypsum board.

Add/C.2 Model Assumptions (Continued)

Alternative Construction assemblies::

IECC Roof:: Coolroof: Three-year aged solar reflectance 0.55, thermal emittance 0.75, SRI 64,

U= 0.048 Btu/h-ft²-F (insulation entirely above roof deck)

IECC Exterior Walls:: (wood framed) U= 0.064 Btu/h-ft²-F

Thermal Mass Interior Walls:: Two 5/8" Gypsum boards on each side, Exposed Concrete Floor (Heavyweight concrete)

Shading:: According to daylight model results for each orientation:: 65 degree profile angle (3') for South, East, West Orientations, 75 (2') for North

IECC Windows:: U-Factor: 0.65 (operable), SHGC: 0.27, Tvis: 0.64 (LSG -Light to solar gain: 2.37)

Maximum air leakage rate 0.20 cfm/ft²

Internal Loads::

Occupancy:: Classrooms : 42 people, M-F 8am to 8pm

Office 275 sqft/person (ASHRAE 90.1, Appendix G), M-F 8am to 6pm

Labs, 275 sqft/person (ASHRAE 90.1, Appendix G), schedule per Labs 21

Modeling guidelines.

Equipment:: ASHRAE 90.1 Receptacle Loads: Classrooms : 0.5 W/sqft ,

Office 0.75 W/sqft,

Labs: 10W/sqft

Lighting:: IECC max LPD: Classrooms 1.24 W/sqft ,

Offices: 0.98 W/sqft (open office),

Laboratory 1.43 W/sqft (laboratory-classroom),

Ventilation:: per ASHRAE 62.1::

Lecture classroom: 7.5 cfm/person + 0.06 cfm/sqft

Office: 5 cfm/person + 0.06 cfm/sqft

University laboratories: 10 cfm/person + 0.18 cfm/sqft

Infiltration:: 0.004 cfm/ft² exterior wall (maximum allowed per IECC)

Add/C.2 Model Assumptions (Continued)

Alternative Internal Load Assumptions:

Additional 1ACH corresponds to assuming that windows are operable and bring in outdoor air if needed (when it gets too warm inside (from 74°F) and the Outdoor Temperature is cooler than the interior temperature)

University laboratories: 10 cfm/person + 2 cfm/sqft (equivalent to 13ACH) as described as usual ventilation rates in Labs 21 Modeling guidelines.

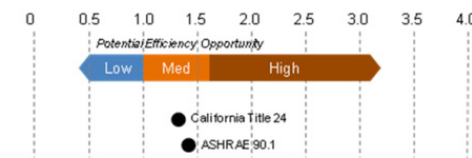
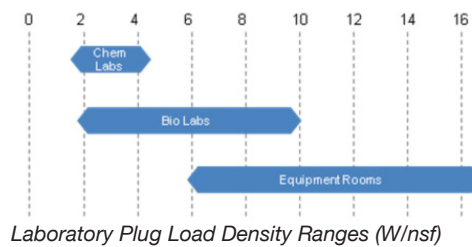
Smart Lab Ventilation:: 4ACH when unoccupied, 6ACH when occupied (as per LBNL self-benchmarking tool)

Lower LPD (see Add/E Efficient Lighting Examples)::

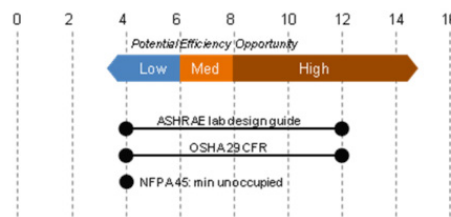
- Classrooms 0.6 W/sqft,
- Offices 0.6 W/sqft,
- Labs 1 W/sqft.

Daylight sensors to continuously dim lights down to 15% when 30Fc on workplane.

Efficient Laboratory Equipment: 6W/sqft (average biolabs plug load intensity as per LBNL self-benchmarking tool)



Laboratory Lighting Installed Power Density ranges (W/nsf)



Minimum Air Change Rate (ACH) Ranges in source: LBNL self-benchmarking tool

Add/C. HVAC AND THERMAL COMFORT STUDIES**3. CLASSROOM ANALYSIS**

The following is a list of the models that were part of this analysis:

a. SOUTH FACING CLASSROOM

0. **TYPICAL EXISTING**:: No Insulation in Opaque Surfaces, Single Pane Glass Windows

A- Window Parametrics

A-1. TYPICAL + 1ACH (Operable Windows)

A-2. TYPICAL + 1ACH + Shading

A-3. TYPICAL + 1ACH + Shading + IECC Glazing

B. Internal Load Parametrics (Lighting)

B.1. TYPICAL + 1ACH + IECC Glazing + Shading + lower LPD

B.2. TYPICAL + 1ACH + IECC Glazing + Shading + Daylight controls

B.3. **MINIMUM SUITE** :: TYPICAL + 1ACH + IECC Glazing + Shading + lower LPD
+ daylight controls

C. Exterior Surface Parametrics

C.1. **IMPROVED SUITE**:: Minimum Suite + IECC Roof

C.2 **CODE SUITE**:: Improved Suite + IECC Walls

D. Ventilation Parametrics::

D.1 MINIMUM SUITE + 2ACH

D.2 IMPROVED SUITE + 2ACH

D.3 CODE SUITE + 2ACH

D.4 MINIMUM SUITE + 3ACH

D.5 IMPROVED SUITE + 3ACH

D.6 CODE SUITE + 3ACH

E. Thermal Mass

E.1. **IDEAL SUITE**:: Code Suite + Thermal Mass

E.2 IDEAL SUITE + 2ACH

OTHER ORIENTATIONS (b. NORTH, c.EAST AND d. WEST)

0. **TYPICAL EXISTING**:: No Insulation in Opaque Surfaces, Single Pane Glass Windows

1. TYPICAL + 1ACH + Shading + IECC Glazing

2. **MINIMUM SUITE**

3. **IMPROVED SUITE**

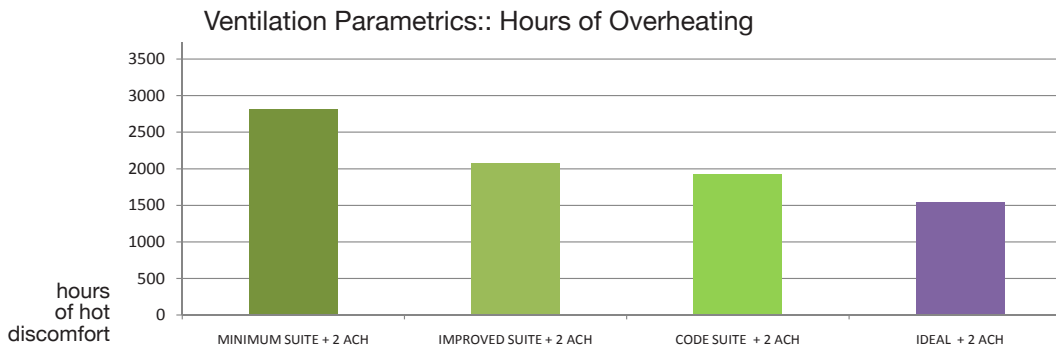
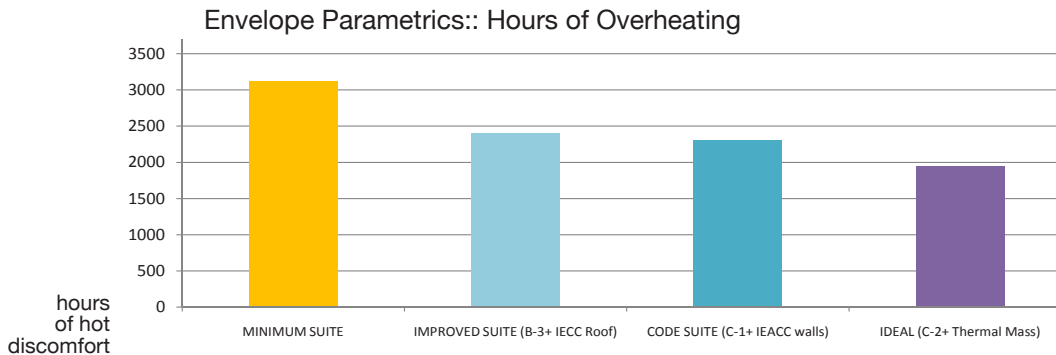
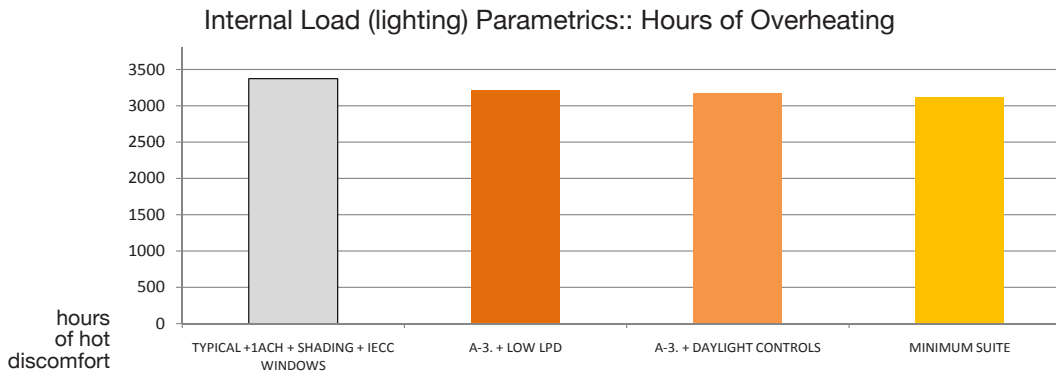
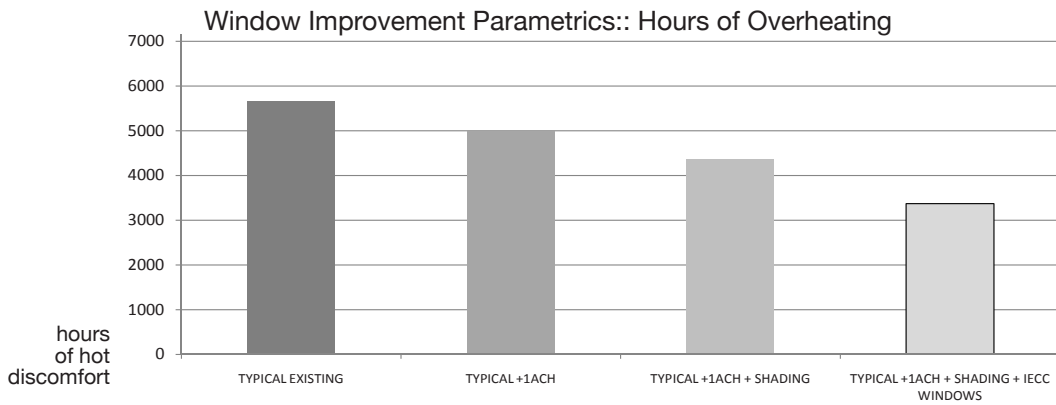
4. **CODE SUITE**

5. IMPROVED SUITE + 2ACH

6. **IDEAL SUITE**

7. IDEAL SUITE + 2ACH

Add/C.3 Classroom Analysis (Continued)



Add/C.3 Classroom Analysis (Continued)

Window Improvement Parametrics:: Summary of Results

		Bottom Floor			Top Floor		
		hours	% of the whole year	% of occupied time	hours	% of the whole year	% of occupied time
TYPICAL EXISTING	too warm	6118	70%	100%	5682	65%	100%
	w/ ceiling fans	4461	51%	100%	4203	48%	100%
A-1 TYPICAL +1ACH	too warm	5247	60%	100%	4981	57%	100%
	w/ ceiling fans	3629	41%	100%	3600	41%	100%
A-2 TYPICAL +1ACH + SHADING	too warm	4446	51%	100%	4368	50%	100%
	w/ ceiling fans	2692	31%	100%	2905	33%	100%
A-3 TYPICAL +1ACH + SHADING + IECC WINDOWS	too warm	2918	33%	100%	3373	39%	100%
	w/ ceiling fans	1249	14%	46%	1790	20%	66%

Internal Load (lighting) Parametrics:: Summary of Result

		Bottom Floor			Top Floor		
		hours	% of the whole year	% of occupied time	hours	% of the whole year	% of occupied time
A-3. + LOW LPD	too warm	2651	30%	98%	3218	37%	100%
	w/ ceiling fans	912	10%	34%	1515	17%	56%
A-3. + DAYLIGHT CONTROLS	too warm	2569	29%	95%	3188	36%	100%
	w/ ceiling fans	797	9%	30%	1446	17%	54%
MINIMUM SUITE	too warm	2461	28%	91%	3116	36%	100%
	w/ ceiling fans	675	8%	25%	1345	15%	50%

Envelope Parametrics:: Summary of Results

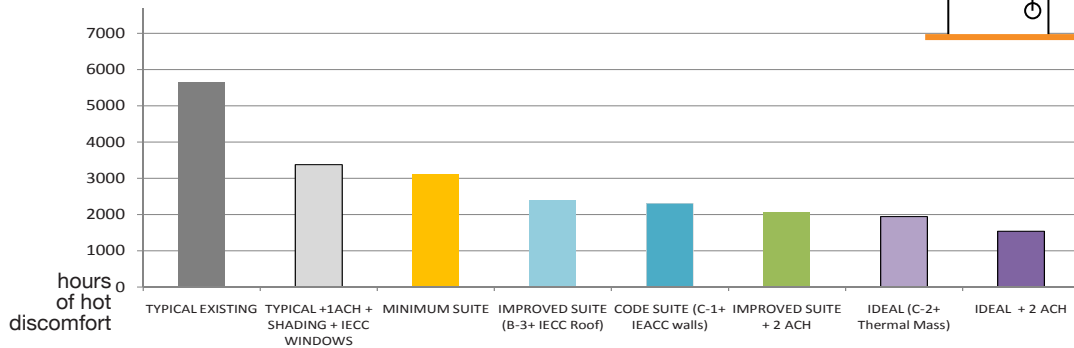
		Bottom Floor			Top Floor		
		hours	% of the whole year	% of occupied time	hours	% of the whole year	% of occupied time
IMPROVED SUITE (B-3+ IECC Roof)	too warm	2406	27%	89%	2402	27%	89%
	w/ ceiling fans	678	8%	25%	525	6%	19%
CODE SUITE (C-1+ IEACC walls)	too warm	2317	26%	86%	2306	26%	85%
	w/ ceiling fans	528	6%	20%	357	4%	13%
IDEAL (C-2+ Thermal Mass)	too warm	1850	21%	69%	1944	22%	72%
	w/ ceiling fans	149	2%	6%	146	2%	5%

Ventilation Parametrics:: Summary of Results

		Bottom Floor			Top Floor		
		hours	% of the whole year	% of occupied time	hours	% of the whole year	% of occupied time
MINIMUM SUITE + 2 ACH	too warm	2136	24%	79%	2817	32%	100%
	w/ ceiling fans	436	5%	16%	1083	12%	40%
IMPROVED SUITE + 2 ACH	too warm	2087	24%	77%	2068	24%	77%
	w/ ceiling fans	427	5%	16%	327	4%	12%
CODE SUITE + 2 ACH	too warm	1954	22%	72%	1918	22%	71%
	w/ ceiling fans	305	3%	11%	193	2%	7%
MINIMUM SUITE + 3 ACH	too warm	1905	22%	71%	2620	30%	97%
	w/ ceiling fans	309	4%	11%	902	10%	33%
IMPROVED SUITE + 3 ACH	too warm	1869	21%	69%	1821	21%	67%
	w/ ceiling fans	308	4%	11%	218	2%	8%
CODE SUITE + 3 ACH	too warm	1715	20%	64%	1665	19%	62%
	w/ ceiling fans	190	2%	7%	128	1%	5%
IDEAL + 2 ACH	too warm	1425	16%	53%	1536	18%	57%
	w/ ceiling fans	55	1%	2%	52	1%	2%

Add/C.3 Classroom Analysis (Continued)

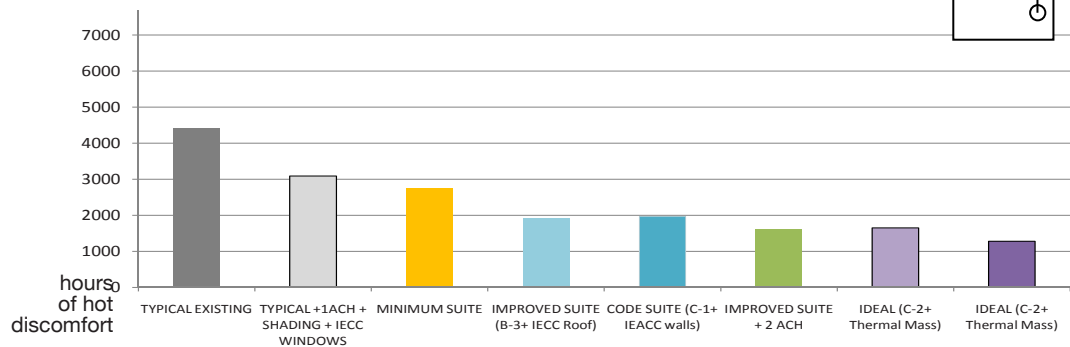
SOUTH FACING CLASSROOMS



Scenario	Bottom Floor				Top Floor			
	hours	% of the whole year	% of occupied time	hours	% of the whole year	% of occupied time		
TYPICAL EXISTING	too warm	6118	70%	100%	5662	65%	100%	
	w/ ceiling fans	4461	51%	100%	4203	48%	100%	
A-1 TYPICAL +1ACH	too warm	5247	60%	100%	4981	57%	100%	
	w/ ceiling fans	3629	41%	100%	3600	41%	100%	
A-2 TYPICAL +1ACH + SHADING	too warm	4446	51%	100%	4368	50%	100%	
	w/ ceiling fans	2692	31%	100%	2905	33%	100%	
A-3 TYPICAL +1ACH + SHADING + IECC WINDOWS	too warm	2918	33%	100%	3373	39%	100%	
	w/ ceiling fans	1249	14%	46%	1790	20%	66%	
B-1 A-3. + LOW LPD	too warm	2651	30%	98%	3218	37%	100%	
	w/ ceiling fans	912	10%	34%	1515	17%	56%	
B-2 A-3. + DAYLIGHT CONTROLS	too warm	2569	29%	95%	3168	36%	100%	
	w/ ceiling fans	797	9%	30%	1446	17%	54%	
B-3 MINIMUM SUITE	too warm	2461	28%	91%	3116	36%	100%	
	w/ ceiling fans	675	8%	25%	1345	15%	50%	
C-1 IMPROVED SUITE (B-3+ IECC Roof)	too warm	2406	27%	89%	2402	27%	89%	
	w/ ceiling fans	678	8%	25%	525	6%	19%	
C-2 CODE SUITE (C-1+ IEACC walls)	too warm	2317	26%	86%	2306	26%	85%	
	w/ ceiling fans	528	6%	20%	357	4%	13%	
D-1 MINIMUM SUITE + 2 ACH	too warm	2136	24%	79%	2817	32%	100%	
	w/ ceiling fans	436	5%	16%	1083	12%	40%	
D-2 IMPROVED SUITE + 2 ACH	too warm	2087	24%	77%	2068	24%	77%	
	w/ ceiling fans	427	5%	16%	327	4%	12%	
D-3 CODE SUITE + 2 ACH	too warm	1954	22%	72%	1918	22%	71%	
	w/ ceiling fans	305	3%	11%	193	2%	7%	
D-4 MINIMUM SUITE + 3 ACH	too warm	1905	22%	71%	2620	30%	97%	
	w/ ceiling fans	309	4%	11%	902	10%	33%	
D-5 IMPROVED SUITE + 3 ACH	too warm	1869	21%	69%	1821	21%	67%	
	w/ ceiling fans	308	4%	11%	218	2%	8%	
D-6 CODE SUITE + 3 ACH	too warm	1715	20%	64%	1665	19%	62%	
	w/ ceiling fans	190	2%	7%	128	1%	5%	
E-1 IDEAL (C-2+ Thermal Mass)	too warm	1850	21%	69%	1944	22%	72%	
	w/ ceiling fans	149	2%	6%	146	2%	5%	
E-2 IDEAL + 2 ACH	too warm	1425	16%	53%	1536	18%	57%	
	w/ ceiling fans	55	1%	2%	52	1%	2%	

Add/C.3 Classroom Analysis (Continued)

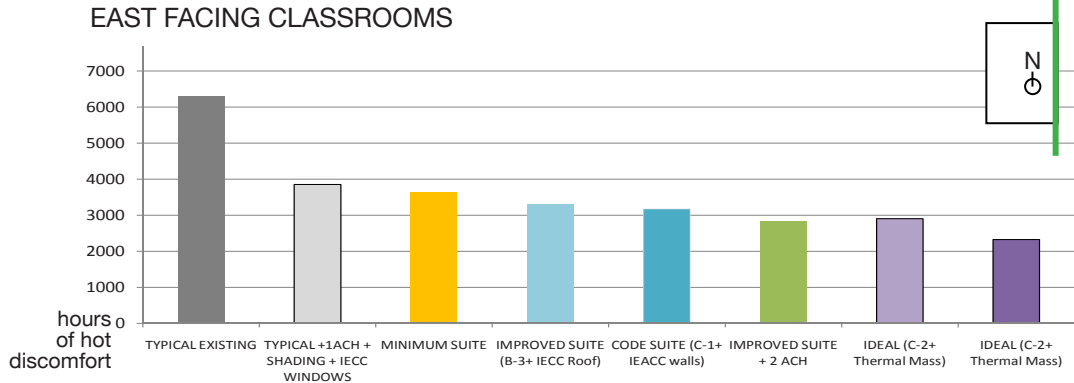
NORTH FACING CLASSROOMS



Scenario	Floor	too warm	w/ ceiling fans		
			hours	% of the whole year	% of occupied time
TYPICAL EXISTING	Bottom Floor	4566	52%	100%	
	Top Floor	4426	51%	100%	
TYPICAL +1ACH + SHADING + IECC WINDOWS	Bottom Floor	2941	34%	100%	
	Top Floor	2937	34%	100%	
A-3 TYPICAL +1ACH + SHADING + IECC WINDOWS	Bottom Floor	2599	30%	96%	
	Top Floor	3087	35%	100%	
B-3 MINIMUM SUITE	Bottom Floor	2057	23%	76%	
	Top Floor	2754	31%	100%	
C-1 IMPROVED SUITE (B-3+ IECC Roof)	Bottom Floor	1995	23%	74%	
	Top Floor	1909	22%	71%	
C-2 CODE SUITE (C-1+ IEACC walls)	Bottom Floor	2001	23%	74%	
	Top Floor	1966	22%	73%	
D-2 IMPROVED SUITE + 2 ACH	Bottom Floor	1671	19%	62%	
	Top Floor	1626	19%	60%	
E-1 IDEAL (C-2+ Thermal Mass)	Bottom Floor	1536	18%	57%	
	Top Floor	1650	19%	61%	
E-1 IDEAL + 2 ACH	Bottom Floor	1141	13%	42%	
	Top Floor	1282	15%	47%	

Add/C.3 Classroom Analysis (Continued)

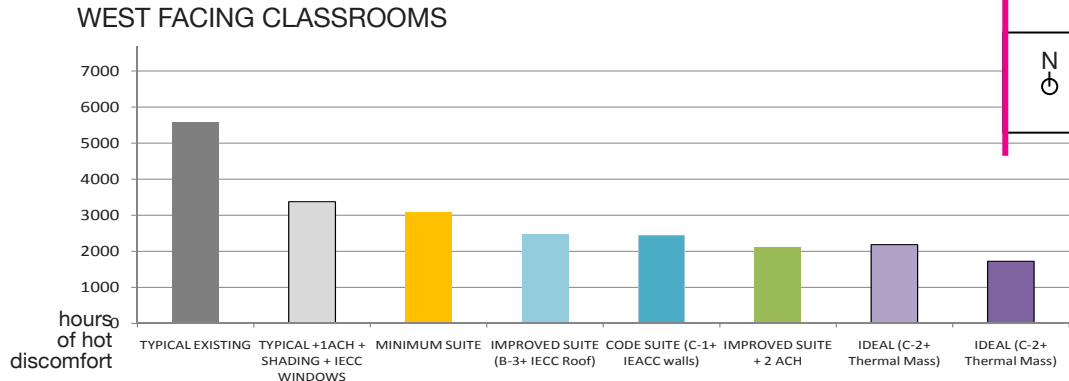
EAST FACING CLASSROOMS



Scenario	Floor	Condition	Bottom Floor			Top Floor		
			hours	% of the whole year	% of occupied time	hours	% of the whole year	% of occupied time
TYPICAL EXISTING		too warm	6858	78%	100%	6291	72%	100%
		w/ ceiling fans	5490	63%	100%	5017	57%	100%
A-3 TYPICAL +1ACH + SHADING + IECC WINDOWS		too warm	3673	42%	100%	2855	44%	100%
		w/ ceiling fans	1863	21%	70%	2270	26%	84%
B-3 MINIMUM SUITE		too warm	3374	39%	100%	3632	41%	100%
		w/ ceiling fans	1226	14%	45%	1799	21%	67%
C-1 IMPROVED SUITE (B-3+ IECC Roof)		too warm	3334	38%	100%	3293	38%	100%
		w/ ceiling fans	1226	14%	45%	991	11%	37%
C-2 CODE SUITE (C-1+ IEACC walls)		too warm	3239	37%	100%	3173	36%	100%
		w/ ceiling fans	962	11%	36%	718	8%	27%
D-2 IMPROVED SUITE + 2 ACH		too warm	2923	33%	100%	2845	32%	100%
		w/ ceiling fans	888	10%	33%	584	7%	22%
E-1 IDEAL (C-2+ Thermal Mass)		too warm	2872	33%	100%	2904	33%	100%
		w/ ceiling fans	333	4%	12%	338	4%	13%
E-1 IDEAL + 2 ACH		too warm	2267	26%	84%	2325	27%	86%
		w/ ceiling fans	350	4%	13%	346	4%	13%

Add/C.3 Classroom Analysis (Continued)

WEST FACING CLASSROOMS



Scenario	Floor	too warm	Bottom Floor		Top Floor		
			hours	% of the whole year	% of occupied time	hours	% of the whole year
TYPICAL EXISTING	Bottom Floor	6230	71%	100%	5580	64%	100%
	Top Floor	4521	52%	100%	4063	46%	100%
A-3 TYPICAL +1ACH + SHADING + IECC WINDOWS	Bottom Floor	3048	35%	100%	3373	39%	100%
	Top Floor	1273	15%	47%	1829	21%	68%
B-3 MINIMUM SUITE	Bottom Floor	2569	29%	95%	3074	35%	100%
	Top Floor	673	8%	25%	1398	16%	52%
C-1 IMPROVED SUITE (B-3+ IECC Roof)	Bottom Floor	2512	29%	93%	2487	28%	92%
	Top Floor	644	7%	24%	507	6%	19%
C-2 CODE SUITE (C-1+ IEACC walls)	Bottom Floor	2461	28%	91%	2446	28%	91%
	Top Floor	559	6%	21%	423	5%	16%
D-2 IMPROVED SUITE + 2 ACH	Bottom Floor	2148	25%	80%	2120	24%	79%
	Top Floor	444	5%	16%	339	4%	13%
E-1 IDEAL (C-2+ Thermal Mass)	Bottom Floor	2051	23%	76%	2187	25%	81%
	Top Floor	196	2%	7%	211	2%	8%
E-1 IDEAL + 2 ACH	Bottom Floor	1589	18%	59%	1726	20%	64%
	Top Floor	99	1%	4%	102	1%	4%

Add/C.3 CLASSROOM ANALYSIS:: SOUTH FACING

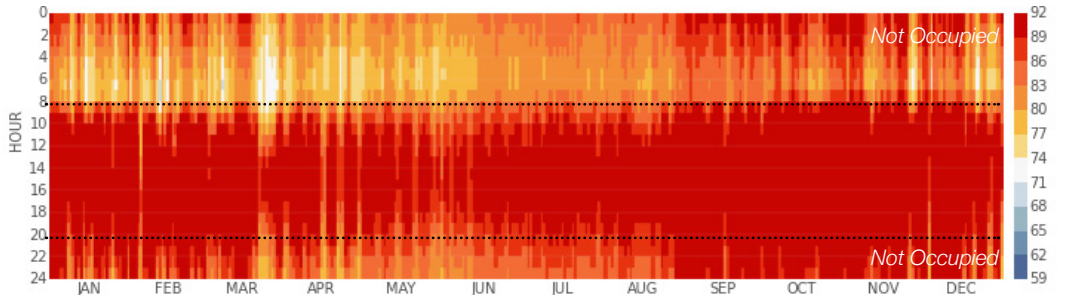
C.3.a.0. TYPICAL EXISTING



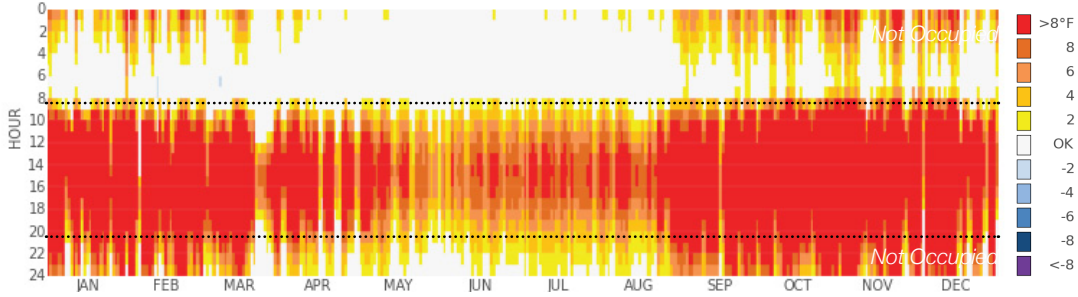
No Insulation in Opaque Surfaces and Single Pane Glass



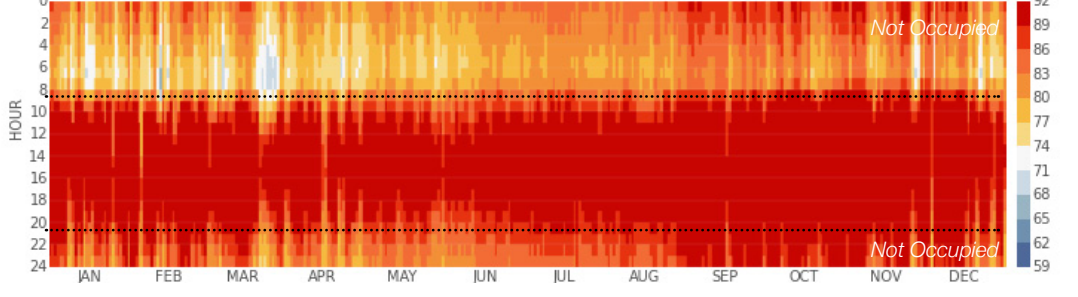
Operative Temperature for bottom floor



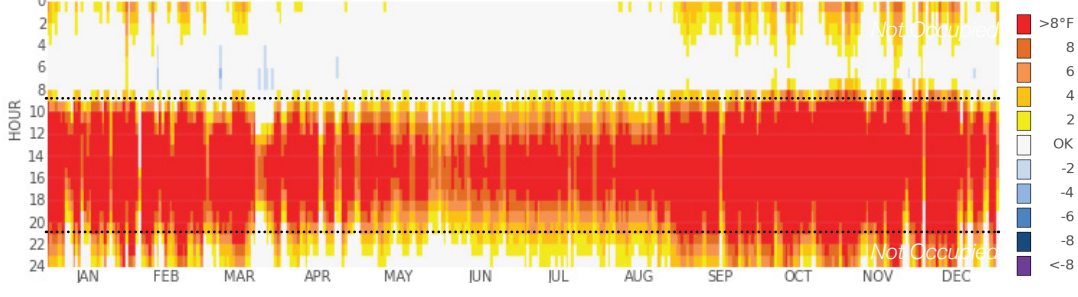
Degrees from comfort for bottom floor



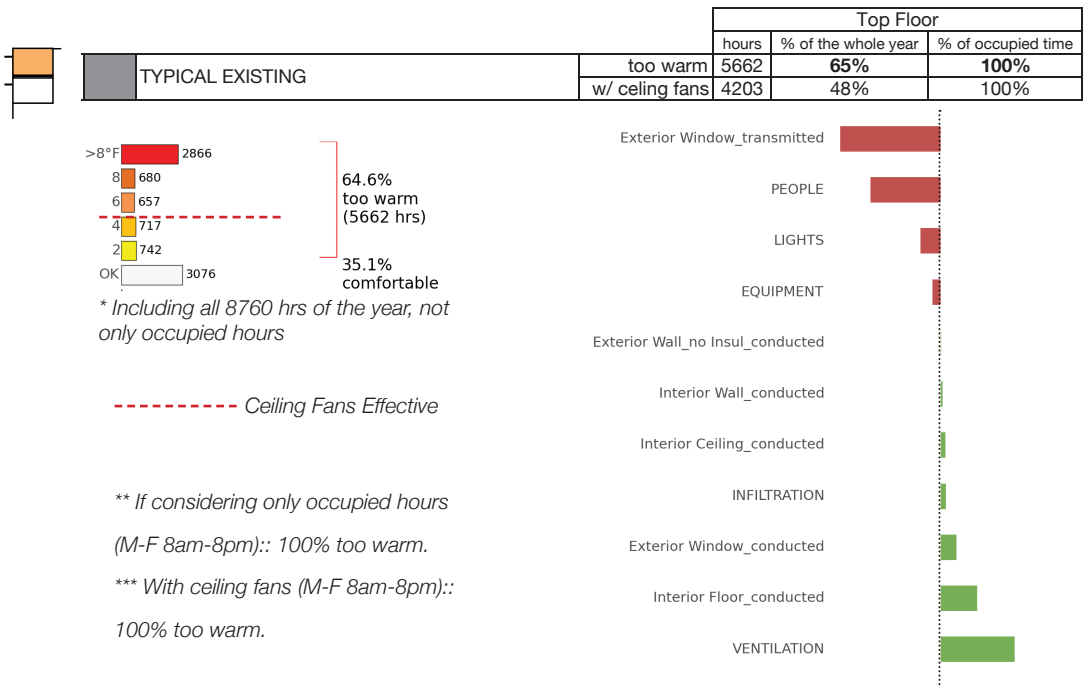
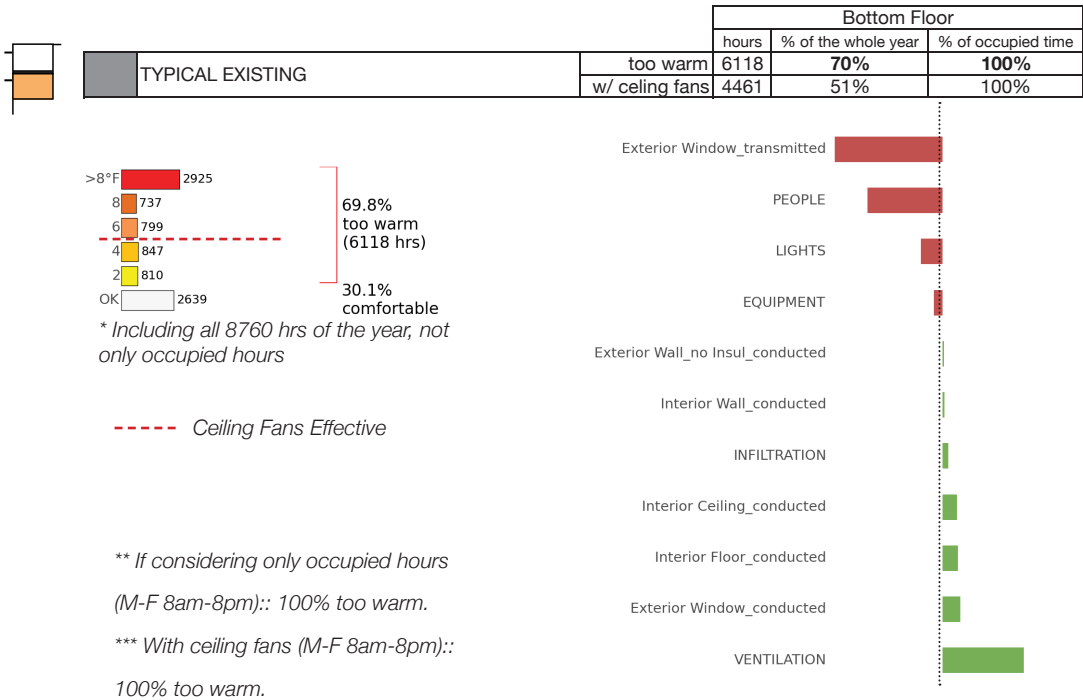
Operative Temperature for top floor



Degrees from comfort for top floor



Add/C.3.a.0 Classroom Analysis:: South Facing (Continued)

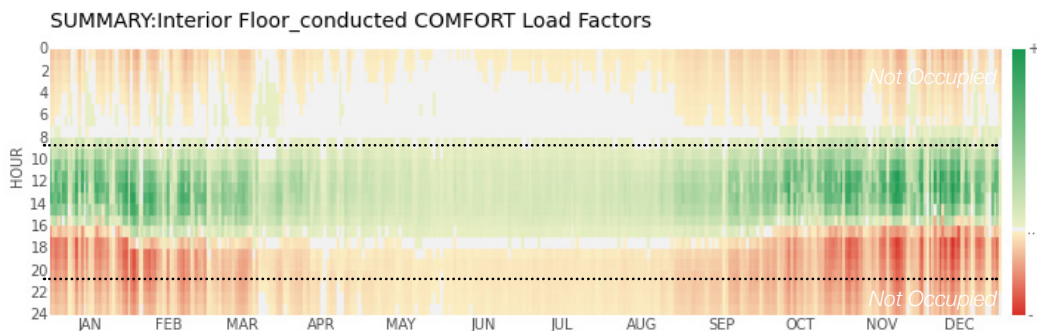
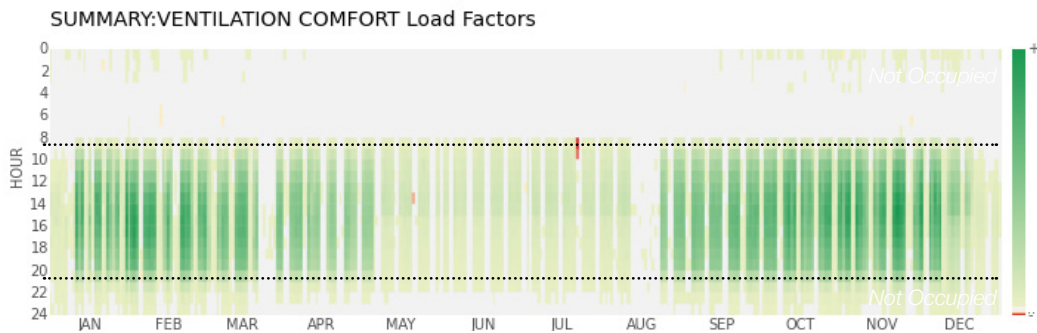
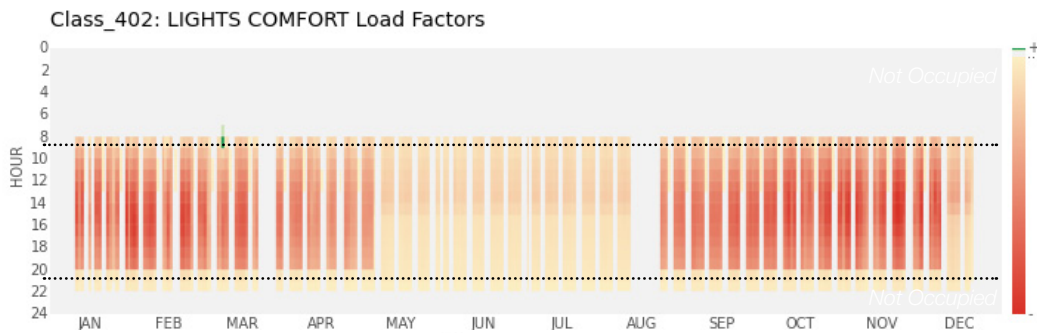
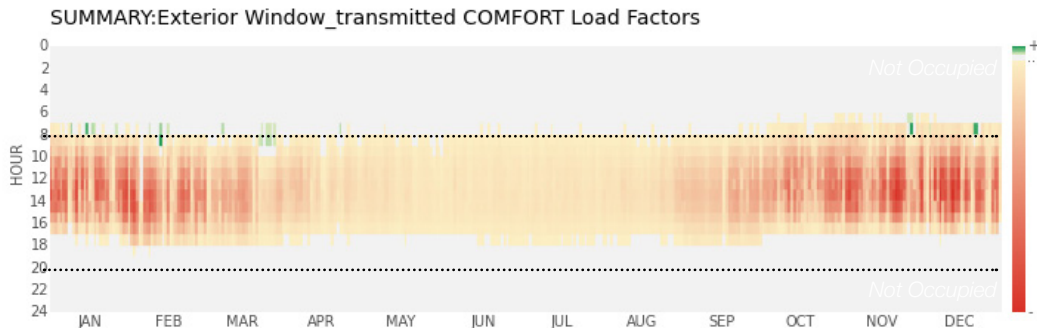


Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

C.3.a.0 TYPICAL EXISTING:: Comfort Load Factors



No Insulation in Opaque Surfaces and Single Pane Glass



Add/C.3.a.0 Classroom Analysis:: South Facing (Continued)

In order to provide a more fine grained analysis of comfort factors, we analyzed the heat flows into and out of the spaces, as well as the difference between the space temperatures and the ideal space temperature (adaptive comfort range). We compared these space loads to the ideal temperature difference to determine which loads are improving comfort and which loads are decreasing comfort. The comfort load factors indicate the degree to which a particular load is pushing the temperature of a space towards the middle of the comfort zone or away from it.

In summary, the factors associated with decreased comfort in this analysis are the solar radiation through the windows and the internal loads (heat released to the space by the occupants but also lighting and equipment).

This analysis also indicates that ventilation and thermal mass (interior floor and wall conduction) are improving building thermal performance and thus improving comfort and reducing future HVAC loads. Ventilation introducing outside air when heat is building up in the space due to high internal loads or solar radiation can prevent overheating. Thermal mass in the floor contributes to achieving comfort conditions by absorbing heat during the day and releasing it at night.

The graphs on the left show the times of the year when each load factor either decreases or increases comfort. For example, the solar transmitted radiation never increases comfort and decreases comfort the most during the fall and winter seasons, which is likely when the lower sun angles hit the windows for longer periods of time.

The internal heat coming from the lights always decreases comfort while ventilation always increases comfort. The interior floor increases comfort during most of the occupied times, even if it decreases comfort during the late afternoons. This is likely due to the floors not being able to absorb any more internal heat and starting to release it into the space even if that further increases the interior temperature.

Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

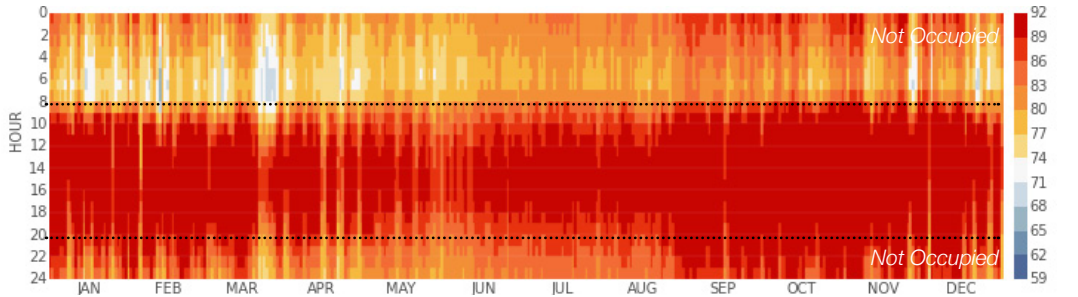
C.3.a.A. WINDOW PARAMETRICS



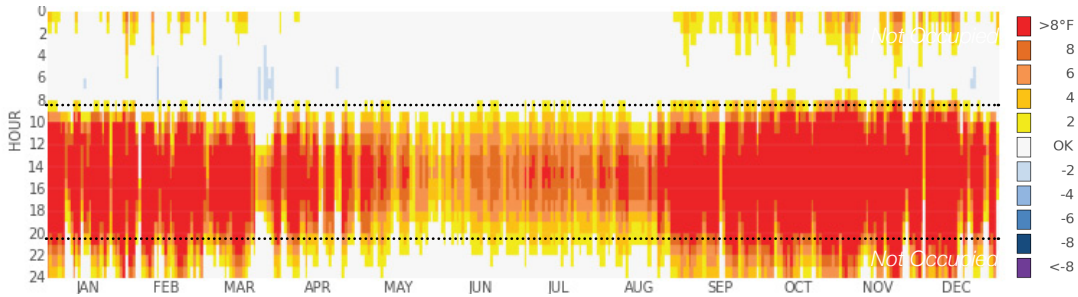
C.3.a. A.1 TYPICAL +1ACH (OPERABLE WINDOWS)



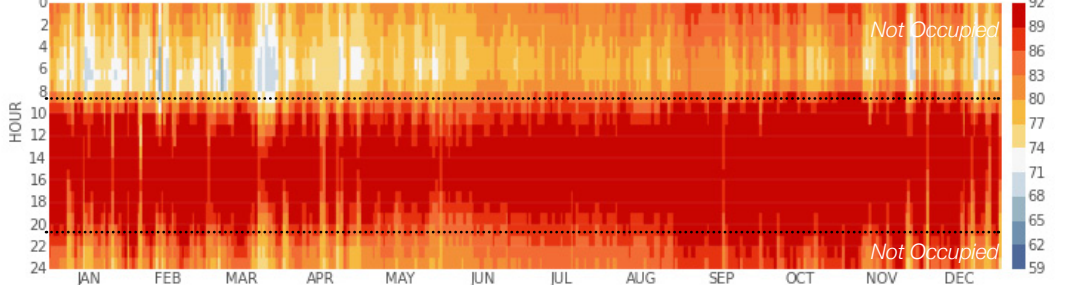
Operative temperature for bottom floor



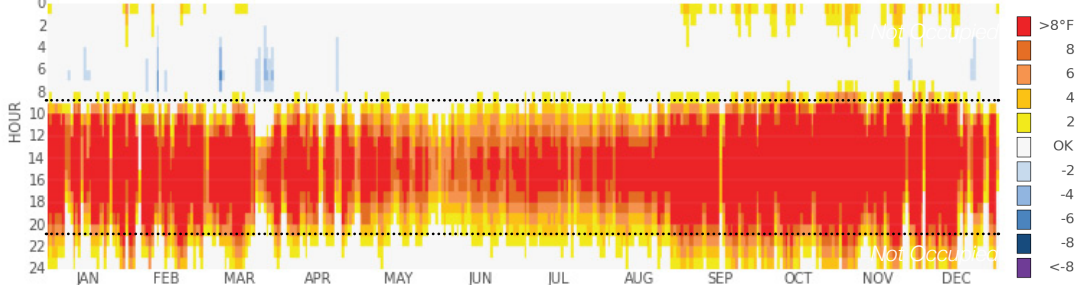
Degrees from comfort for bottom floor



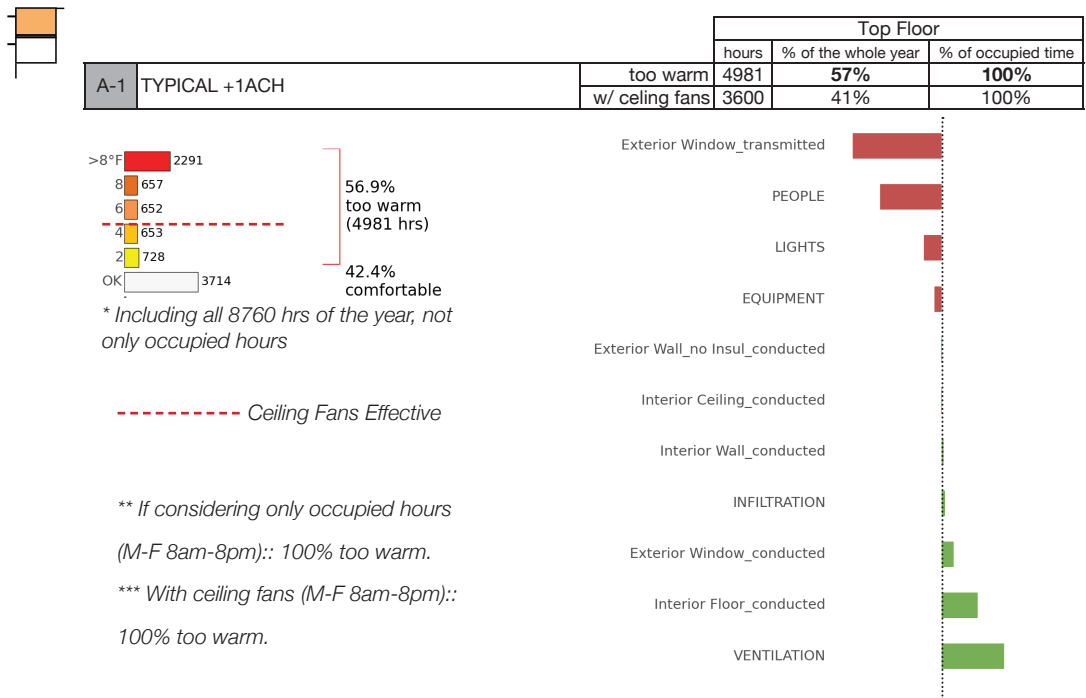
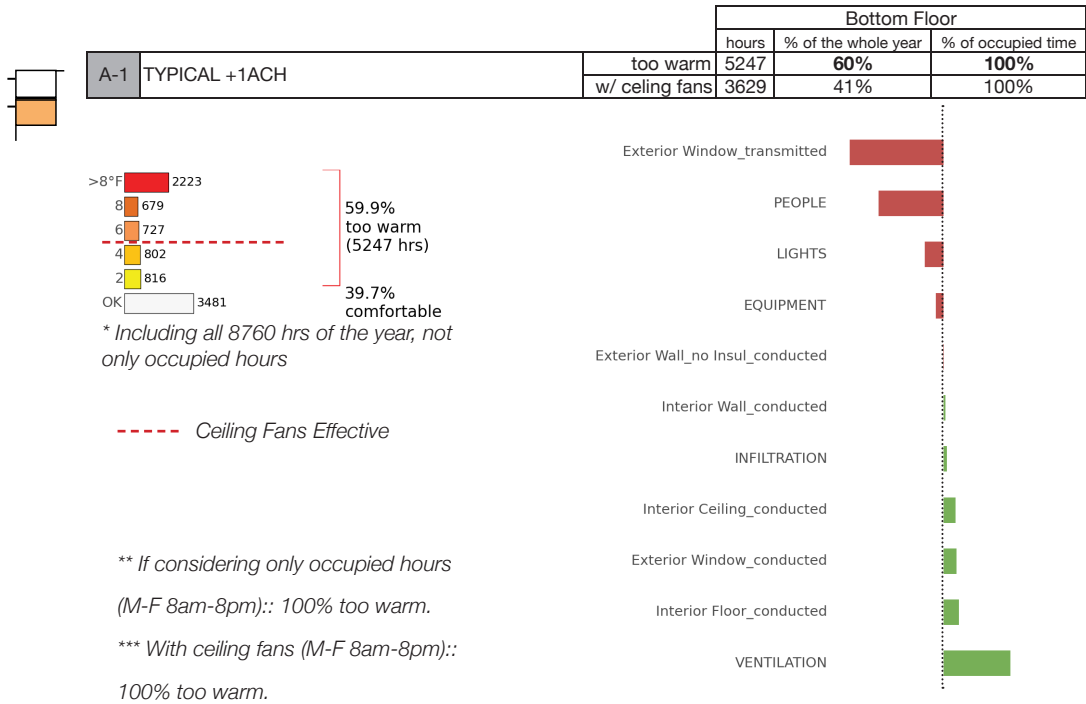
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.a.A.1 Classroom Analysis:: South Facing (Continued)



Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

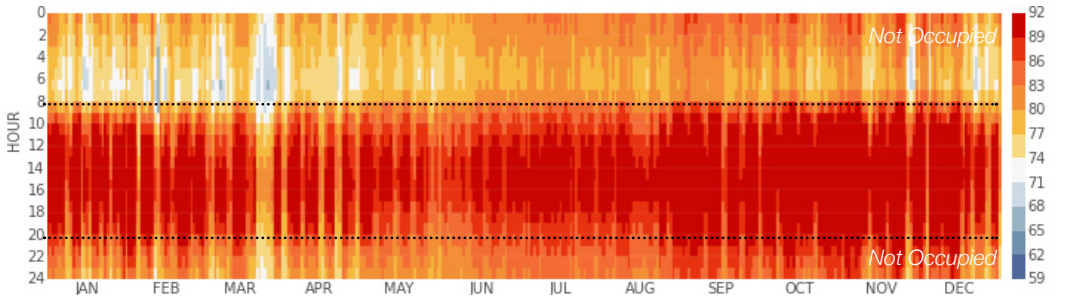


C.3.a.A. WINDOW PARAMETRICS

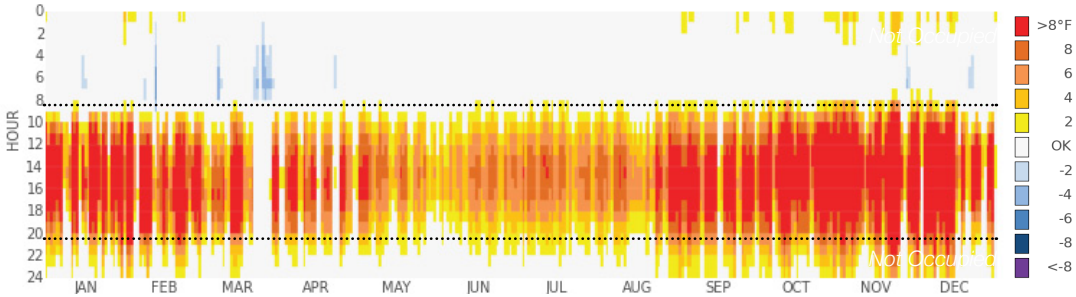
C.3.a.A.2 TYPICAL + 1ACH + Shading



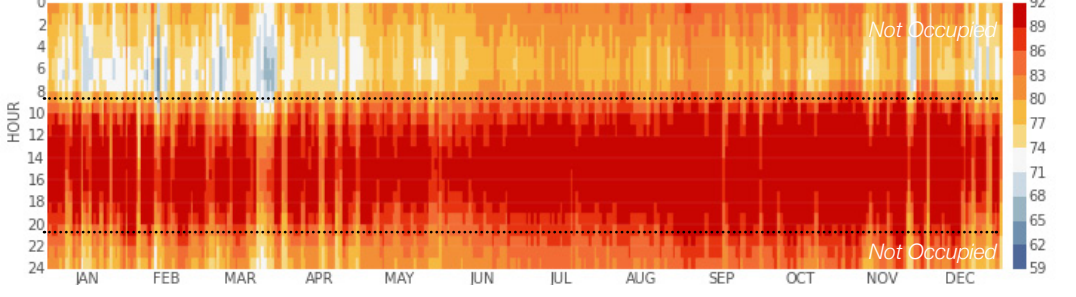
Operative temperature for bottom floor



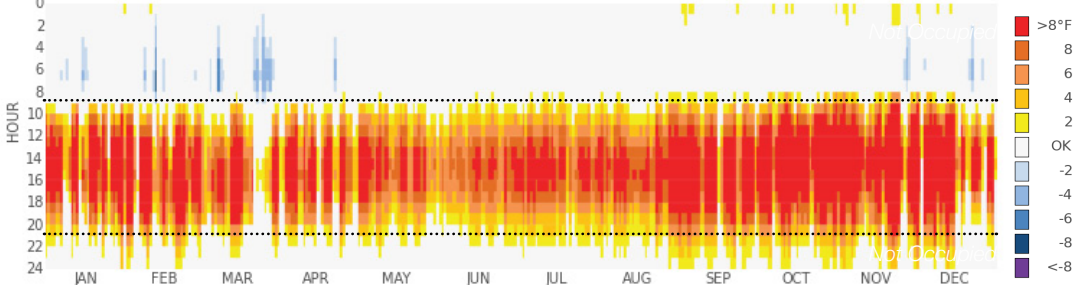
Degrees from comfort for bottom floor



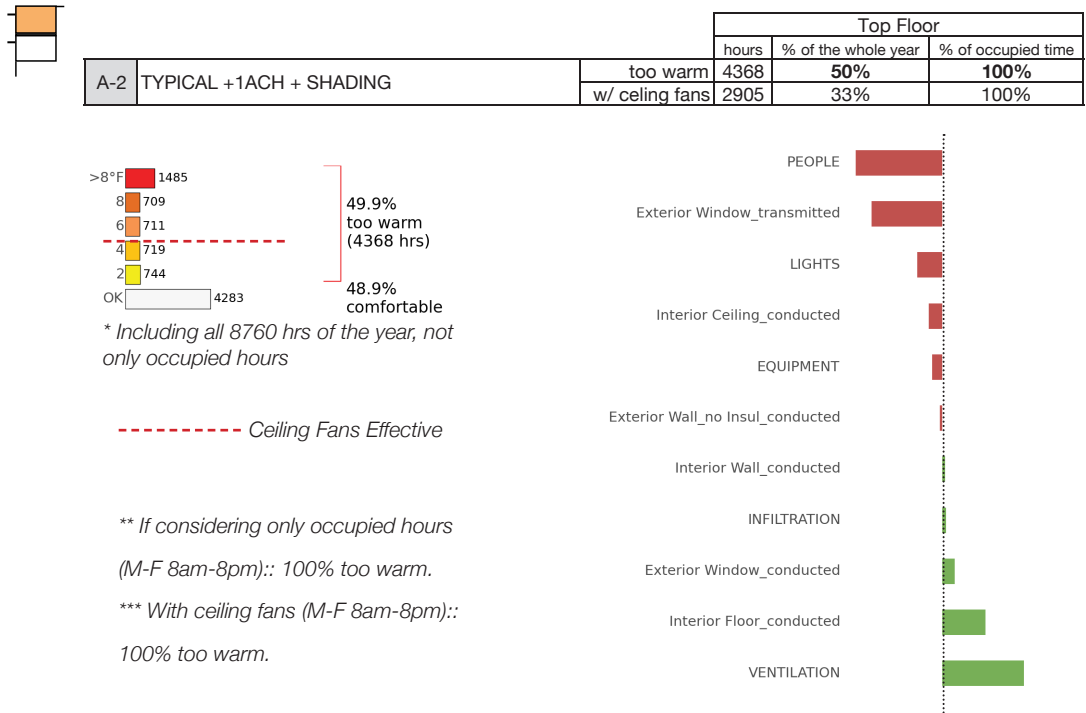
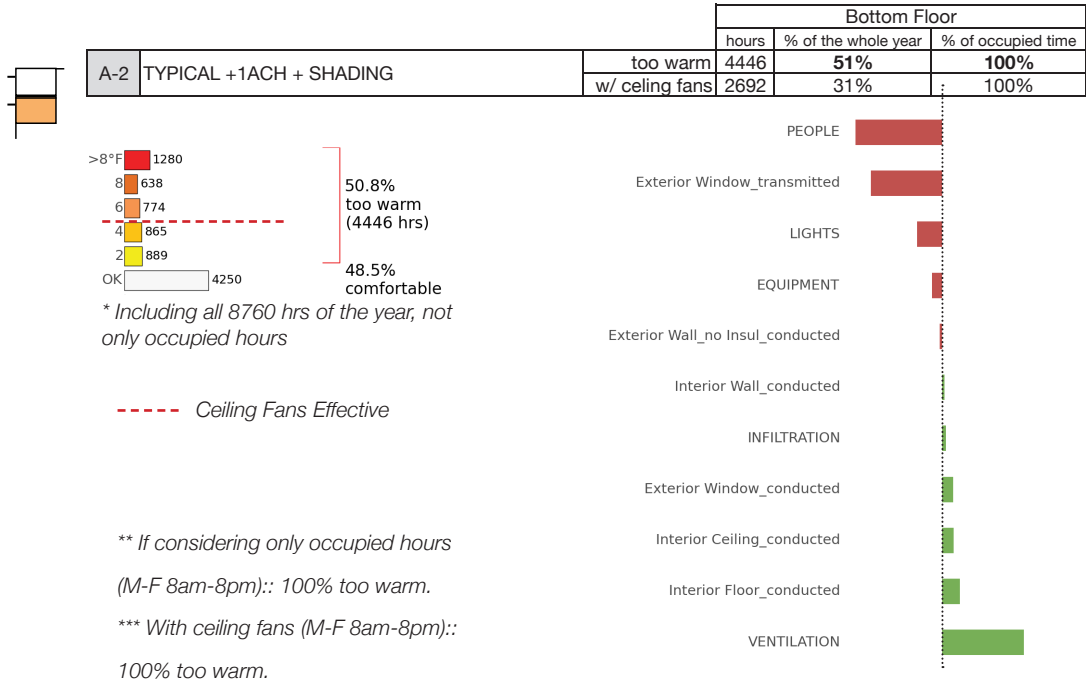
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.a.A.2 Classroom Analysis:: South Facing (Continued)



Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

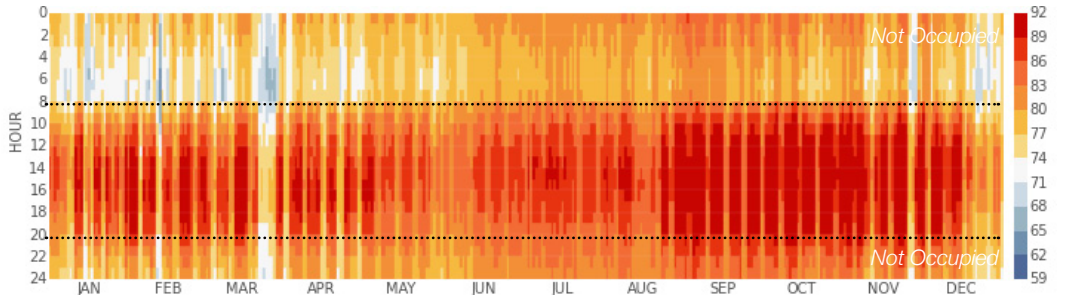


C.3.a.A. WINDOW PARAMETRICS

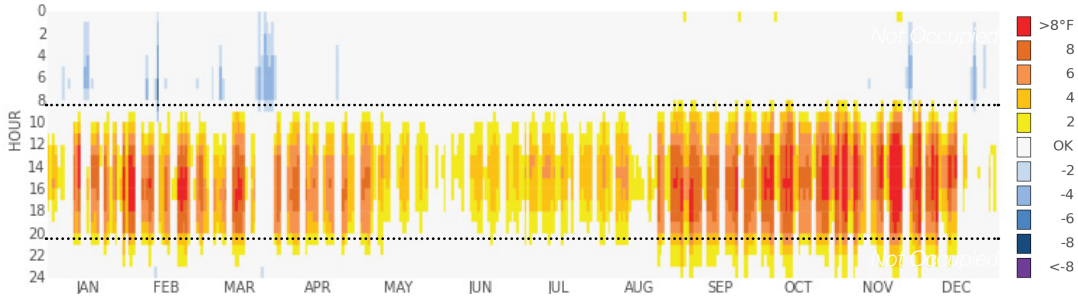
C.3.a.A,3 TYPICAL + 1ACH + Shading + IECC 2015 Windows



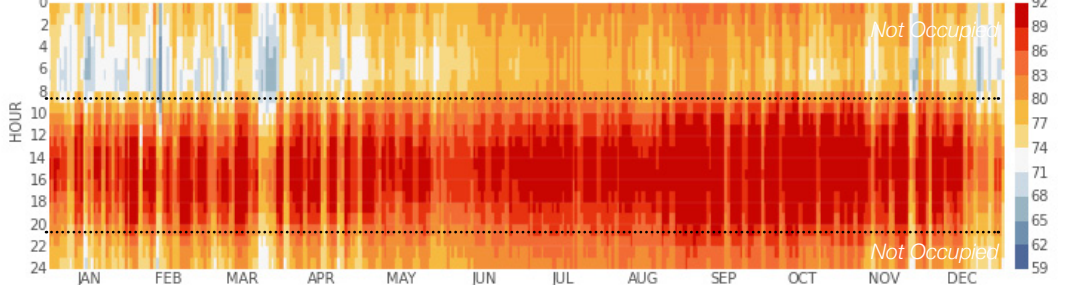
Operative temperature for bottom floor



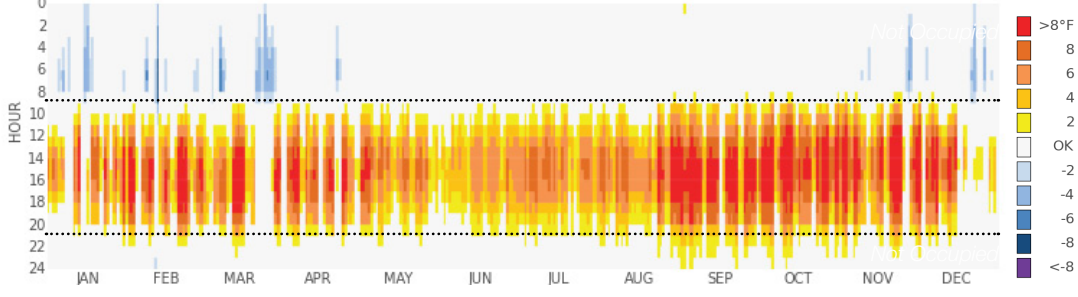
Degrees from comfort for bottom floor



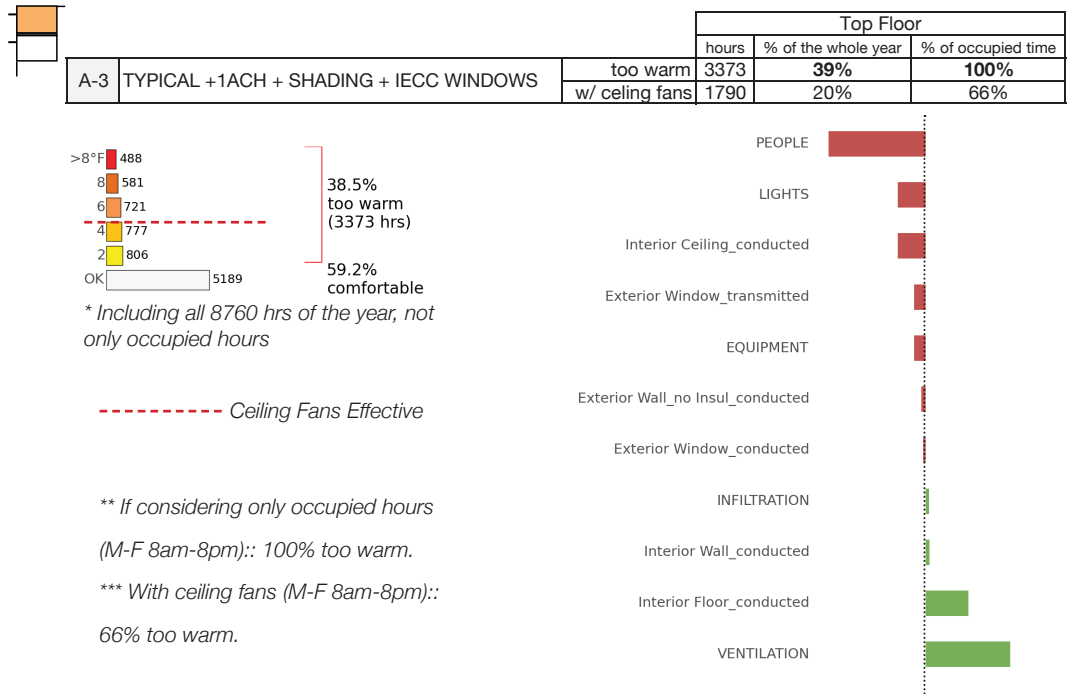
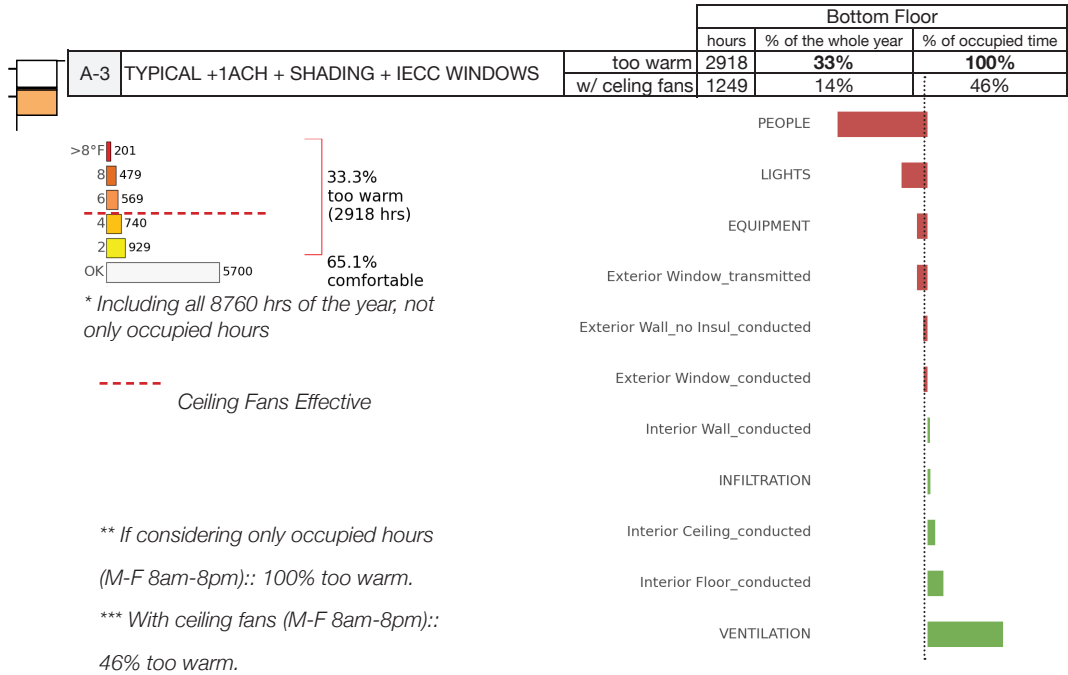
Operative temperature for top floor



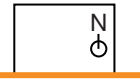
Degrees from comfort for top floor



Add/C.3.a.A.3 Classroom Analysis:: South Facing (Continued)



Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

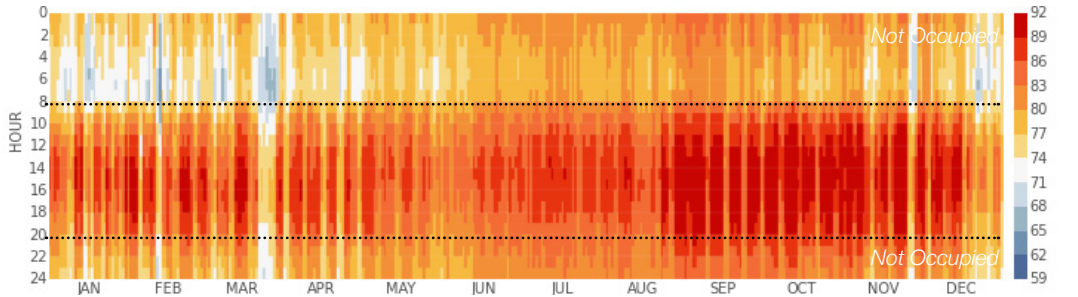


C.3.a.B. INTERNAL LOAD PARAMETRICS

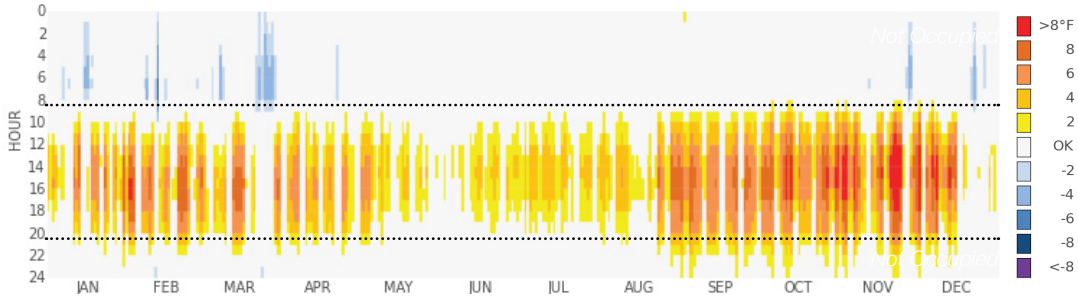
C.3.a.B.1 TYPICAL + IECC Windows + Shading + lower LPD +1ACH



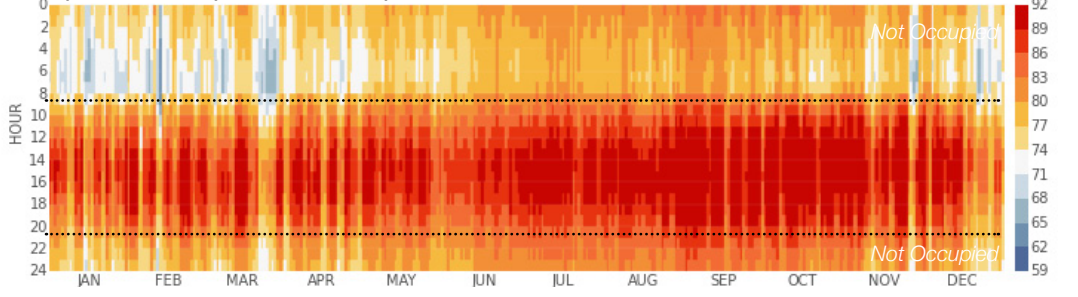
Operative temperature for bottom floor



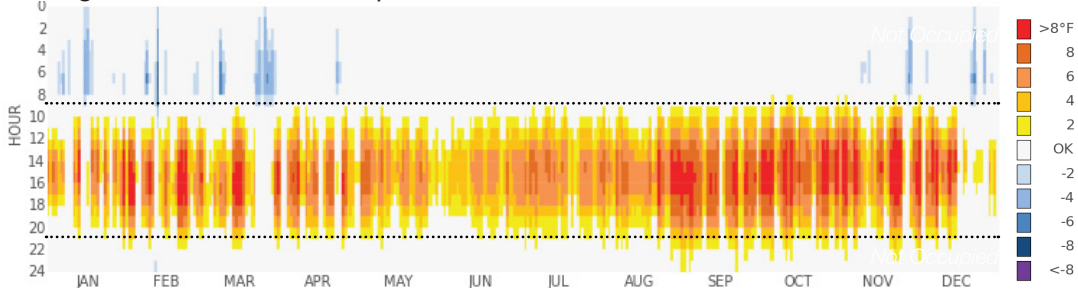
Degrees from comfort for bottom floor



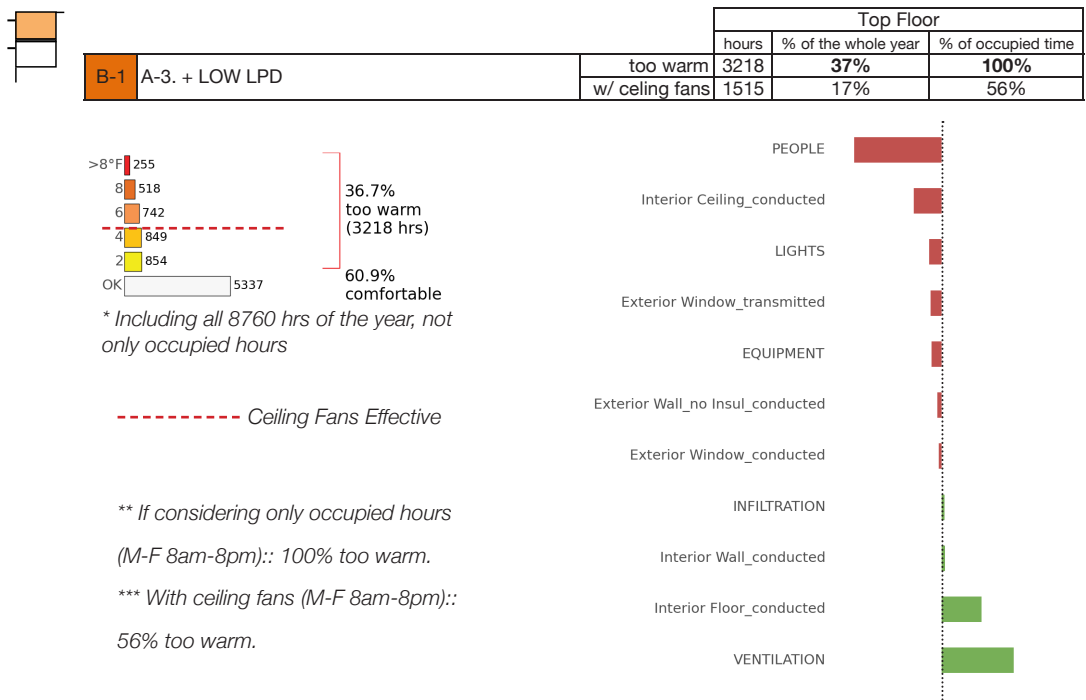
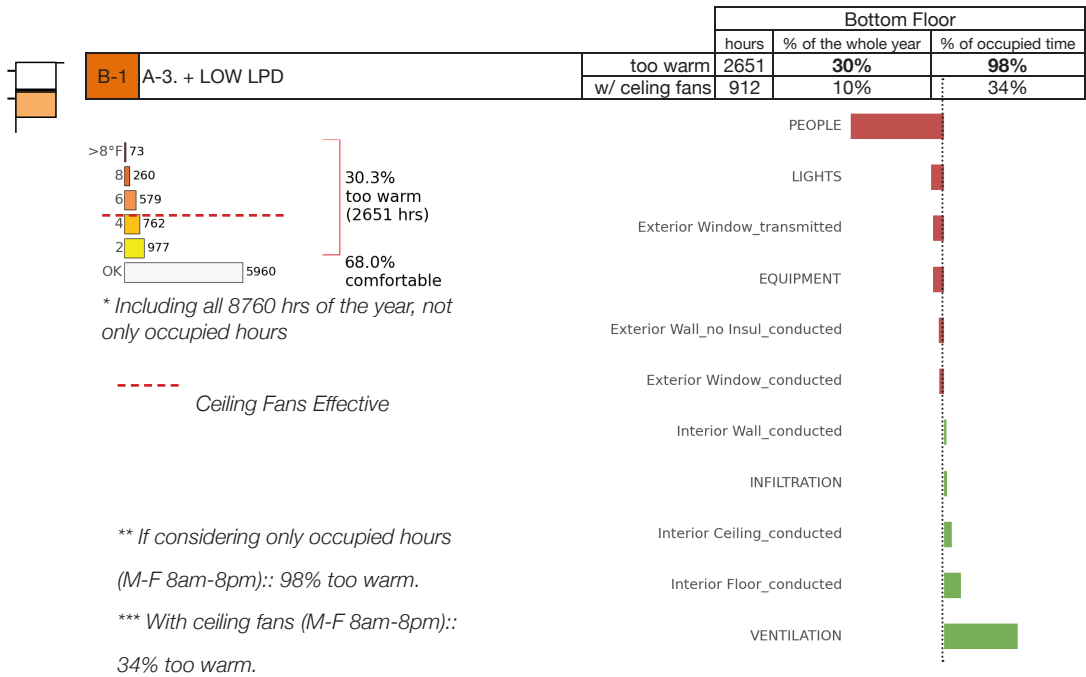
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.a.B.1 Classroom Analysis:: South Facing (Continued)



Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

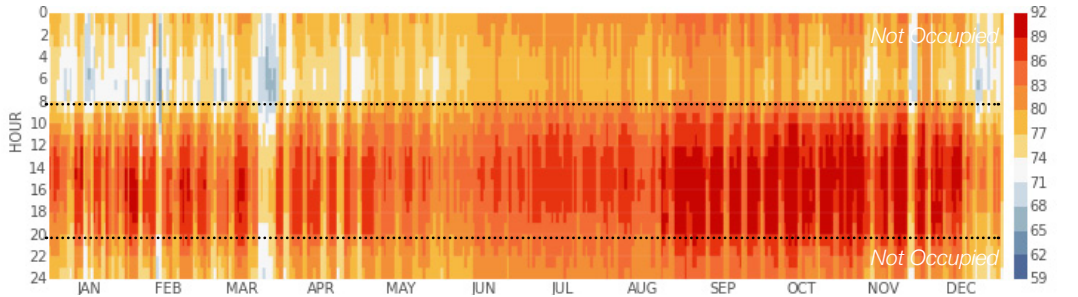


C.3.a.B. INTERNAL LOAD PARAMETRICS

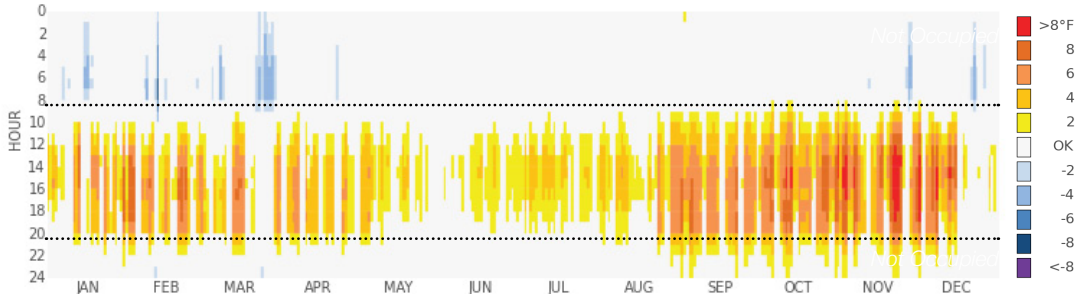
C.3.a.B.2 TYPICAL + IECC Windows + Shading + Daylight Controls +1ACH



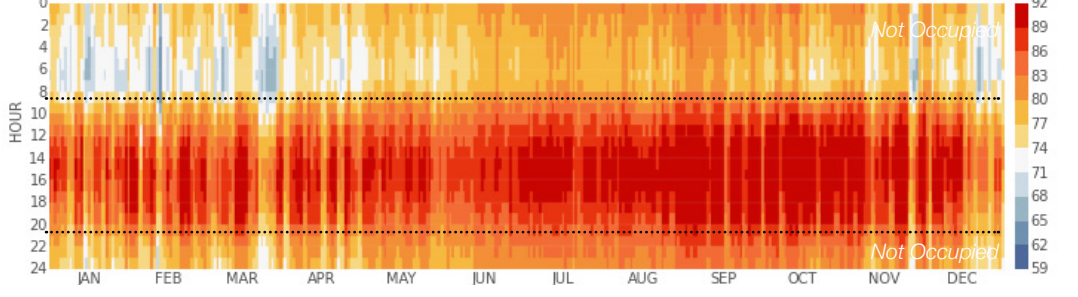
Operative temperature for bottom floor



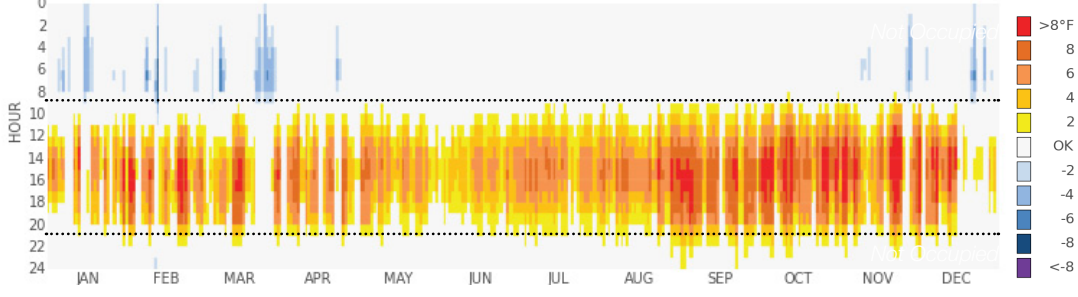
Degrees from comfort for bottom floor



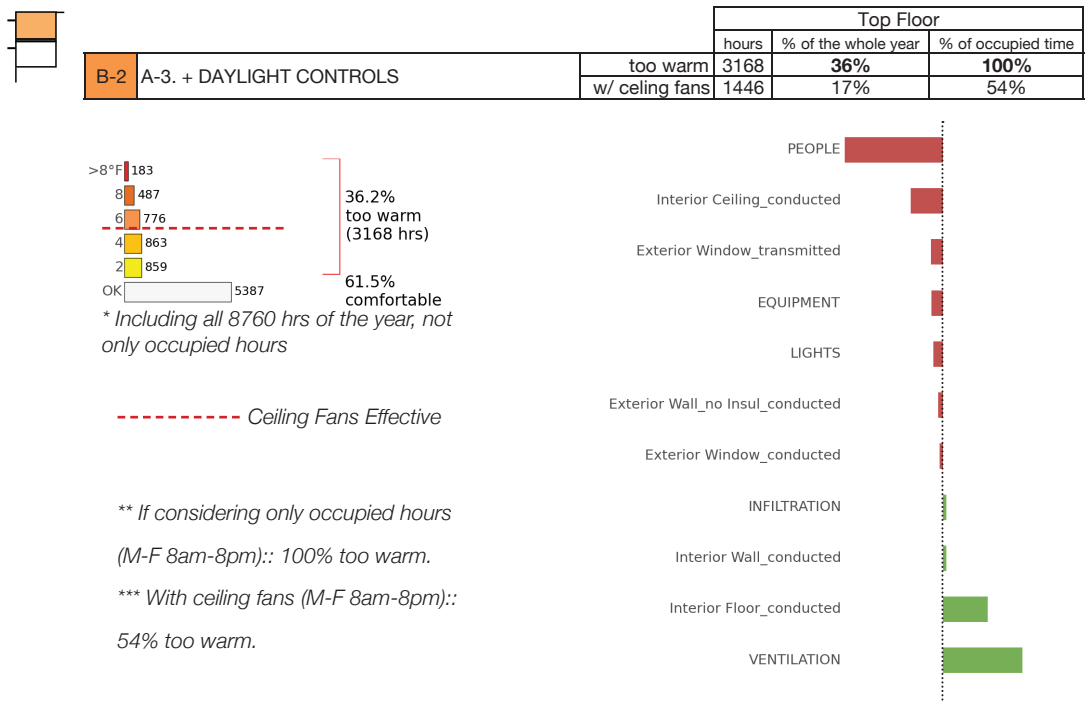
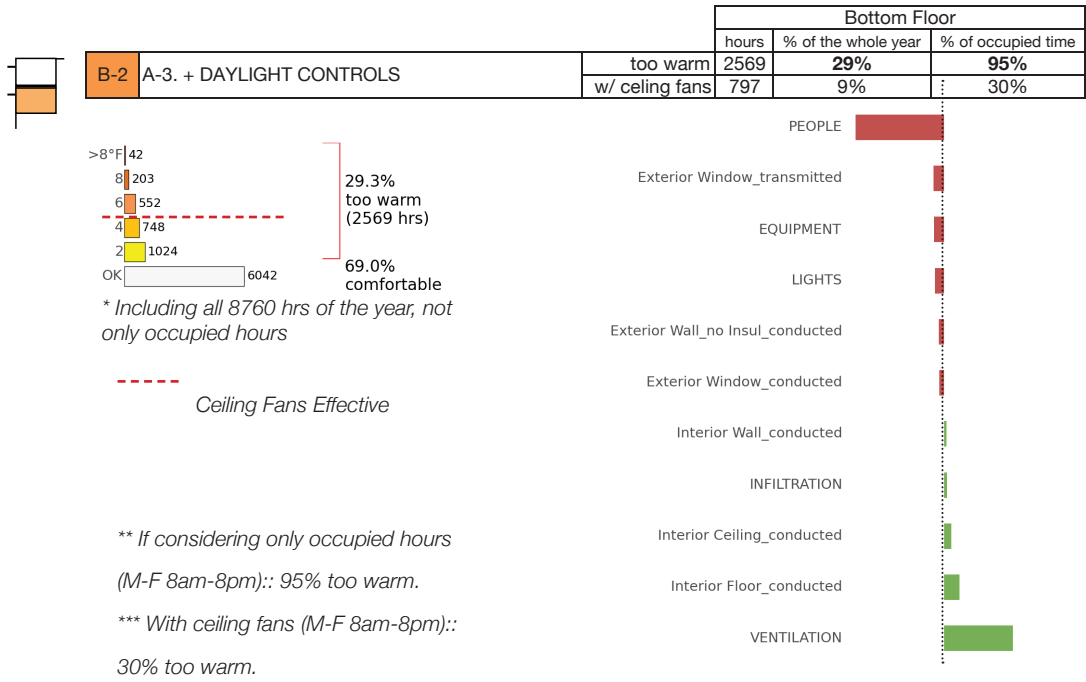
Operative temperature for top floor



Degrees from comfort for top floor

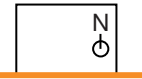


Add/C.3.a.B.2 Classroom Analysis:: South Facing (Continued)



Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

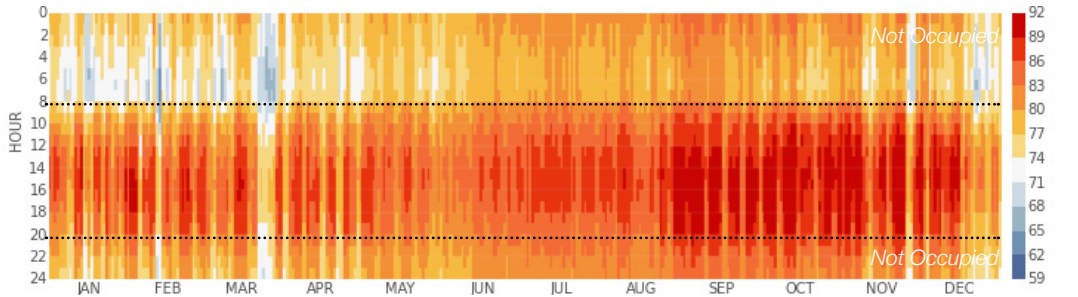
C.3.a.B. INTERNAL LOAD PARAMETRICS:: MINIMUM SUITE



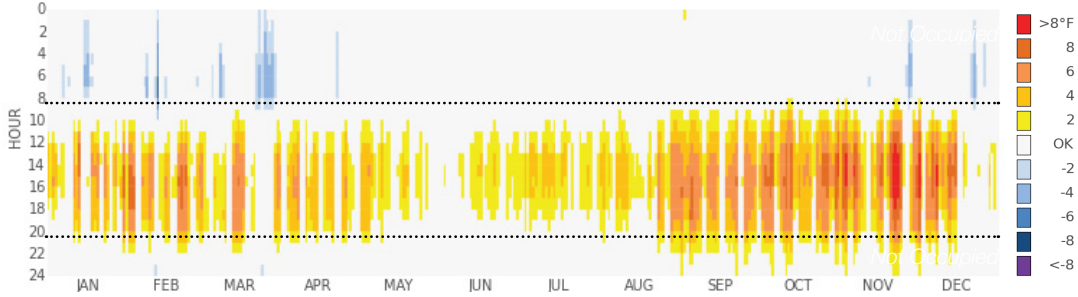
C.3.a.B.3 TYPICAL + IECC Windows + Shading +lower LPD + Daylight Controls +1ACH



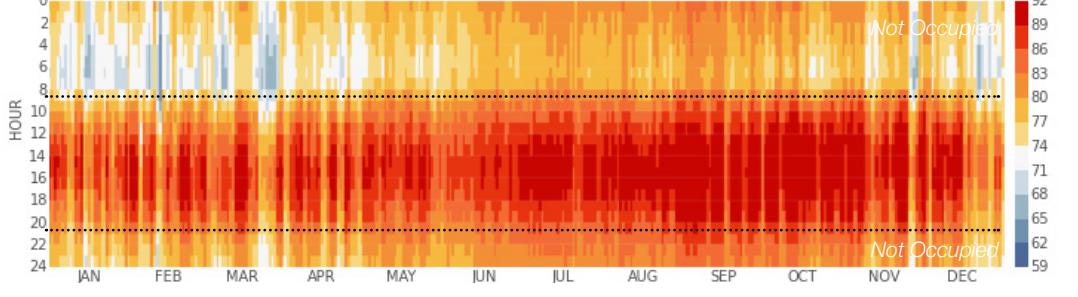
Operative temperature for bottom floor



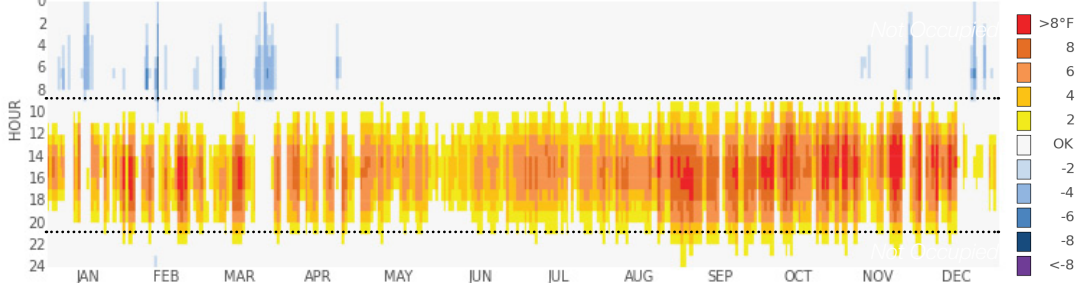
Degrees from comfort for bottom floor



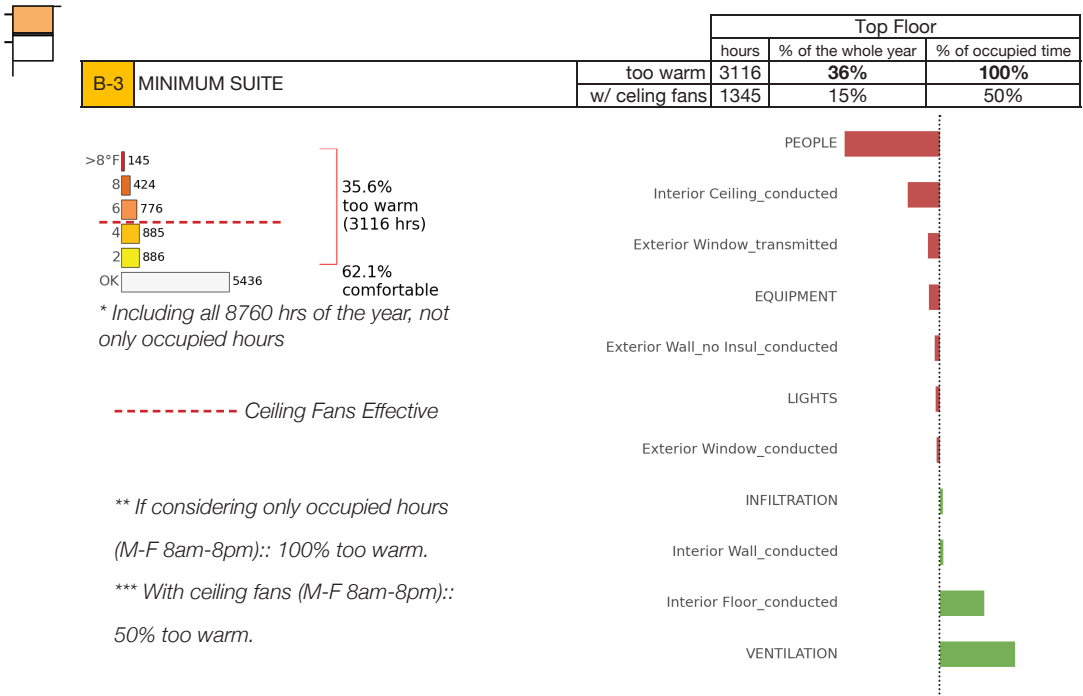
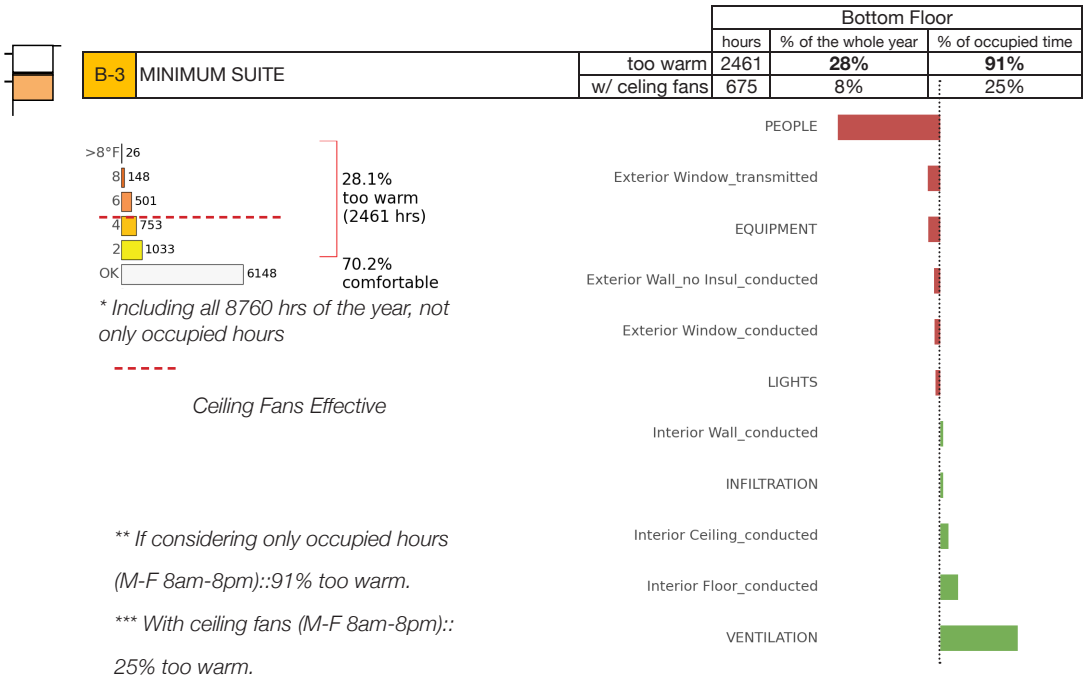
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.a.B.3 Classroom Analysis:: South Facing (Continued)



Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

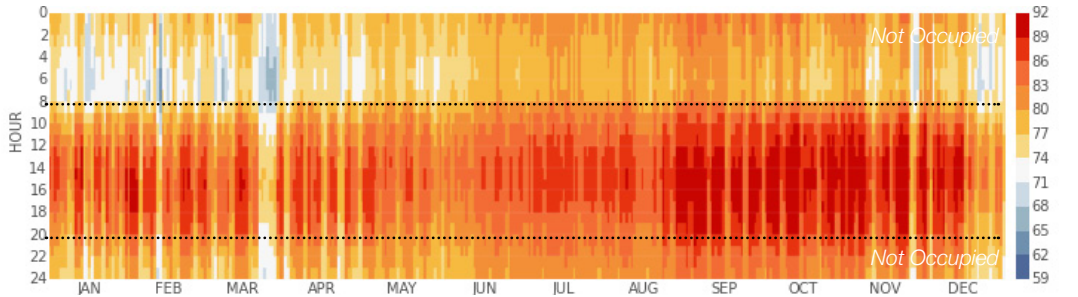
C.3.a.C. EXTERIOR OPAQUE SURFACE PARAMETRICS:: IMPROVED SUITE



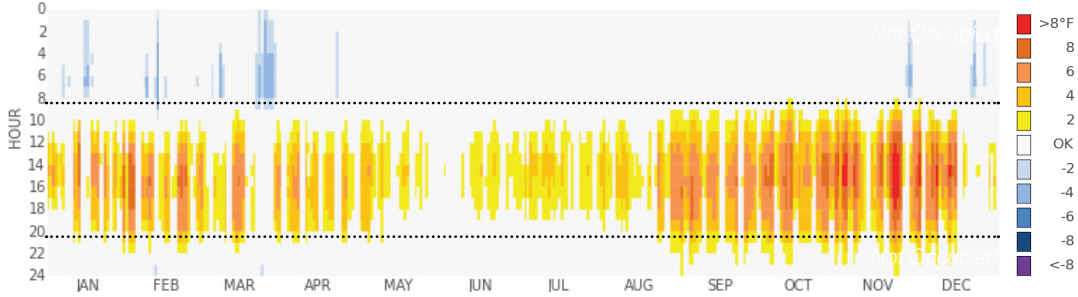
C.3.a.C.1 MINIMUM SUITE + IECC Roof



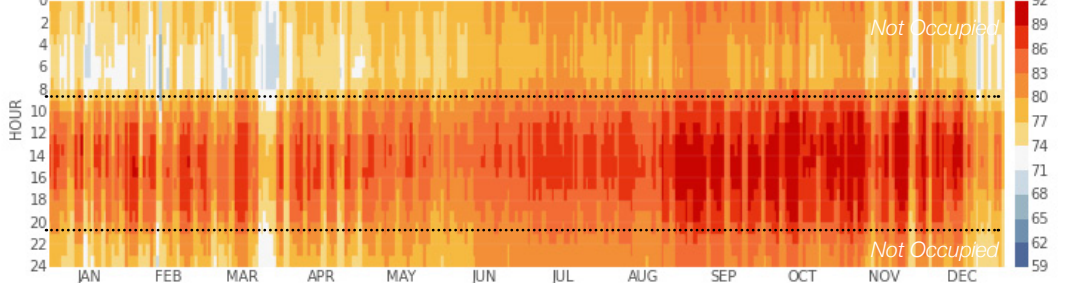
Operative temperature for bottom floor



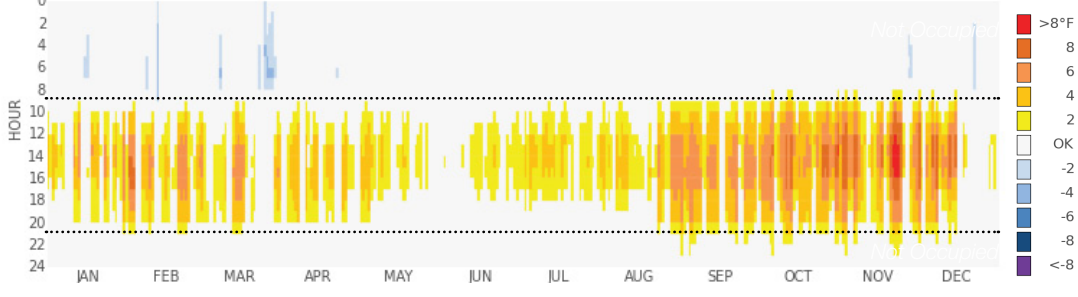
Degrees from comfort for bottom floor



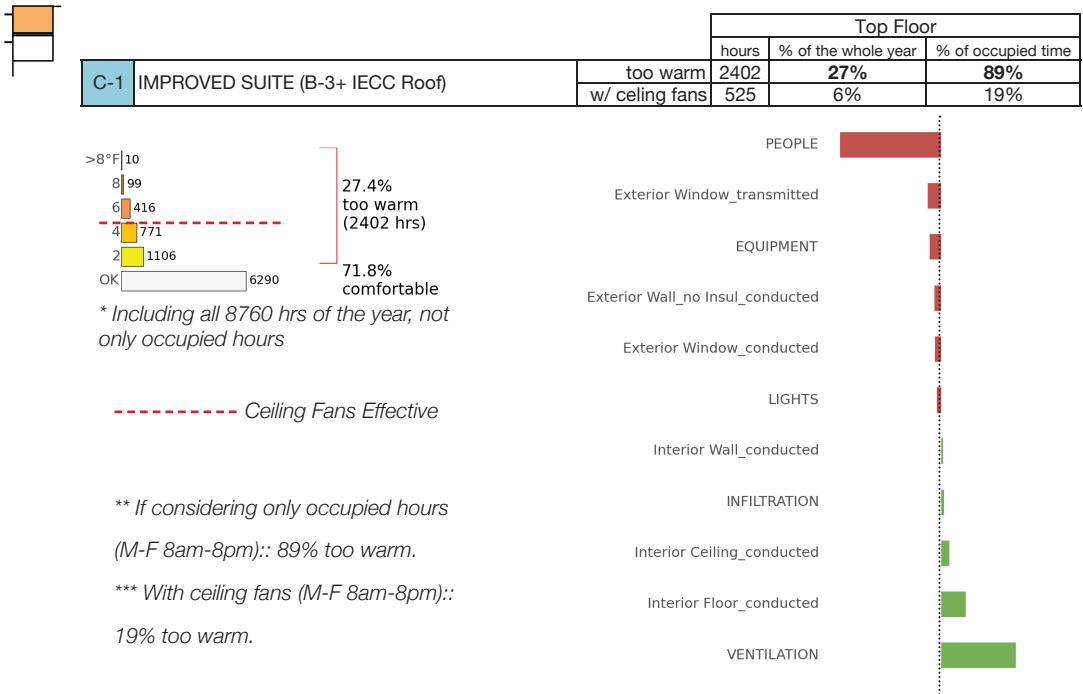
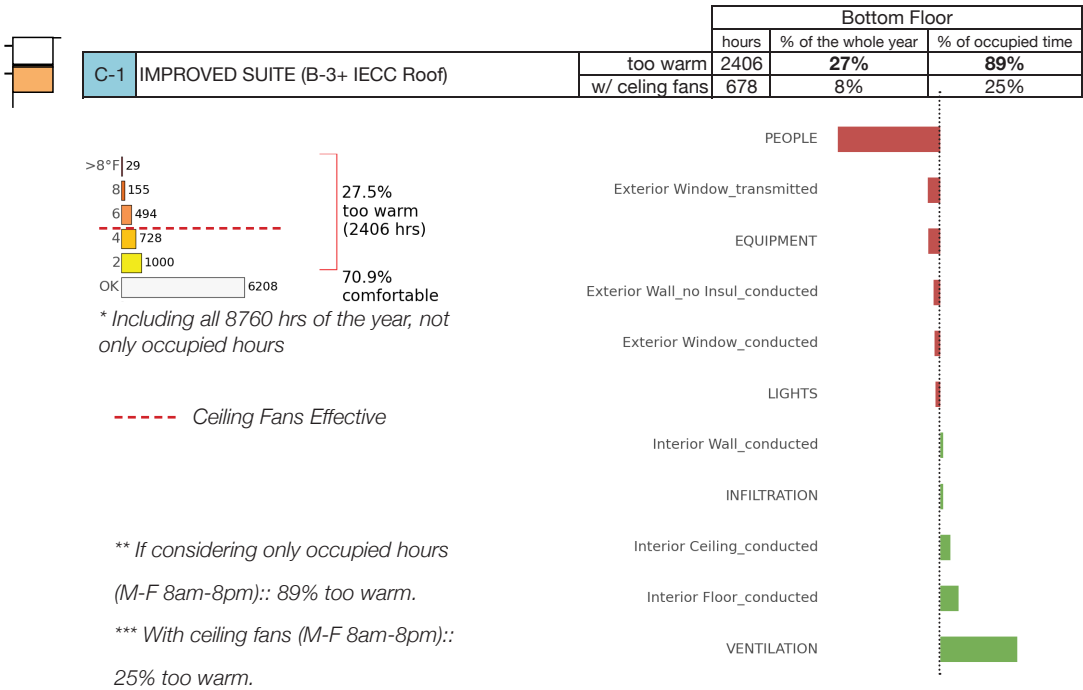
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.a.C.1 Classroom Analysis:: South Facing (Continued)



Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

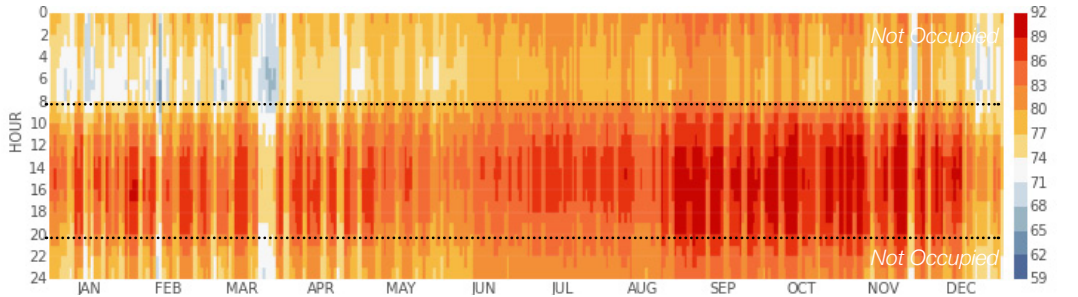
C.3.a.C. EXTERIOR OPAQUE SURFACE PARAMETRICS:: CODE SUITE



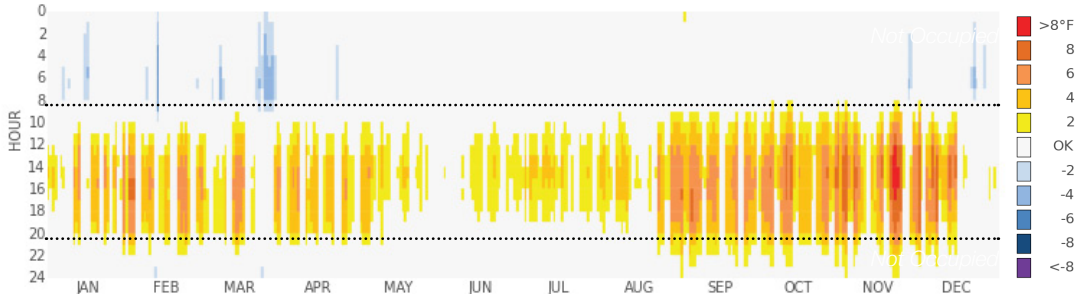
C.3.a.C.2 IMPROVED SUITE + IECC Walls



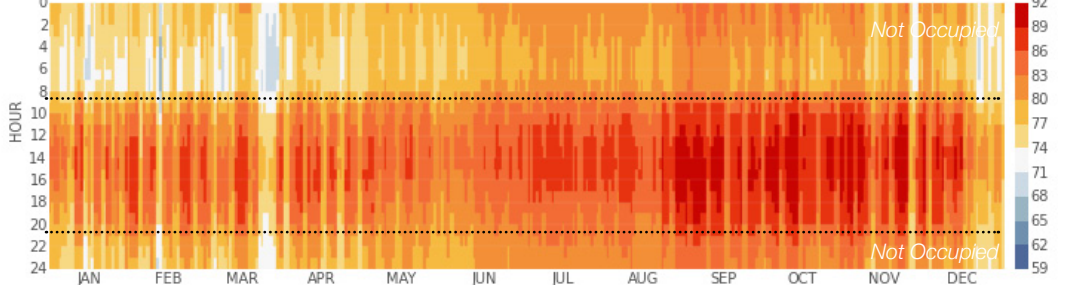
Operative temperature for bottom floor



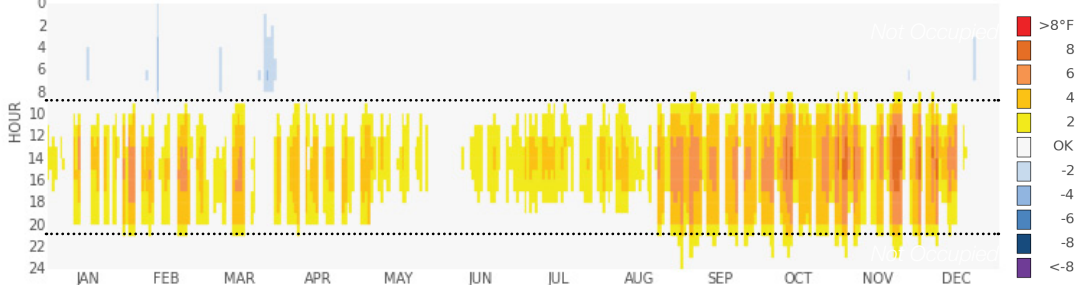
Degrees from comfort for bottom floor



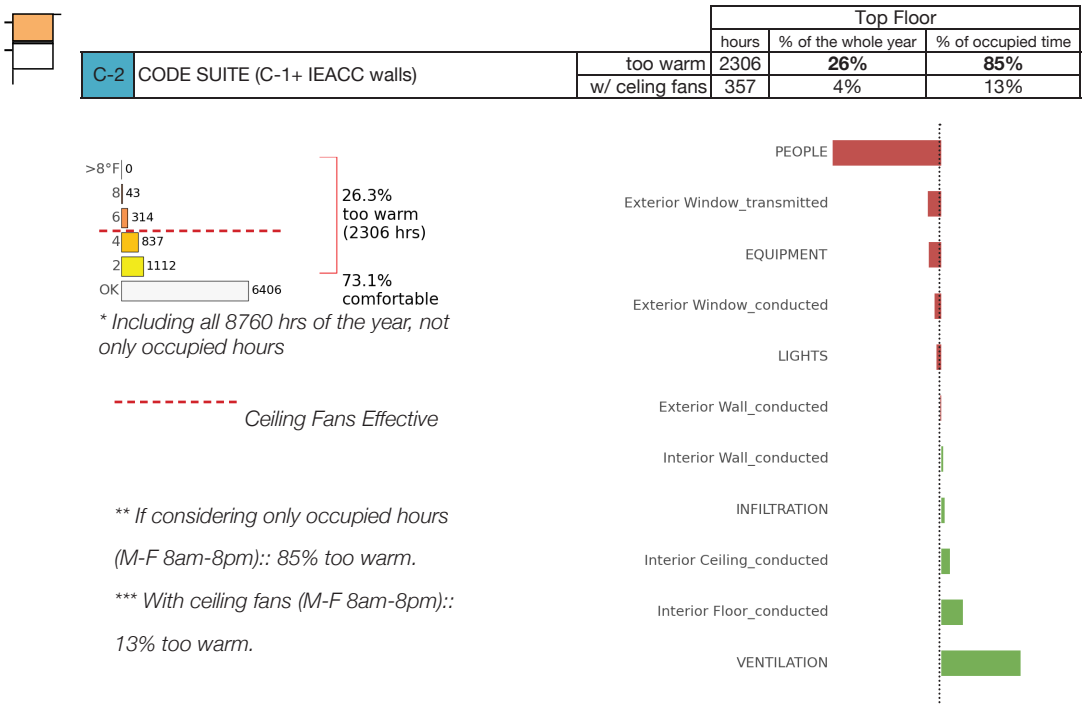
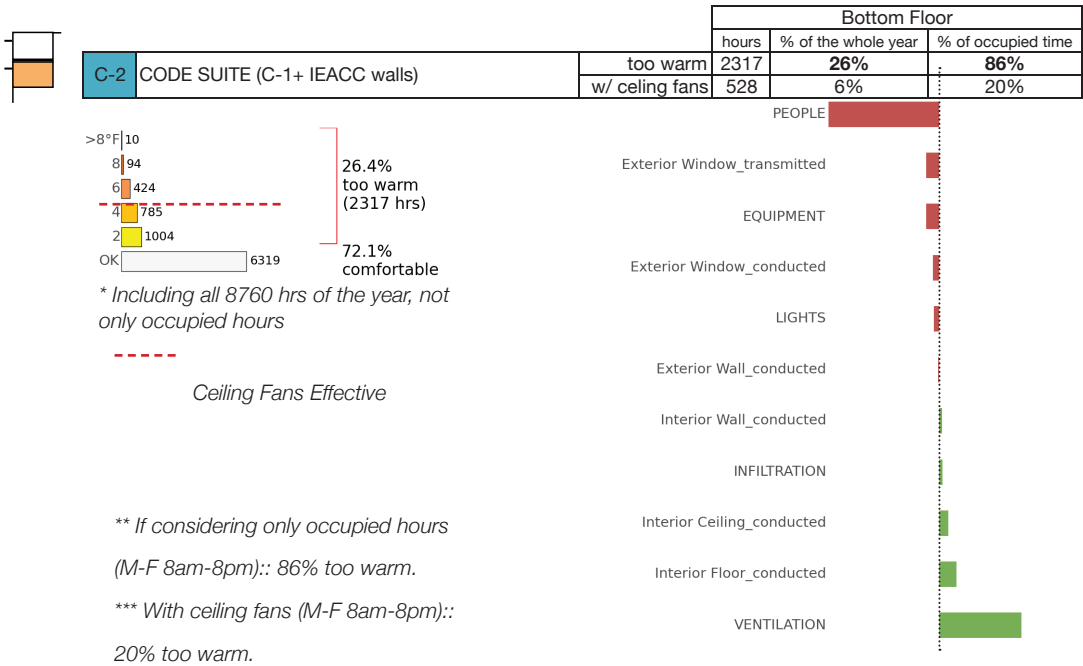
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.a.C.2 Classroom Analysis:: South Facing (Continued)



Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

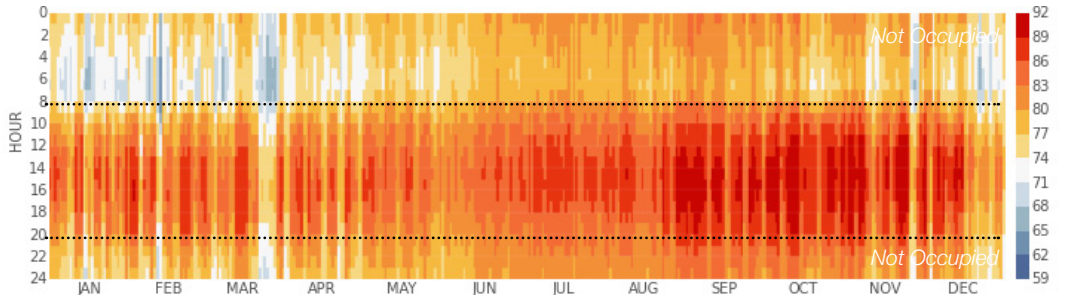


C.3.a.D. VENTILATION PARAMETRICS

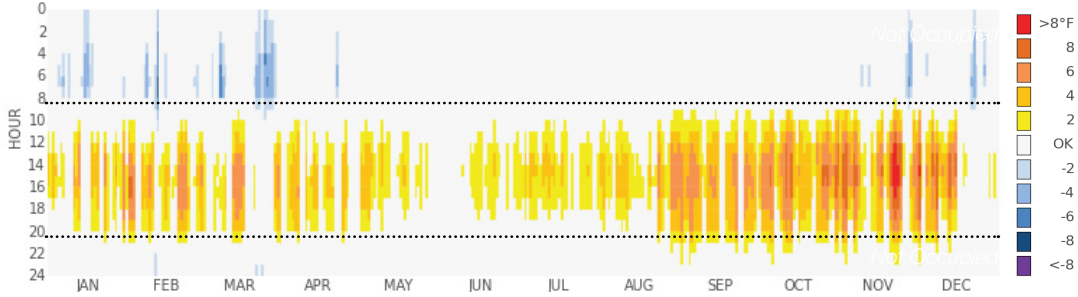
C.3.a.D.1 MINIMUM SUITE +2ACH



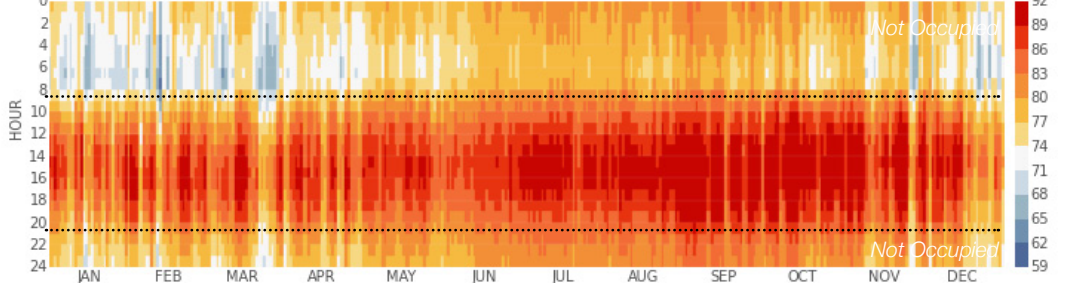
Operative temperature for bottom floor



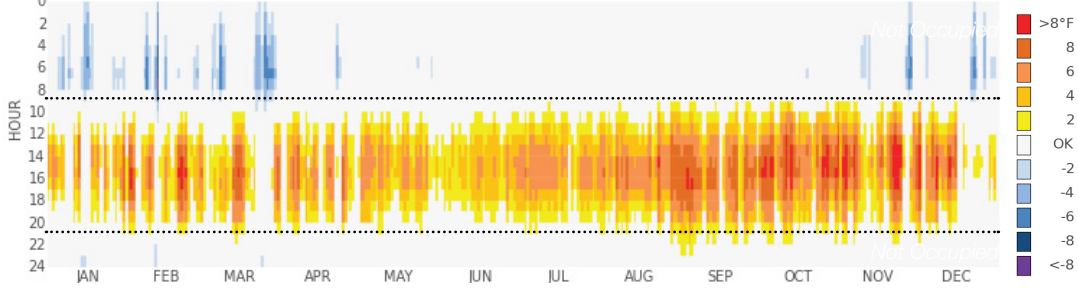
Degrees from comfort for bottom floor



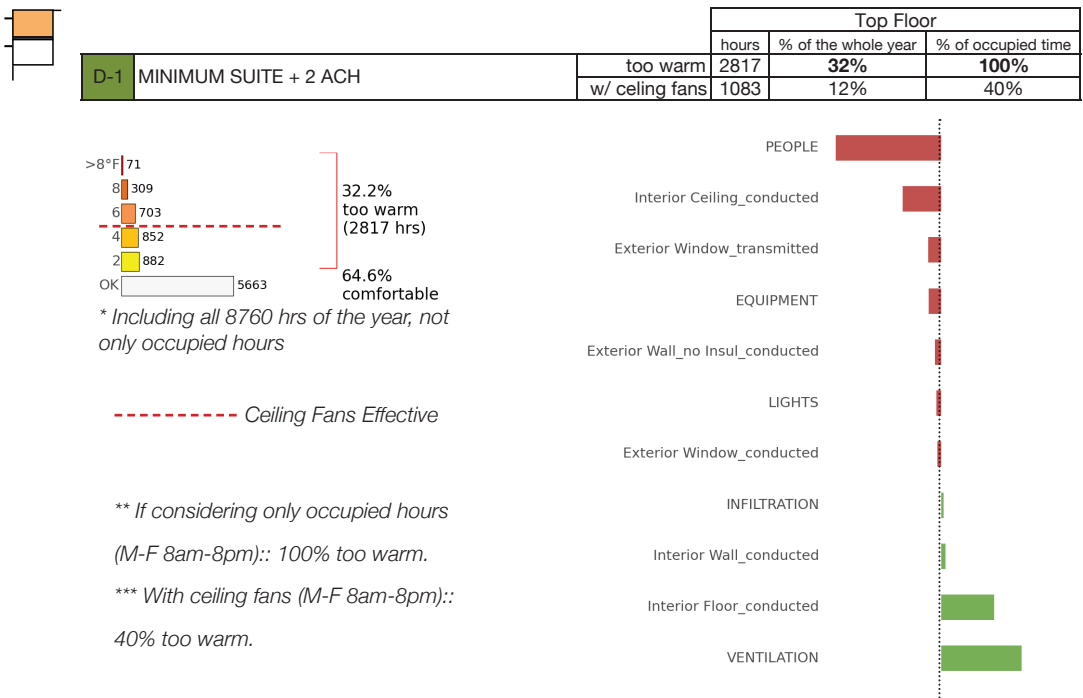
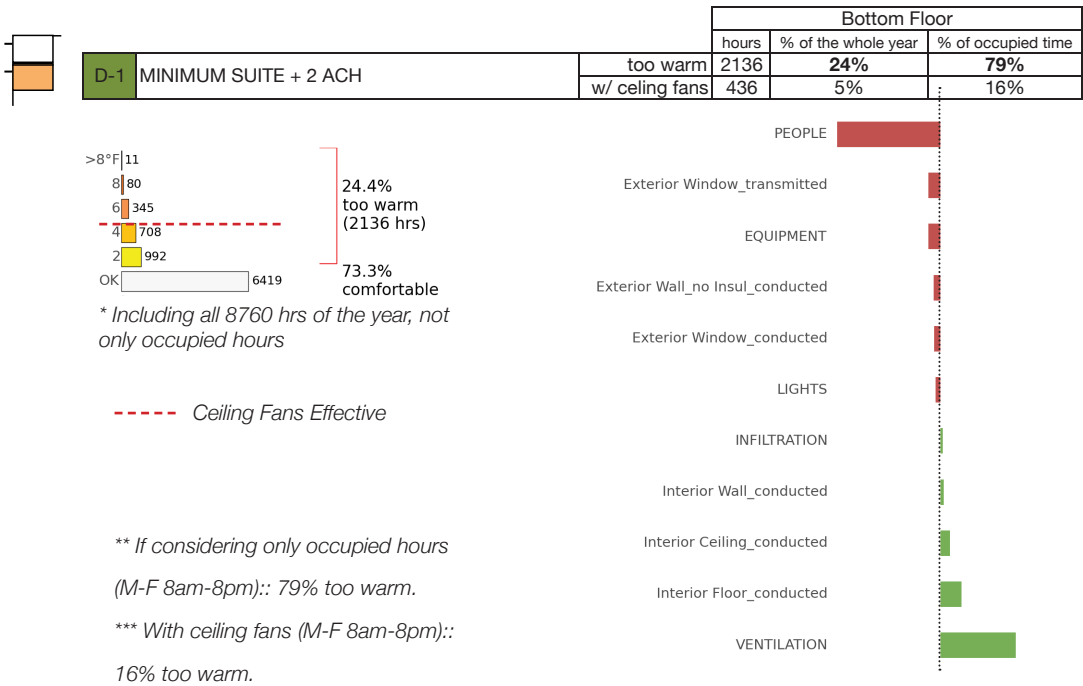
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.a.D.1 Classroom Analysis:: South Facing (Continued)



Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

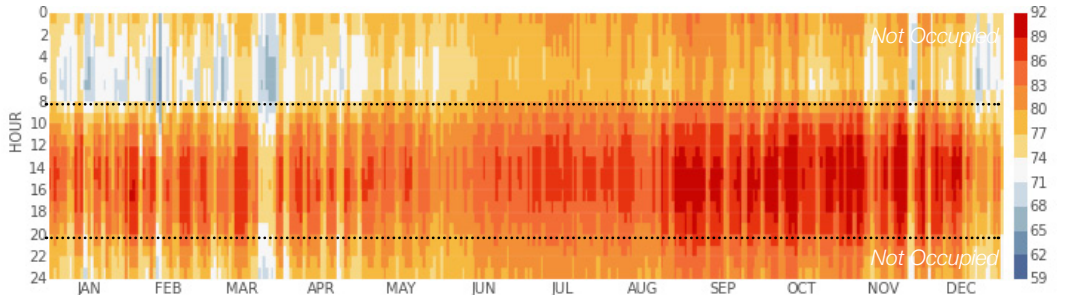


C.3.a.D. VENTILATION PARAMETRICS

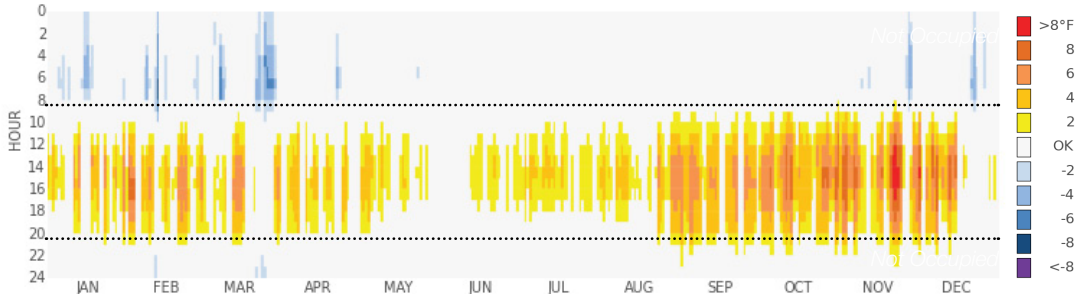
C.3.a.D.2 IMPROVED SUITE +2ACH



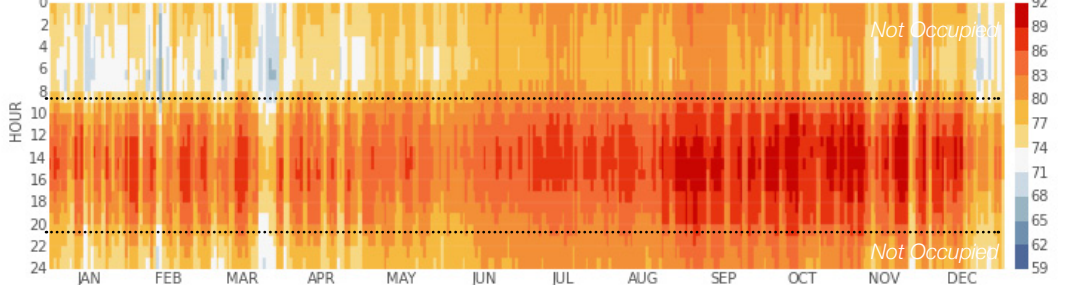
Operative temperature for bottom floor



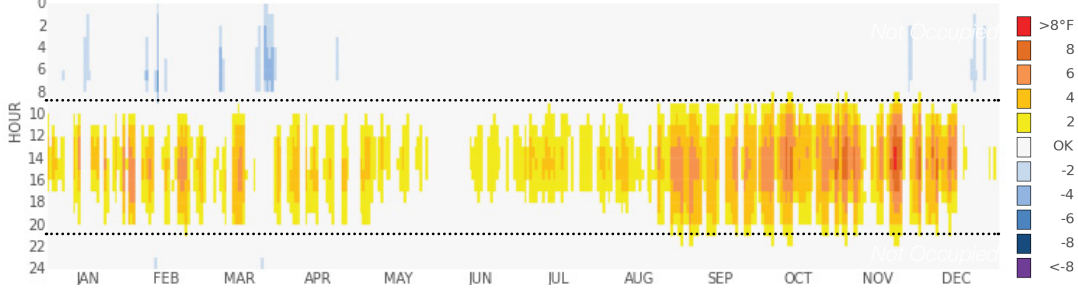
Degrees from comfort for bottom floor



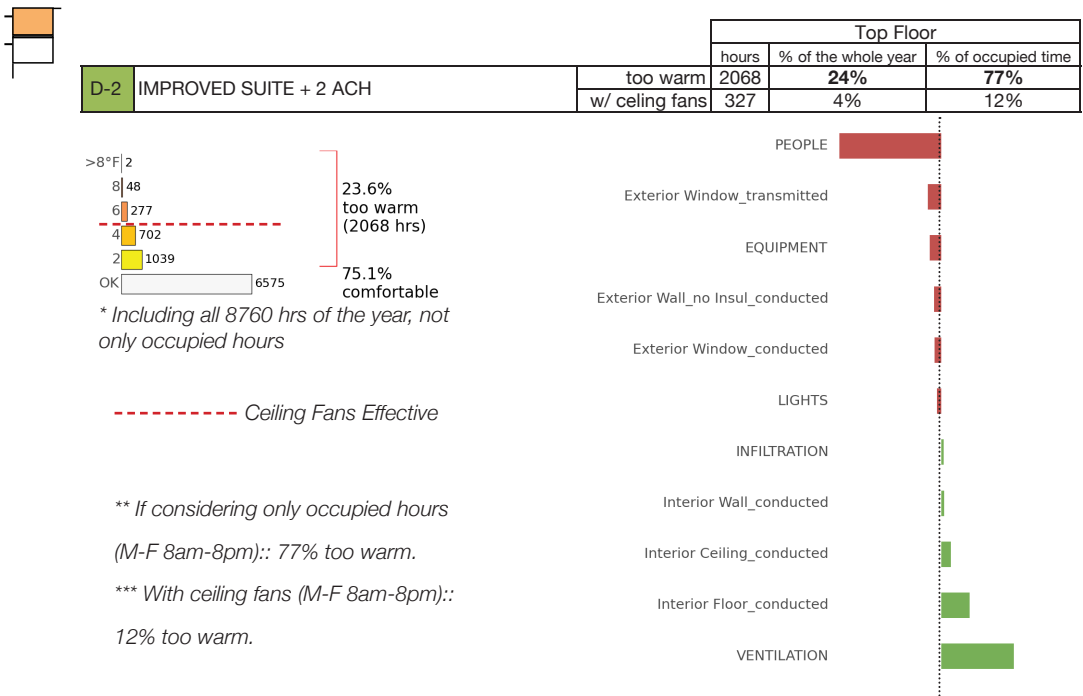
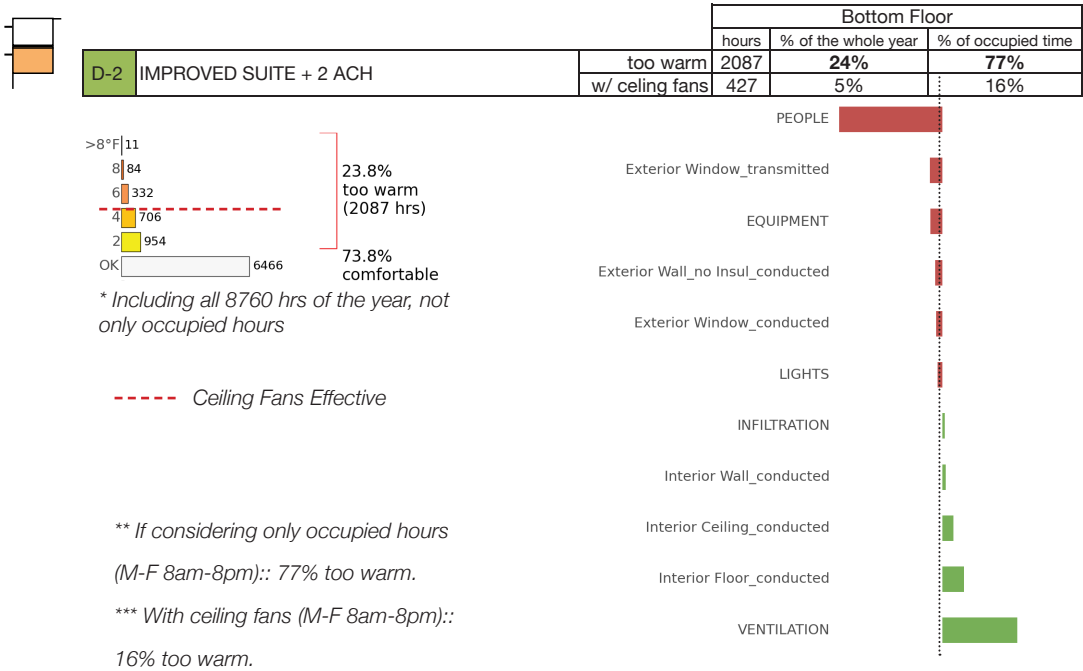
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.a.D.2 Classroom Analysis:: South Facing (Continued)



Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

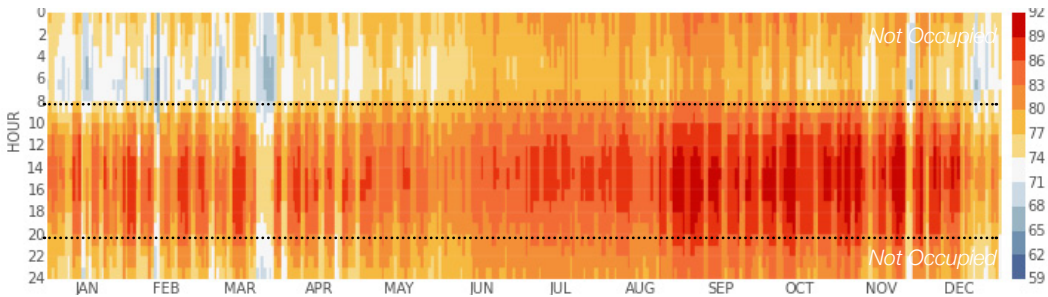


C.3.a.D. VENTILATION PARAMETRICS

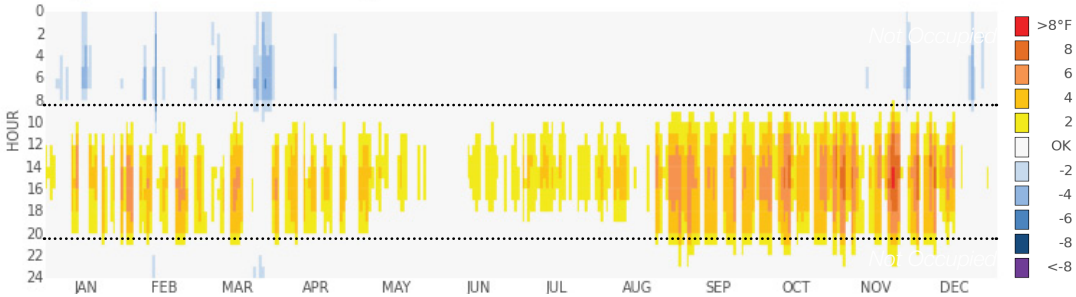
C.3.a.D.3 CODE SUITE +2ACH



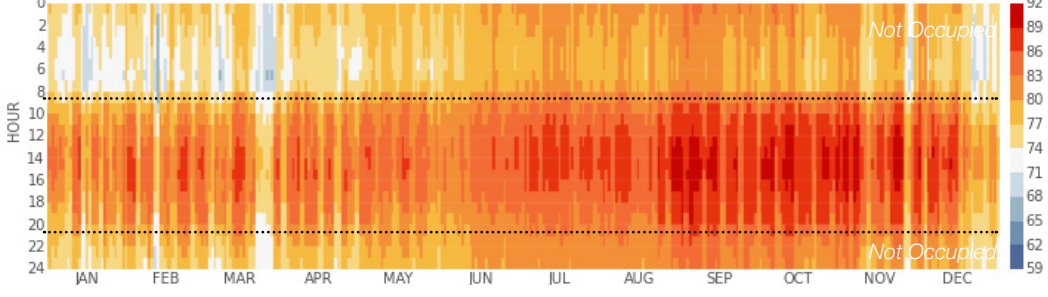
Operative temperature for bottom floor



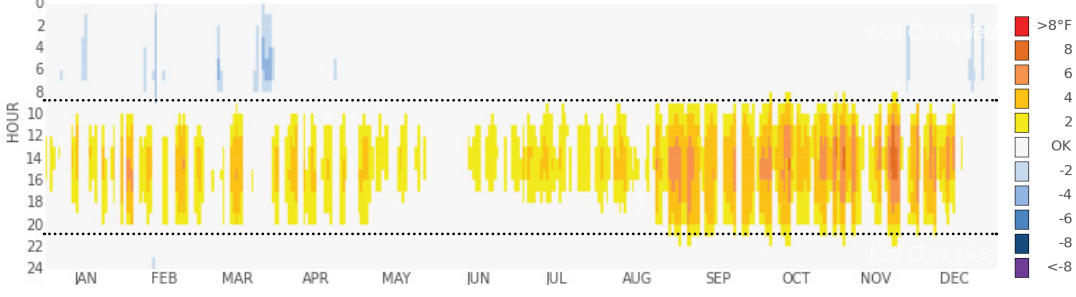
Degrees from comfort for bottom floor



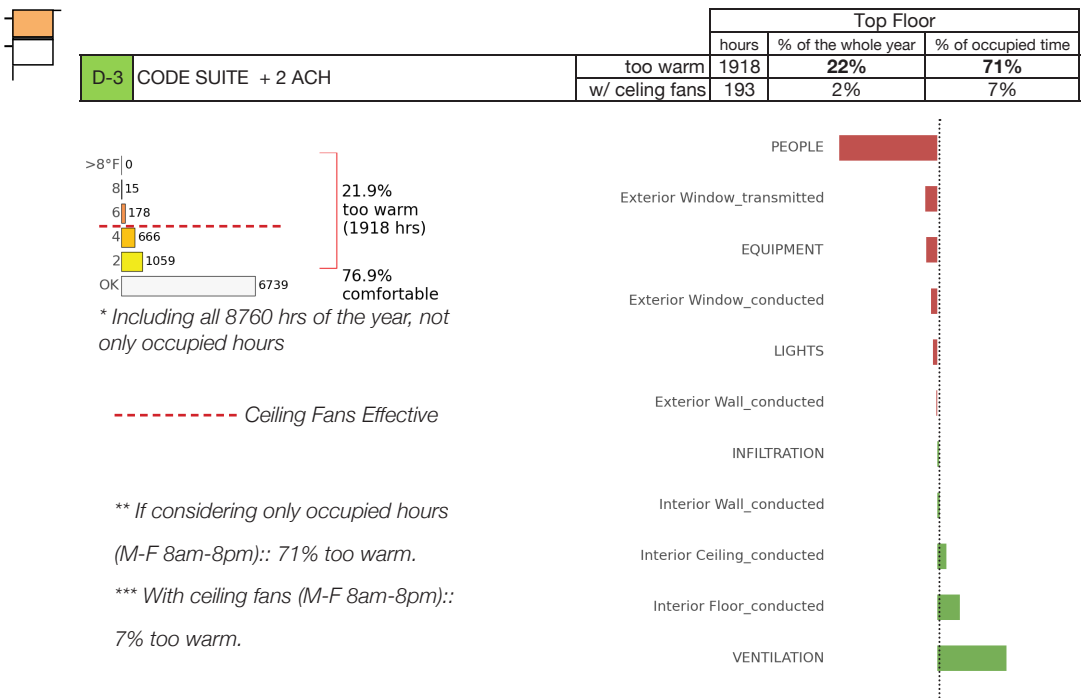
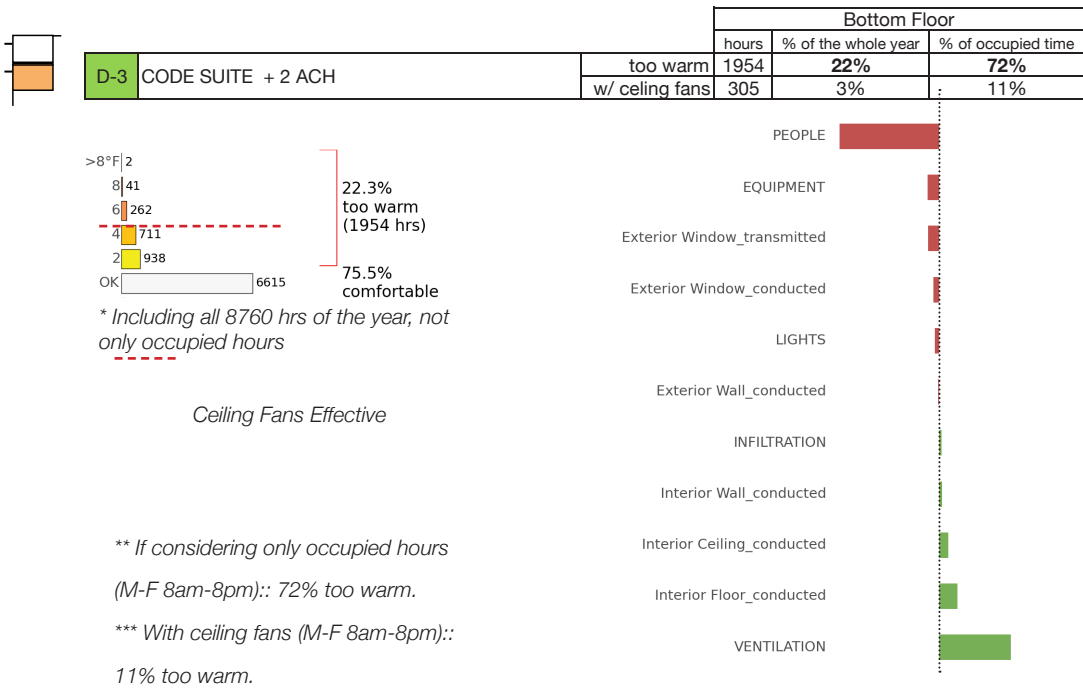
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.a.D.3 Classroom Analysis:: South Facing (Continued)



Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

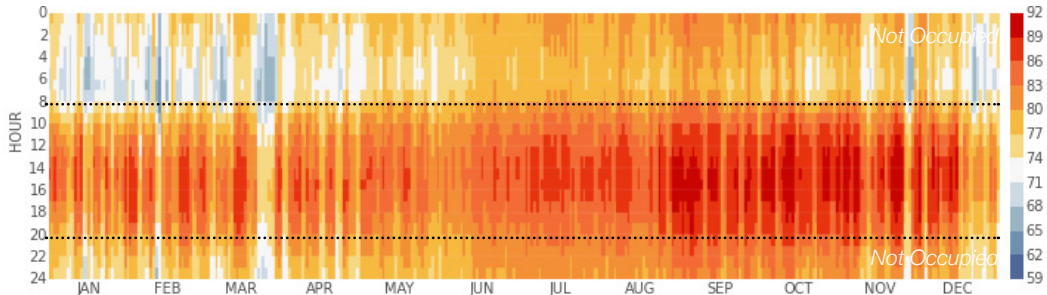


C.3.a.D. VENTILATION PARAMETRICS

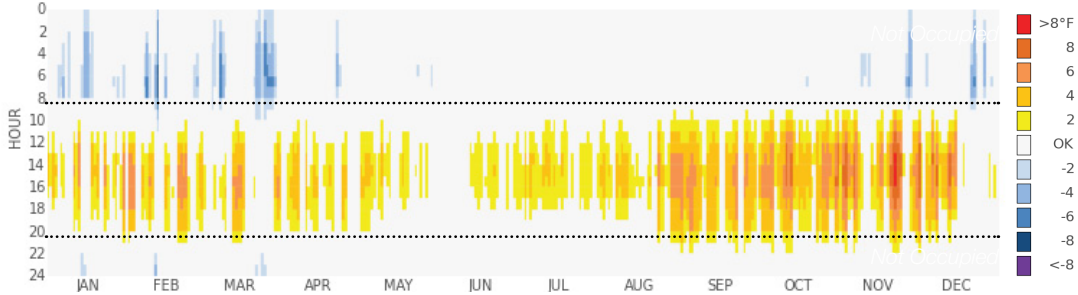
C.3.a.D.4 MINIMUM SUITE +3ACH



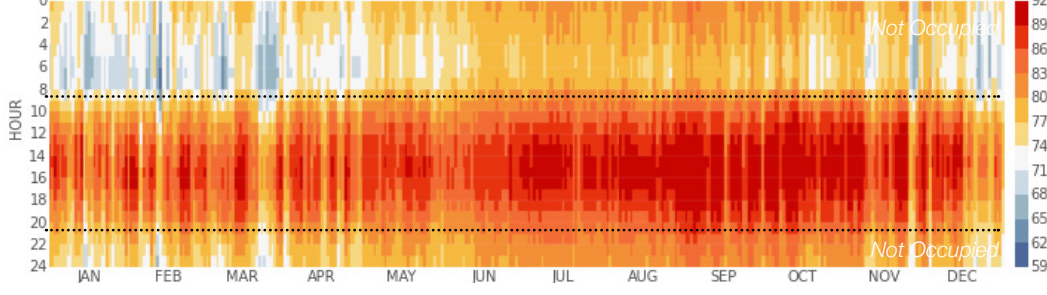
Operative temperature for bottom floor



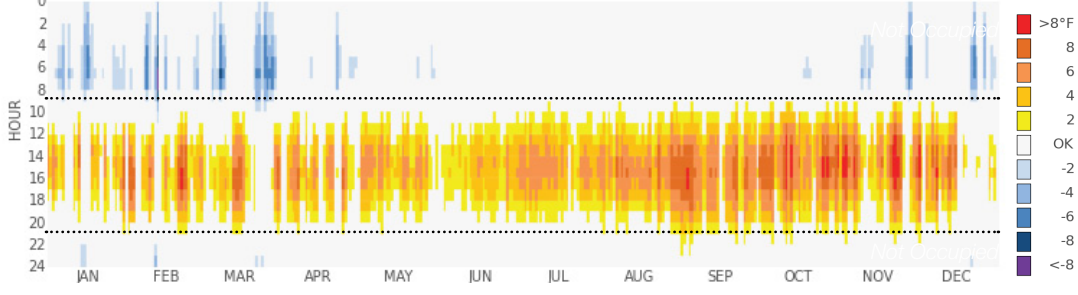
Degrees from comfort for bottom floor



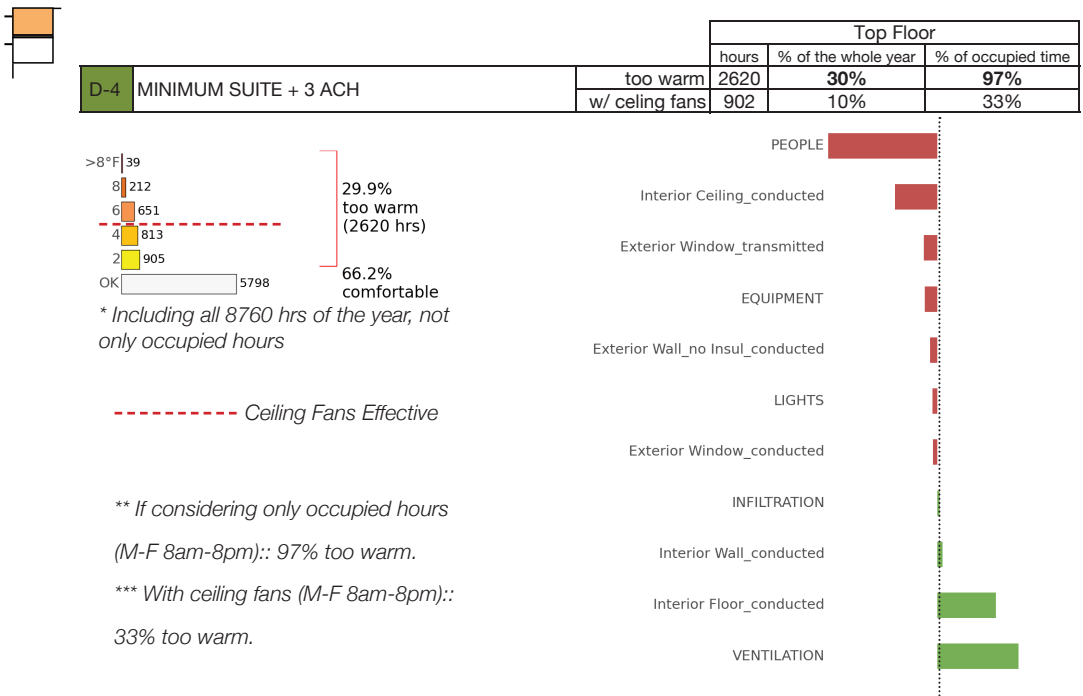
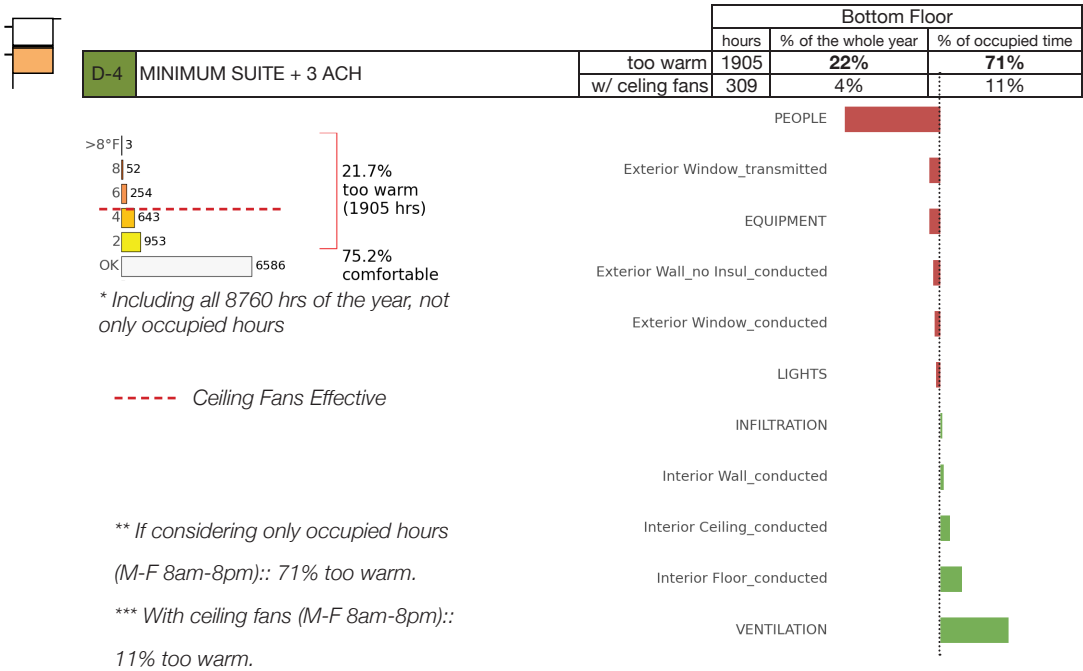
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.a.D.4 Classroom Analysis:: South Facing (Continued)



Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

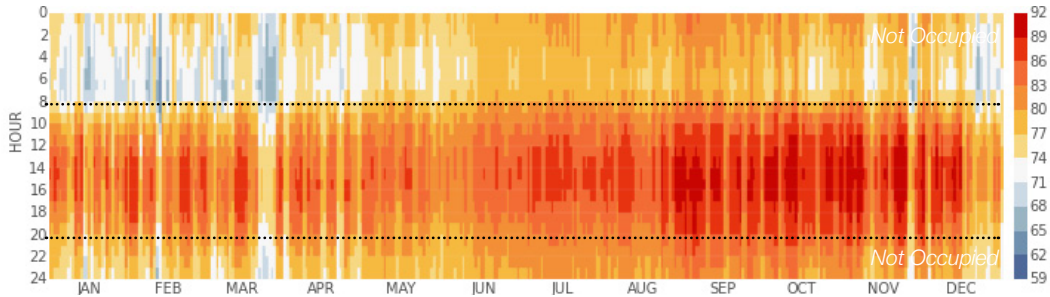


C.3.a.D. VENTILATION PARAMETRICS

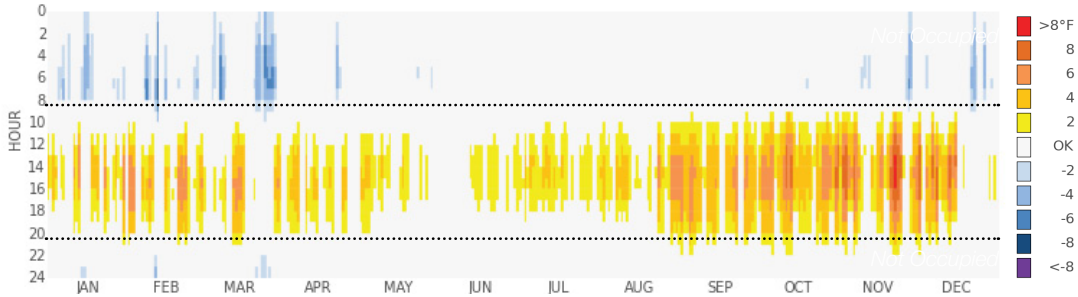
C.3.a.D.5 IMPROVED SUITE +3ACH



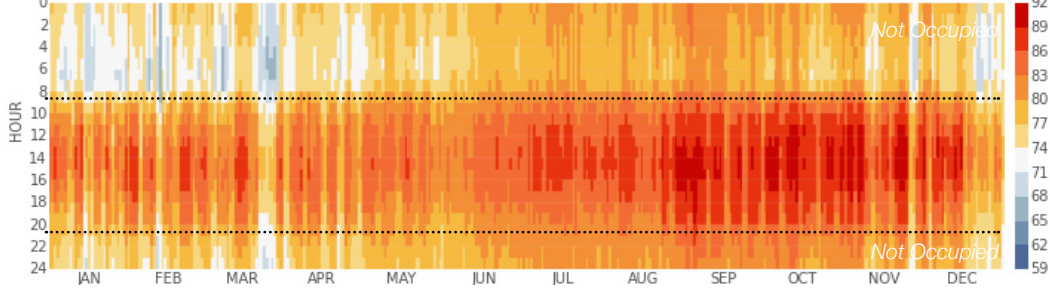
Operative temperature for bottom floor



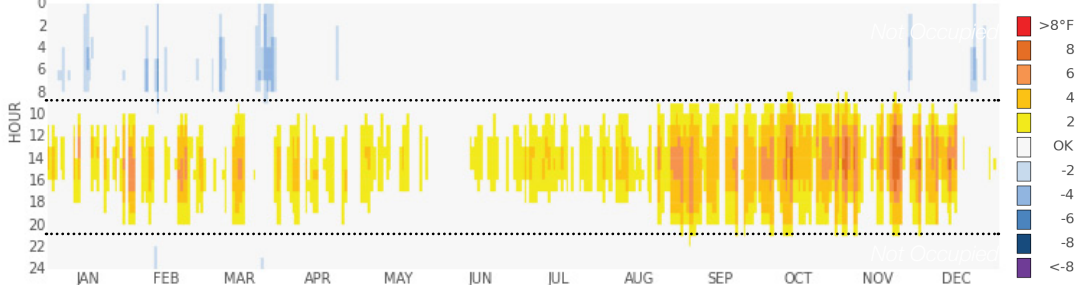
Degrees from comfort for bottom floor



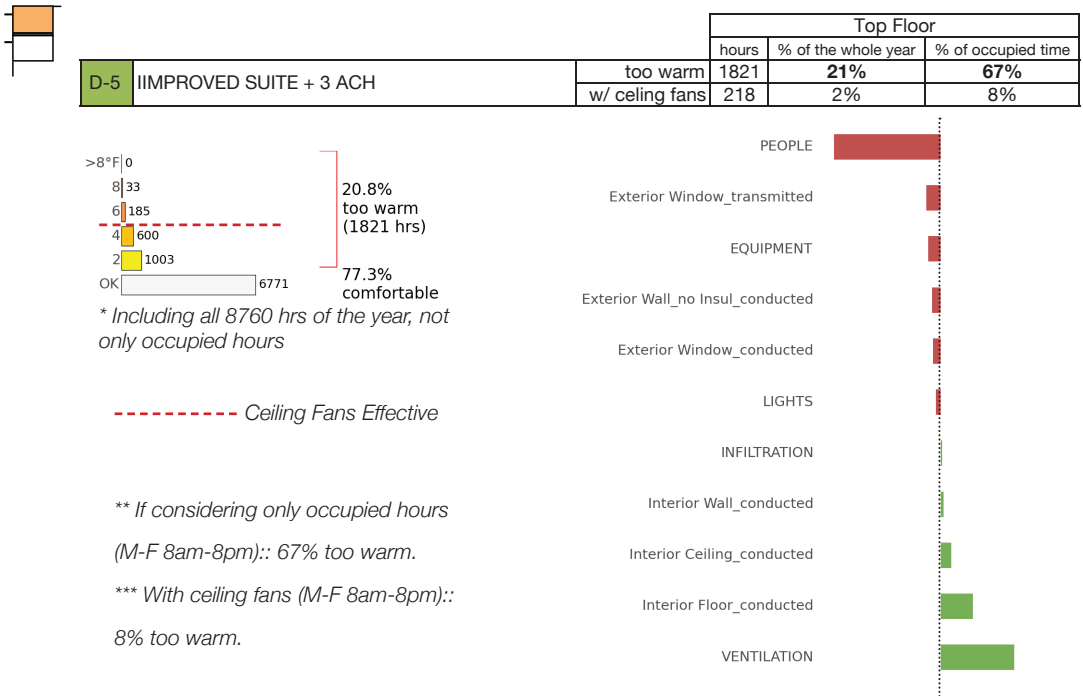
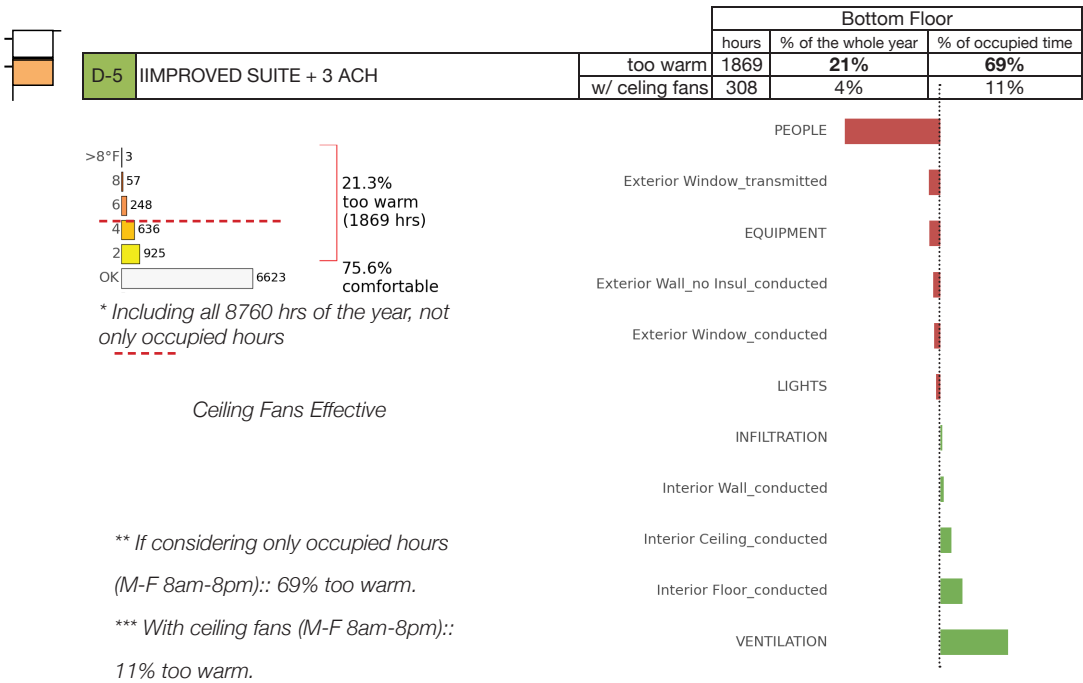
Operative temperature for top floor



Degrees from comfort for top floor



AAdd/C.3.a.D.5 Classroom Analysis:: South Facing (Continued)



Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

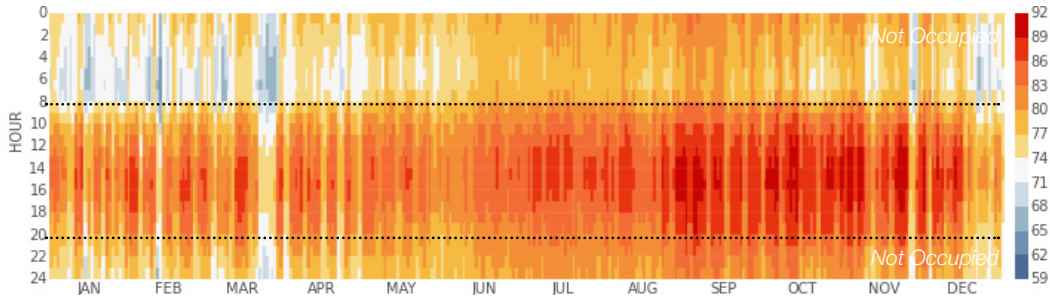


C.3.a.D. VENTILATION PARAMETRICS

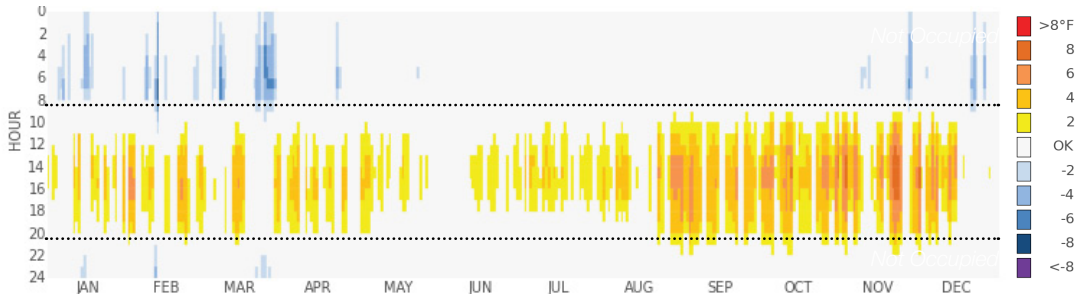
C.3.a.D.6 CODE SUITE +3ACH



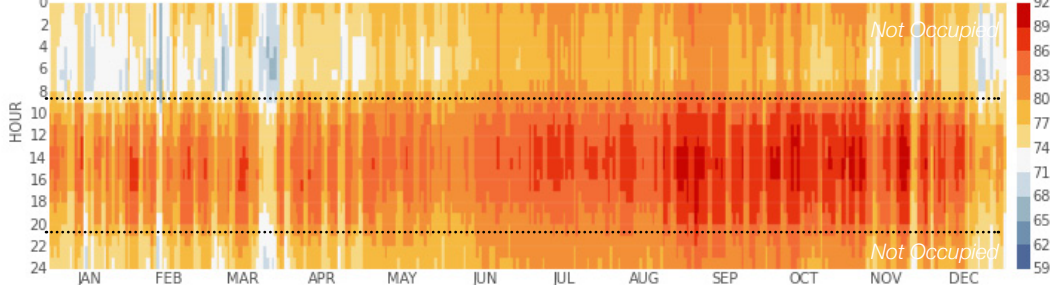
Operative temperature for bottom floor



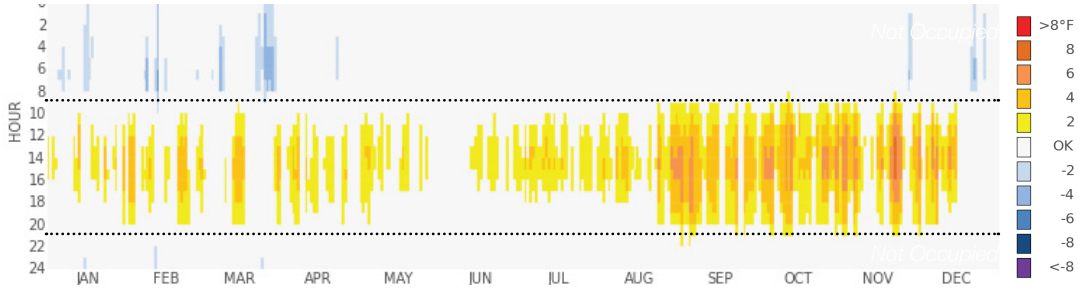
Degrees from comfort for bottom floor



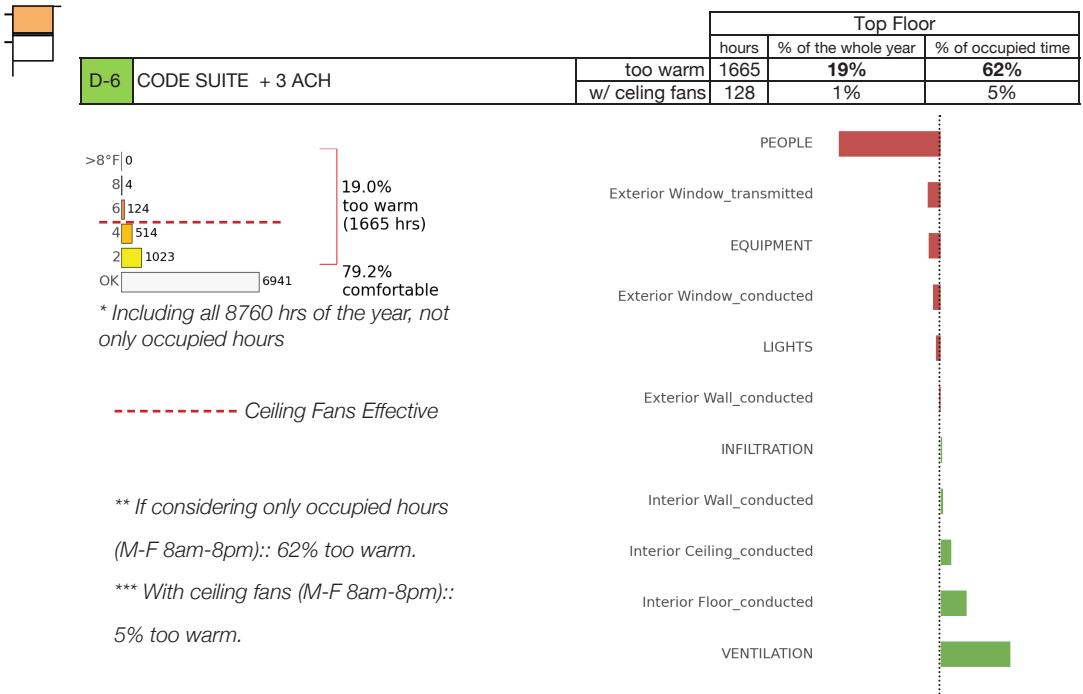
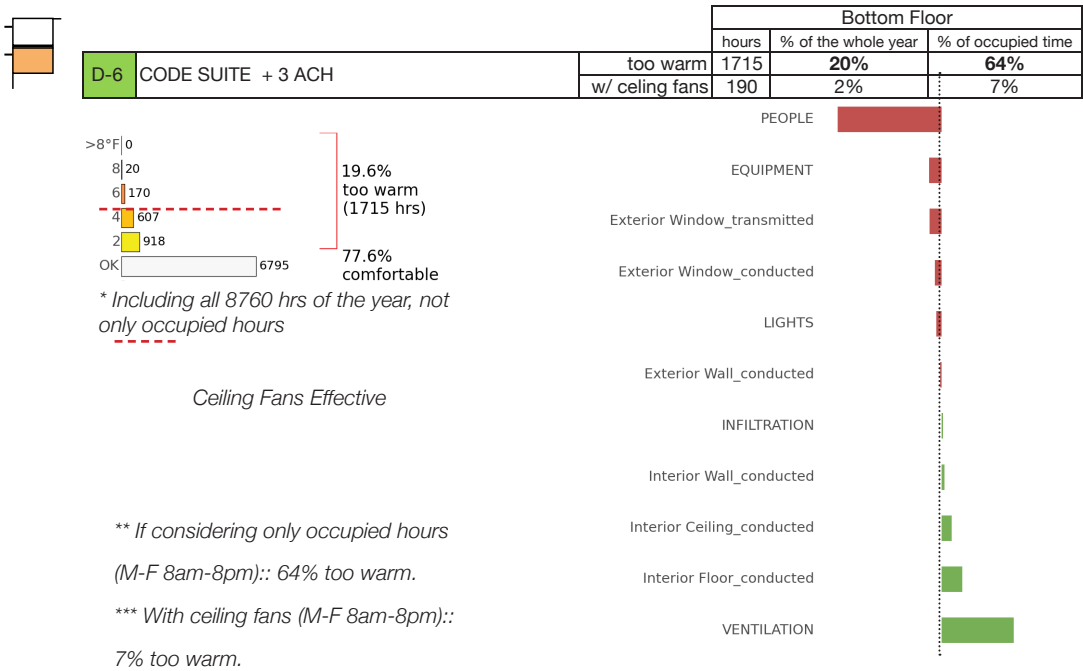
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.a.D.6 Classroom Analysis:: South Facing (Continued)



Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

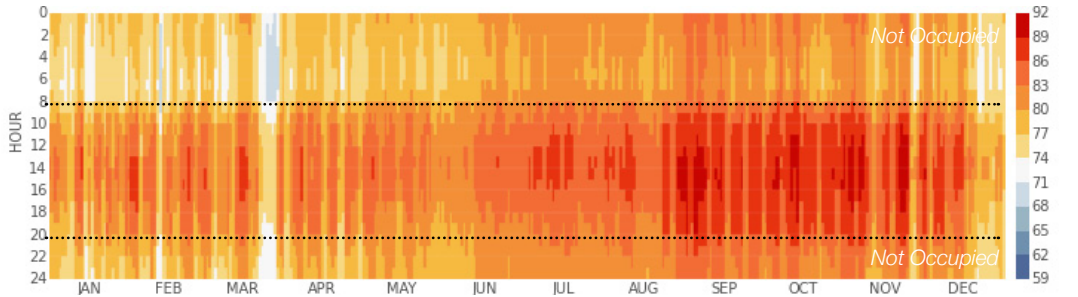
C.3.a.E. THERMAL MASS:: IDEAL SUITE



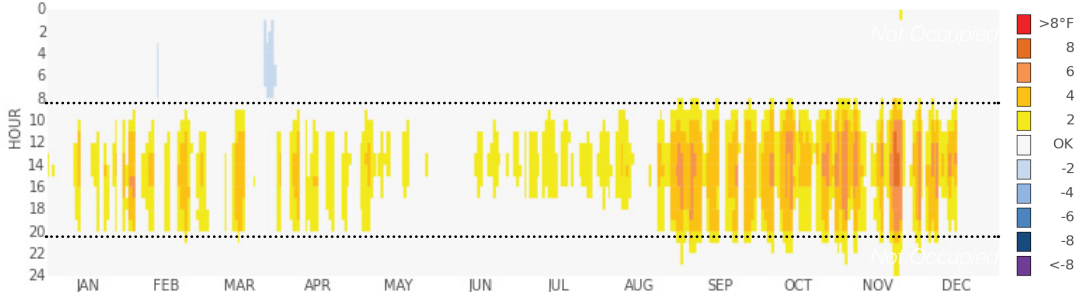
C.3.a.E.1 CODE SUITE + Thermal Mass



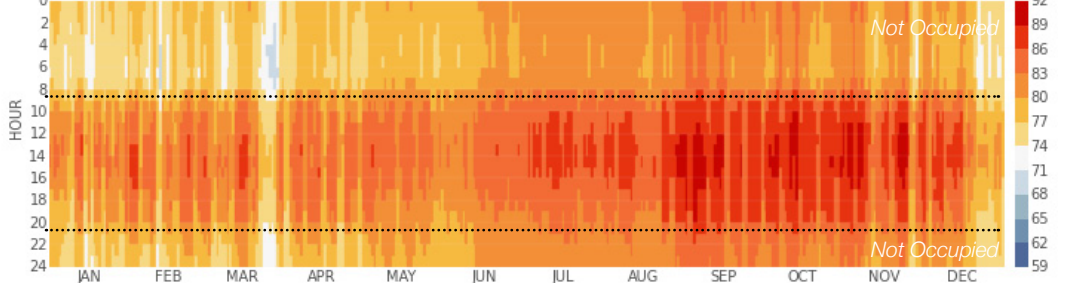
Operative temperature for bottom floor



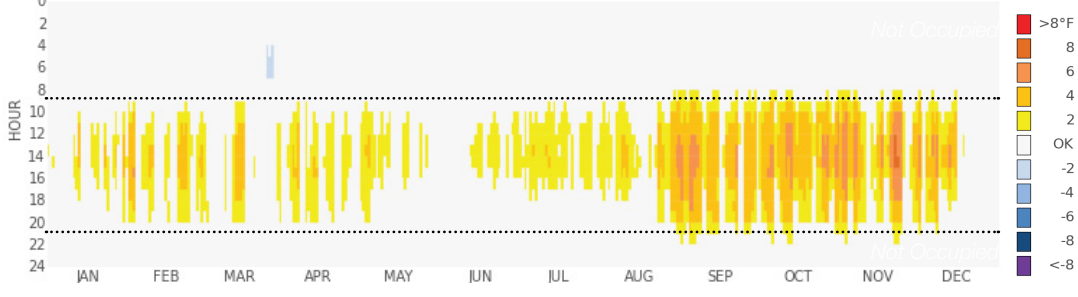
Degrees from comfort for bottom floor



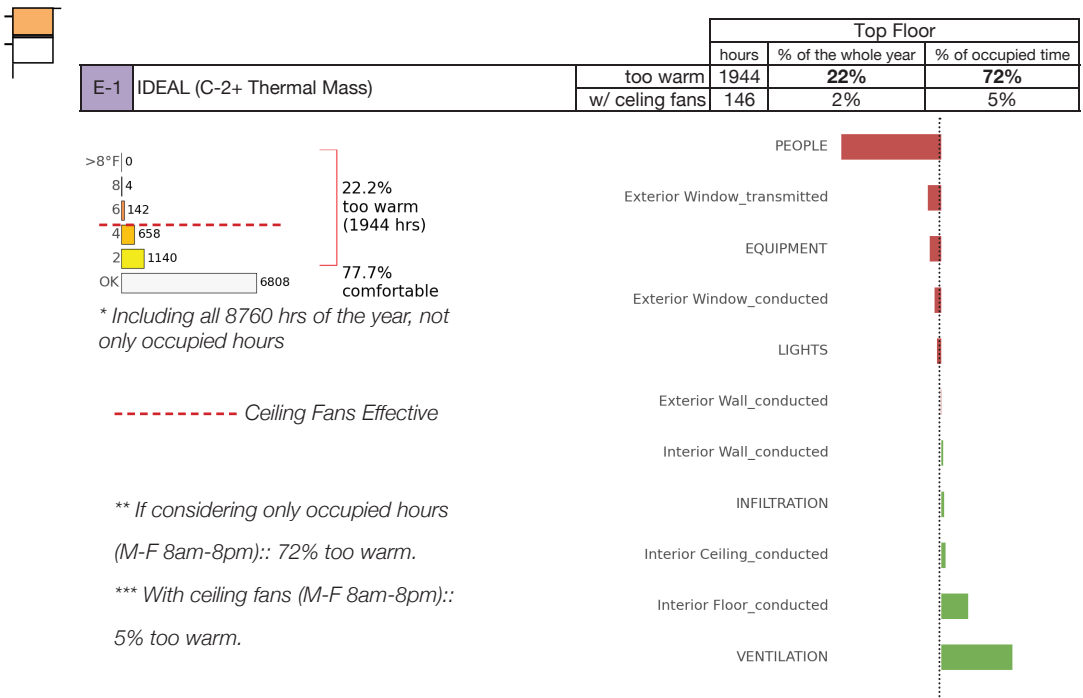
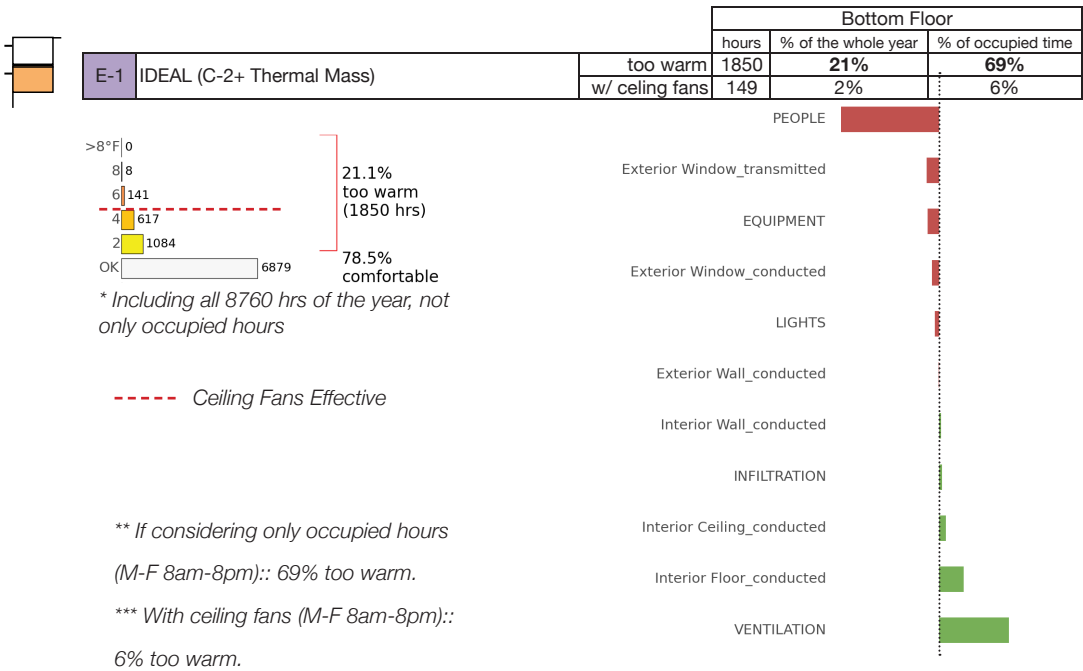
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.a.E.1 Classroom Analysis:: South Facing (Continued)



Add/C.3.a CLASSROOM ANALYSIS:: SOUTH FACING

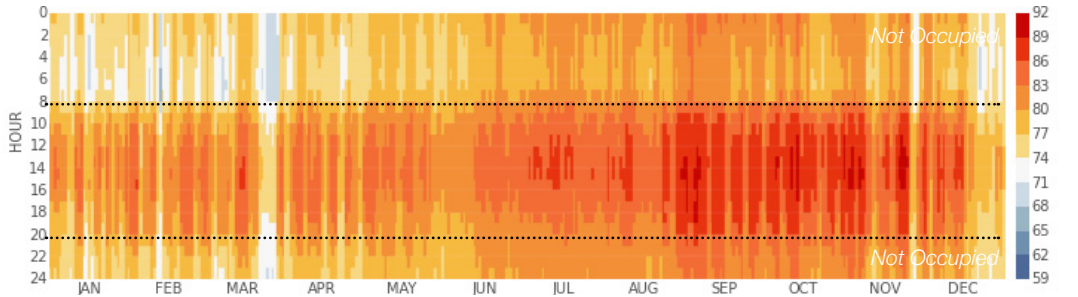
C.3.a.E. THERMAL MASS:: IDEAL SUITE



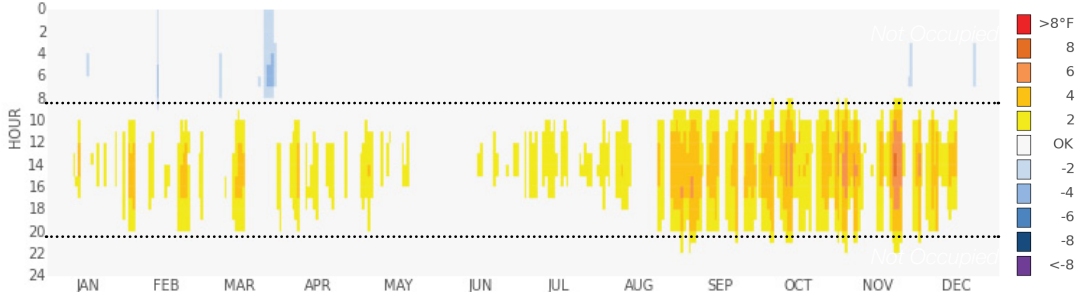
C.3.a.E.2 IDEAL SUITE + 2ACH



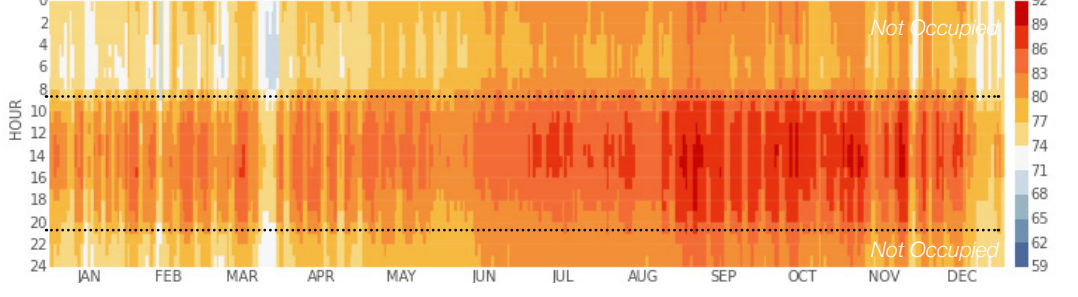
Operative temperature for bottom floor



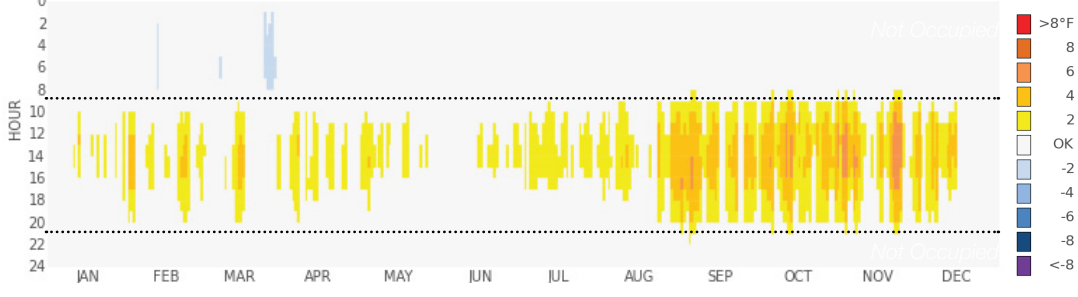
Degrees from comfort for bottom floor



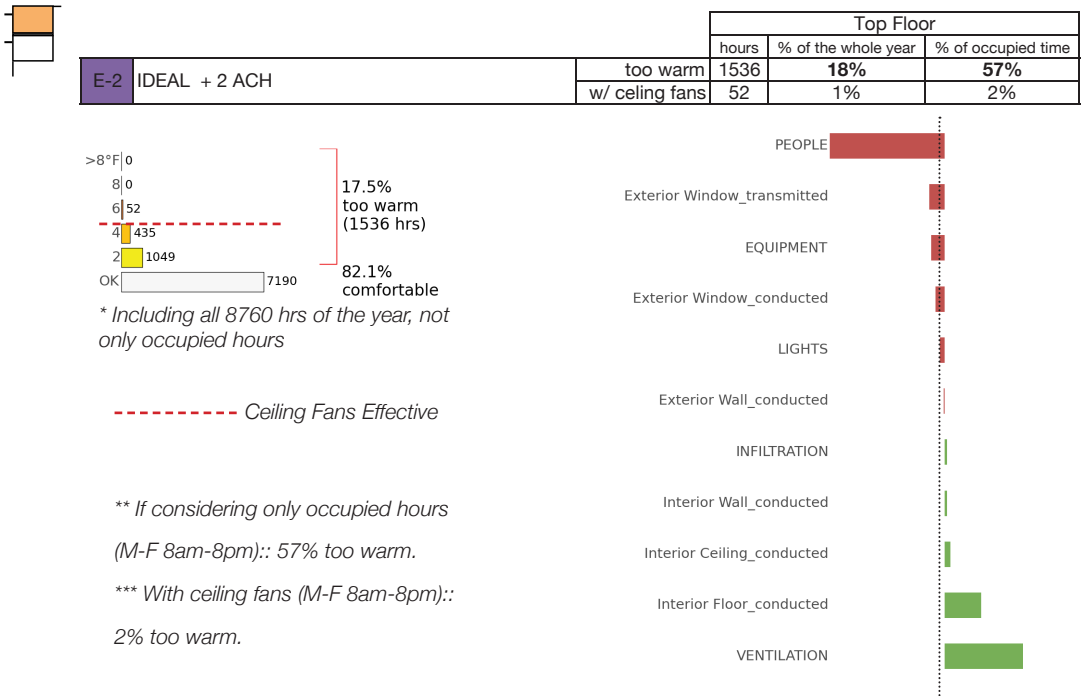
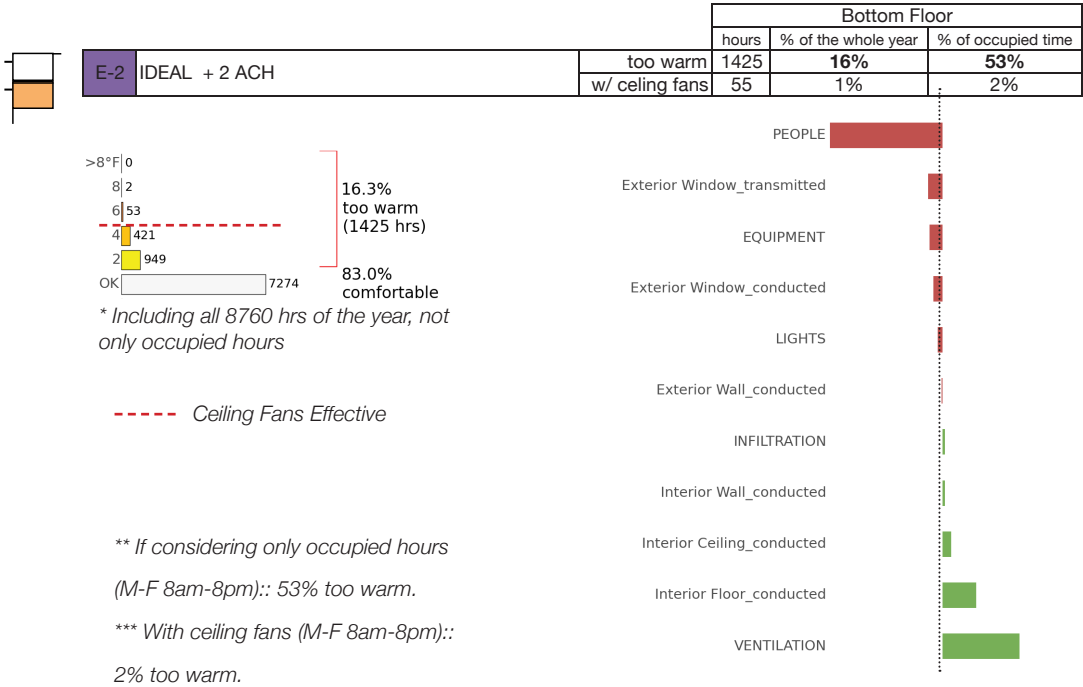
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.a.E.2 Classroom Analysis:: South Facing (Continued)



Add/C.3.b CLASSROOM ANALYSIS:: NORTH FACING

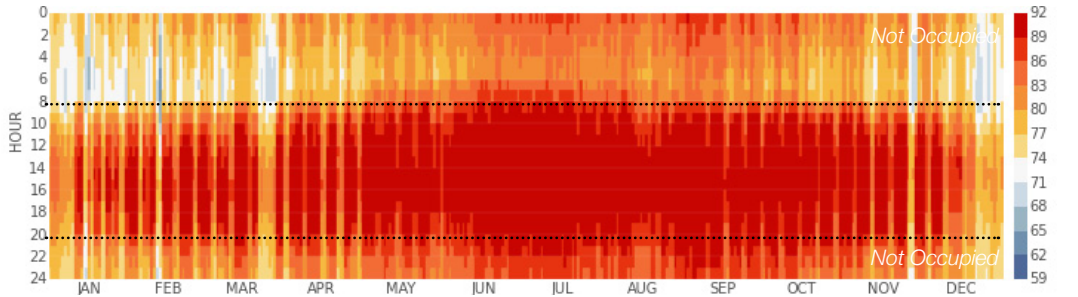


C.3.b.0. TYPICAL EXISTING

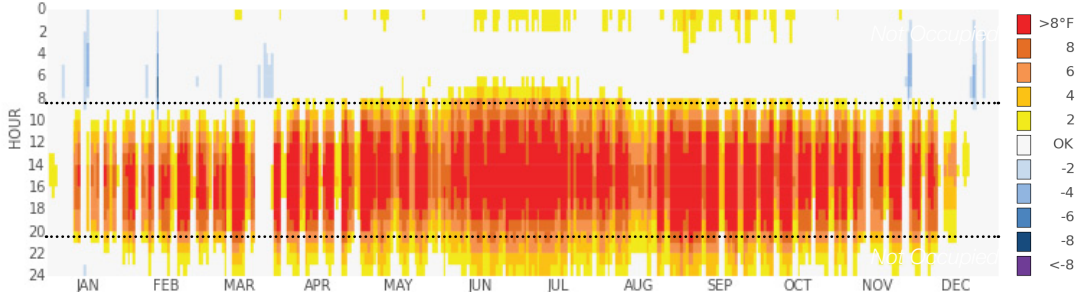
No Insulation in Opaque Surfaces and Single Pane Glass



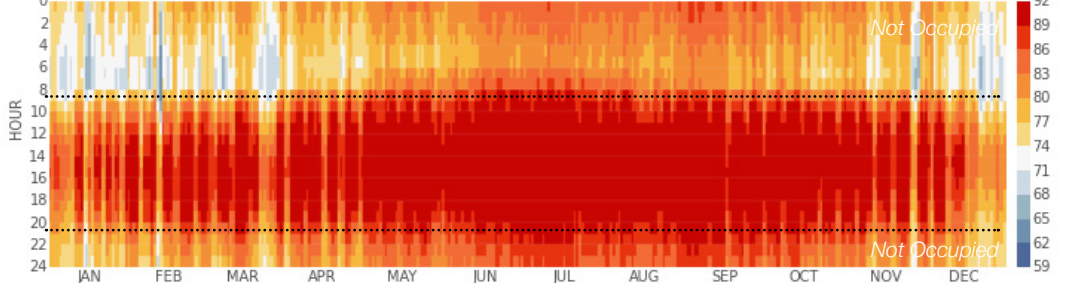
Operative temperature for bottom floor



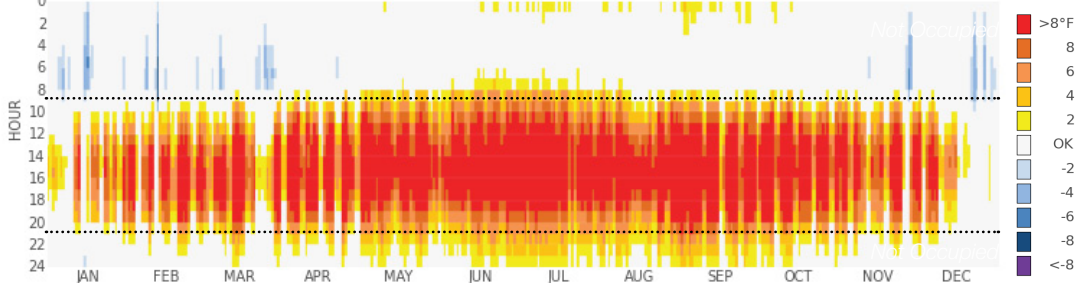
Degrees from comfort for bottom floor



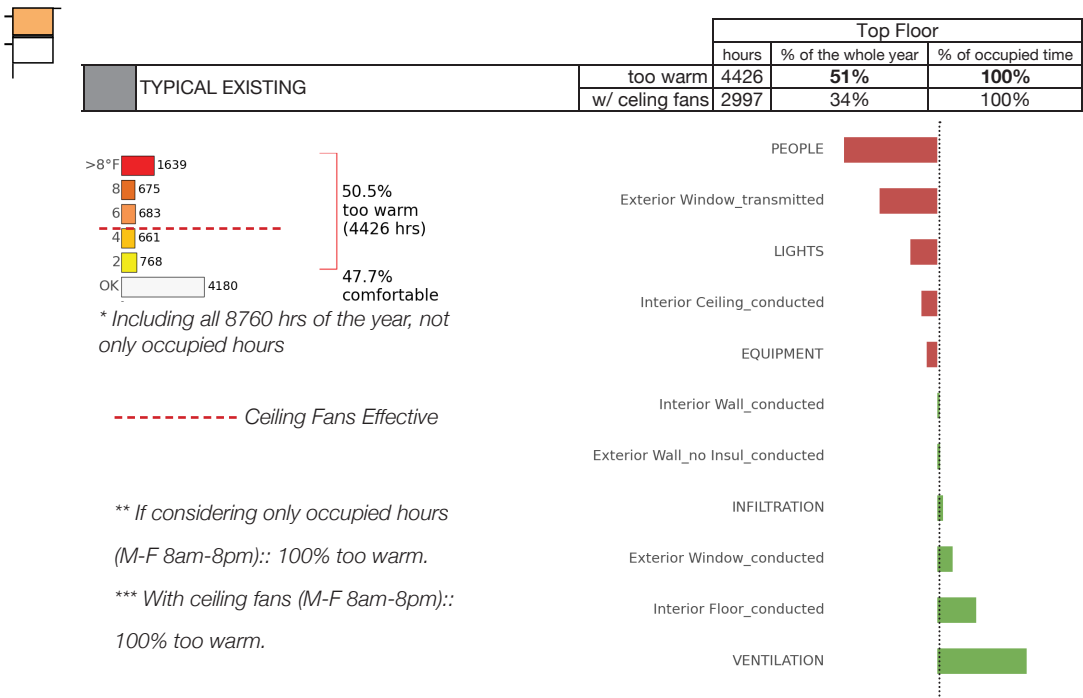
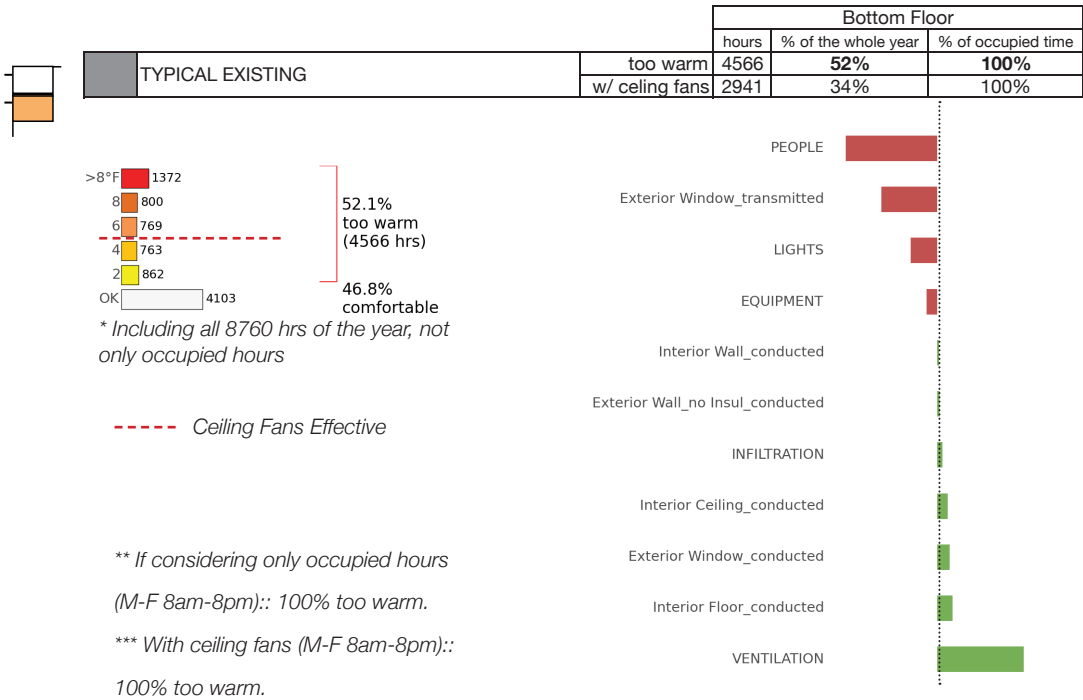
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.b.0 Classroom Analysis:: North Facing (Continued)



Add/C.3.b CLASSROOM ANALYSIS:: NORTH FACING

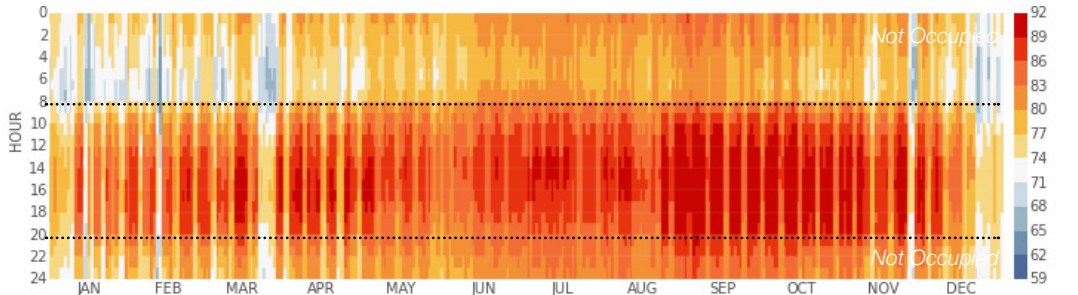


C.3.b.1. TYPICAL WITH WINDOW IMPROVEMENTS

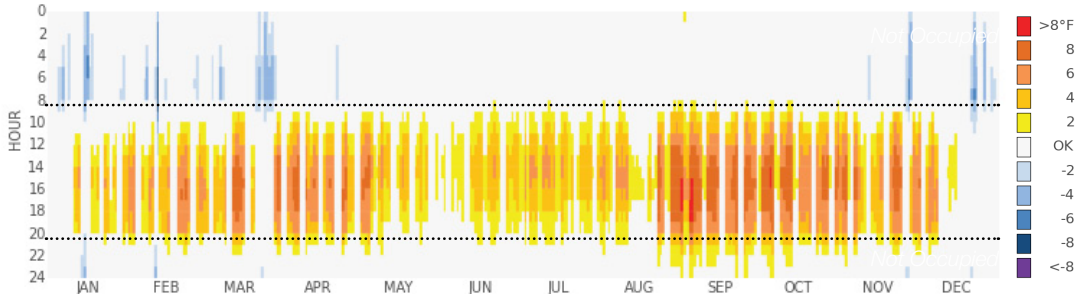
Equal to TYPICAL + 1ACH + Shading + IECC 2015 Windows



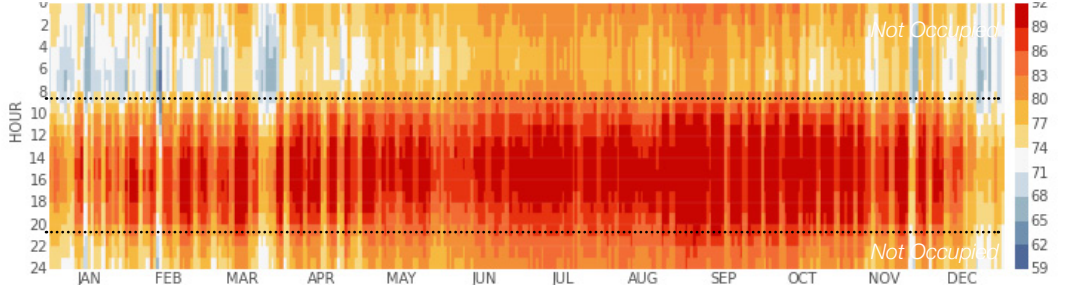
Operative temperature for bottom floor



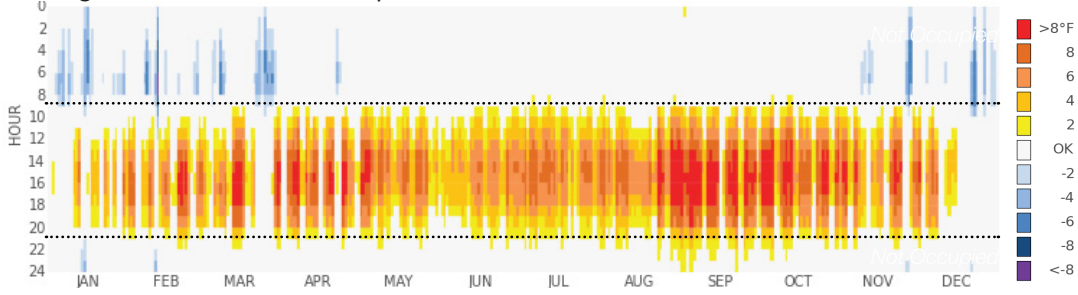
Degrees from comfort for bottom floor



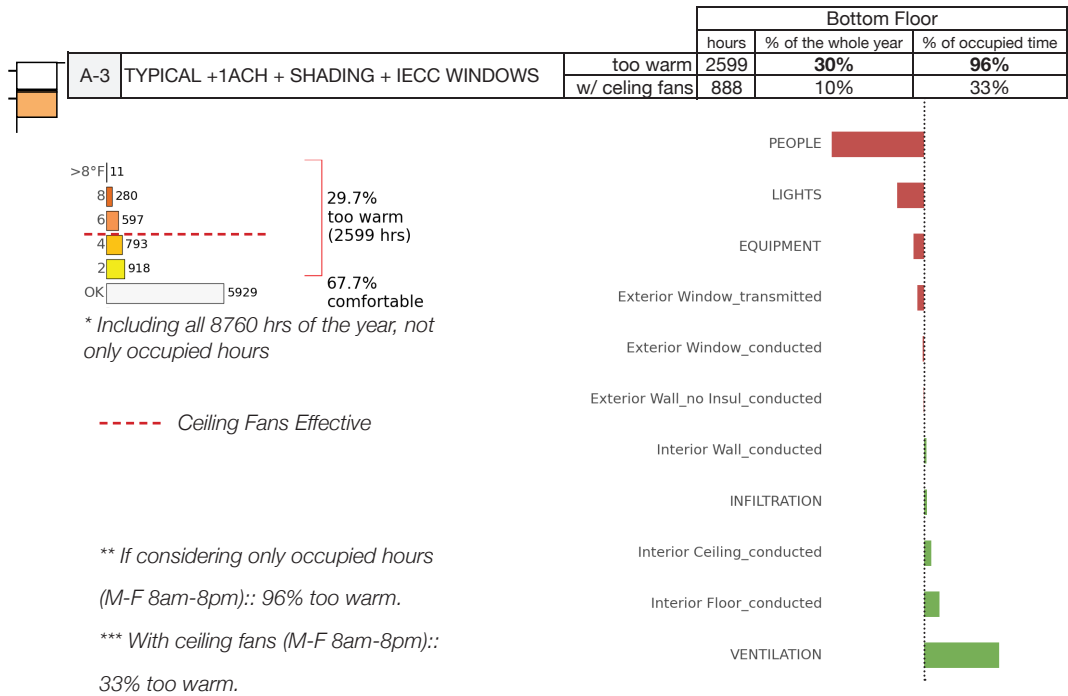
Operative temperature for top floor



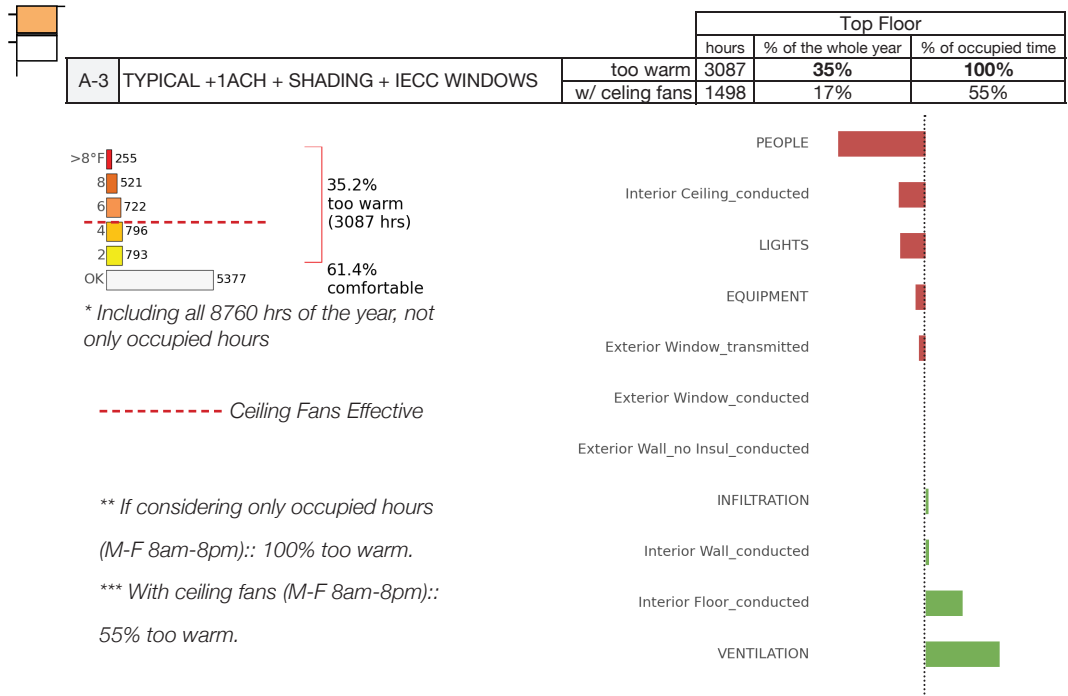
Degrees from comfort for top floor



Add/C.3.b.1 Classroom Analysis:: North Facing (Continued)



A-3 TYPICAL +1ACH +



Add/C.3.b CLASSROOM ANALYSIS:: NORTH FACING

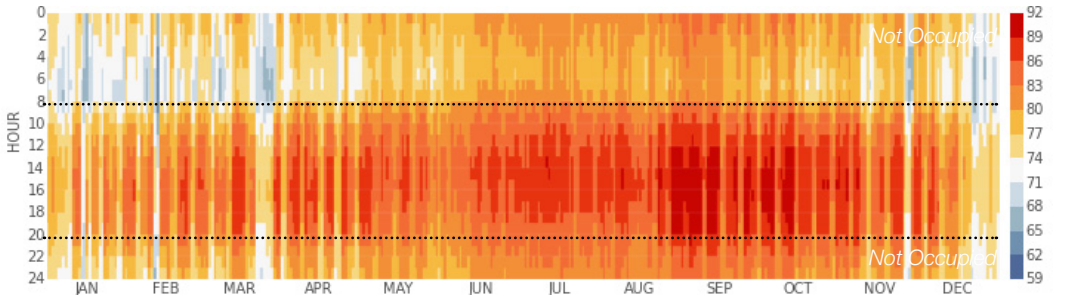


C.3.b.2. MINIMUM SUITE

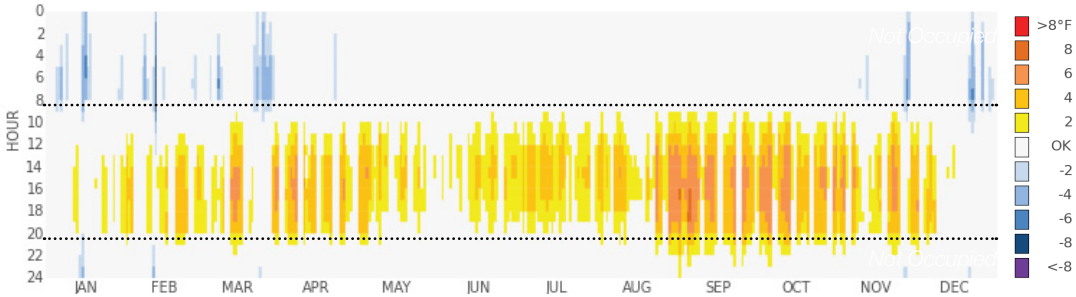
Equal to TYPICAL + IECC Windows + Shading +lower LPD + Daylight Controls +1ACH



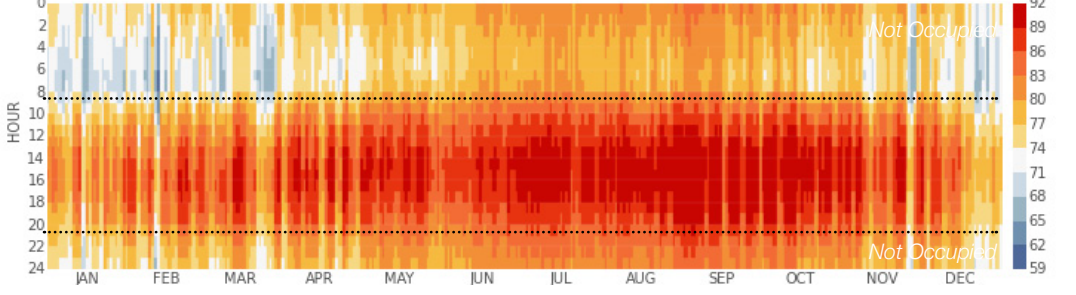
Operative temperature for bottom floor



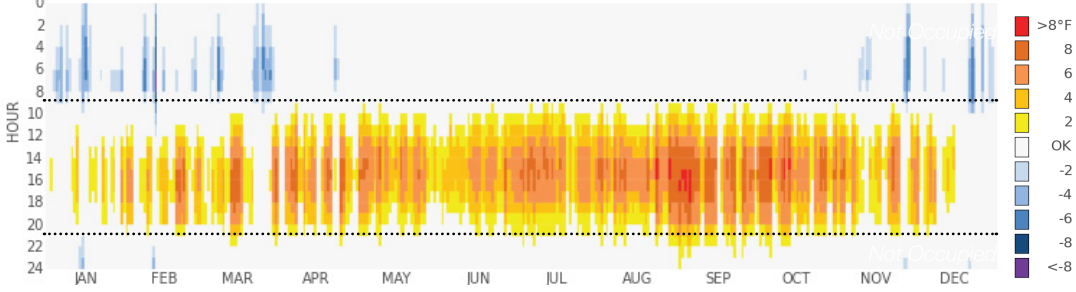
Degrees from comfort for bottom floor



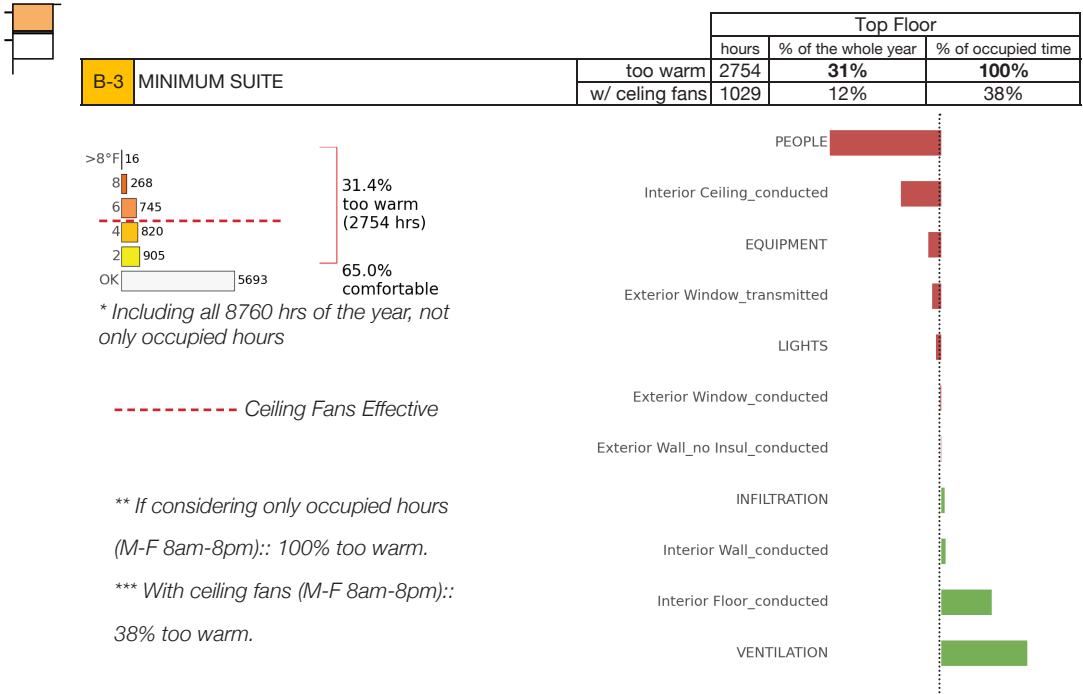
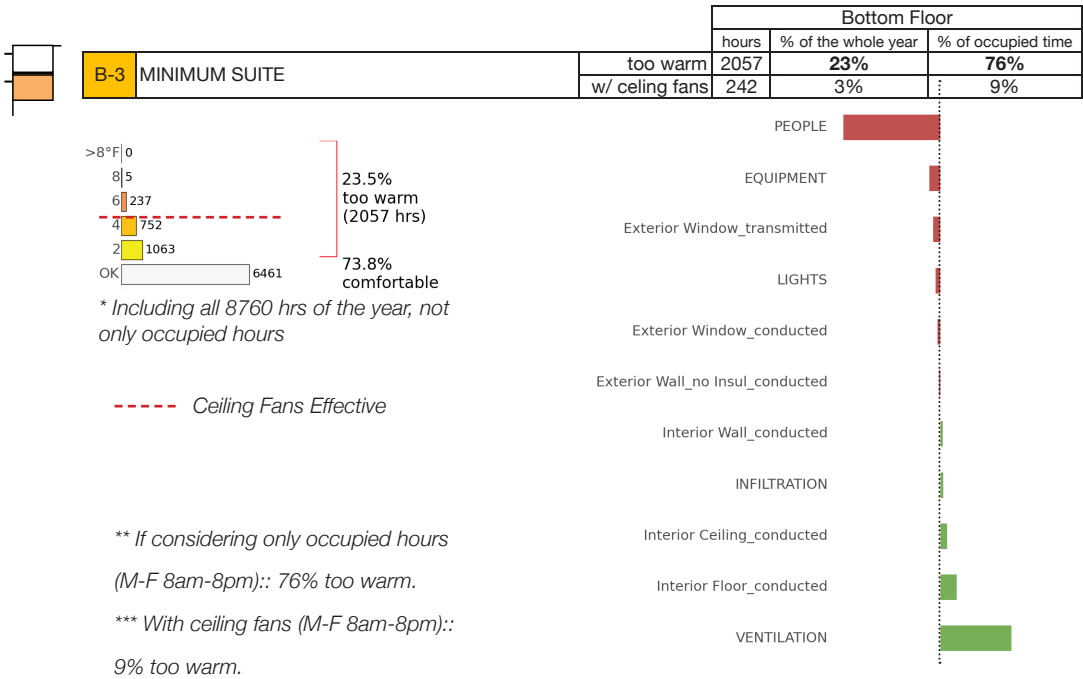
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.b.2 Classroom Analysis:: North Facing (Continued)



Add/C.3.b CLASSROOM ANALYSIS:: NORTH FACING

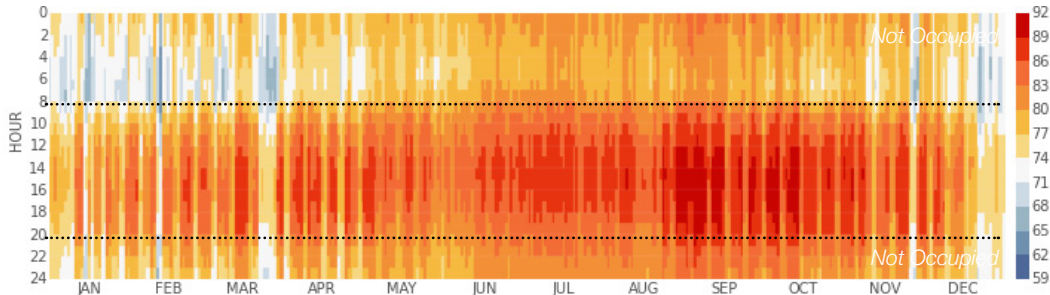


C.3.b.3. IMPROVED SUITE

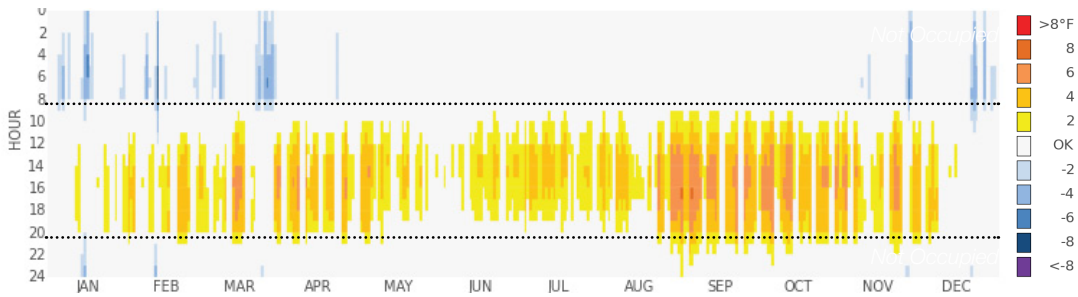
Equal to MINIMUM SUITE + IECC Roof



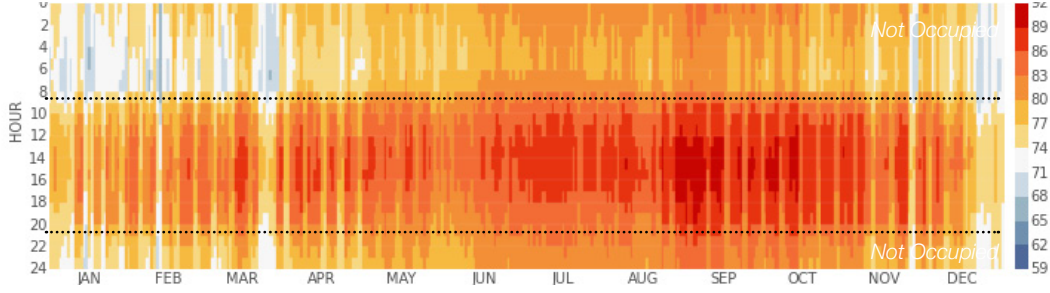
Operative temperature for bottom floor



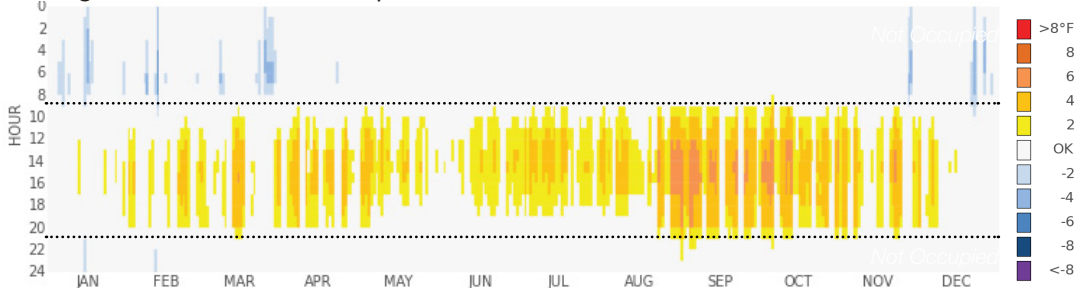
Degrees from comfort for bottom floor



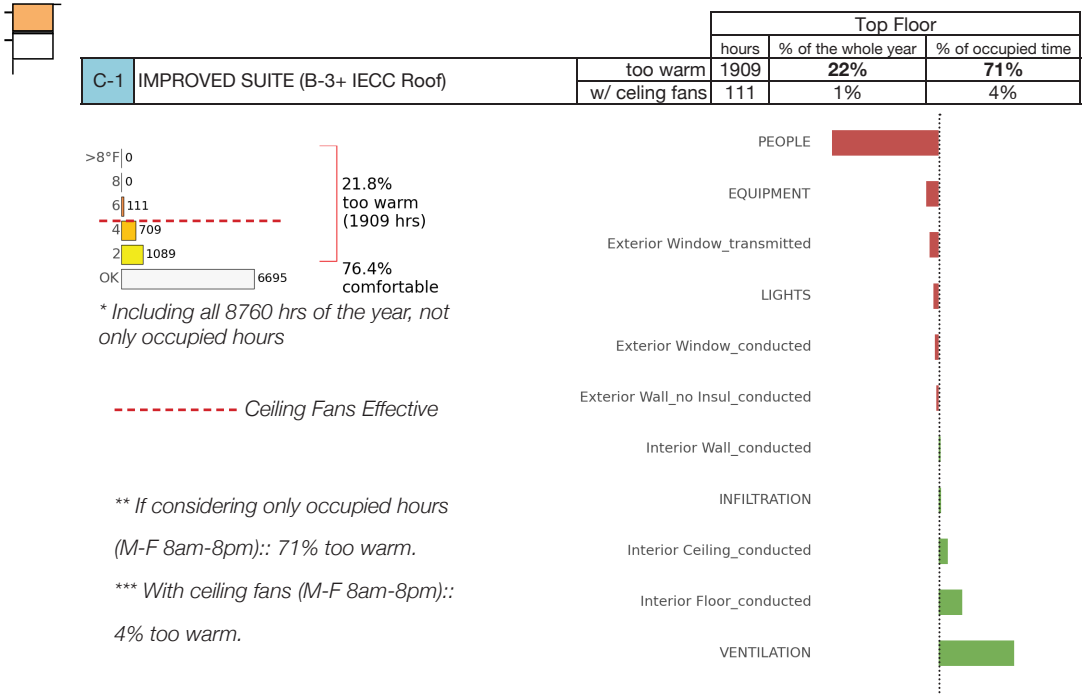
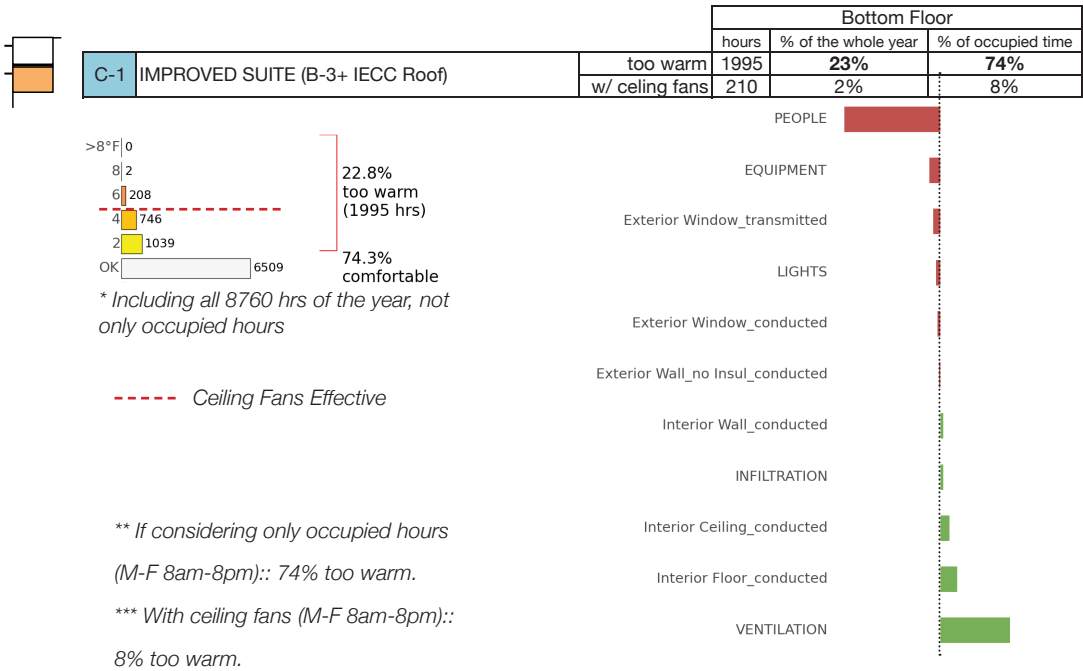
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.b.3 Classroom Analysis:: North Facing (Continued)



Add/C.3.b CLASSROOM ANALYSIS:: NORTH FACING

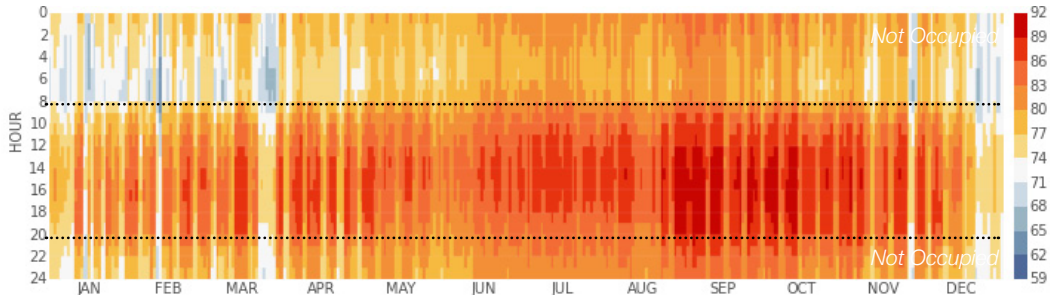


C.3.b.4. CODE SUITE

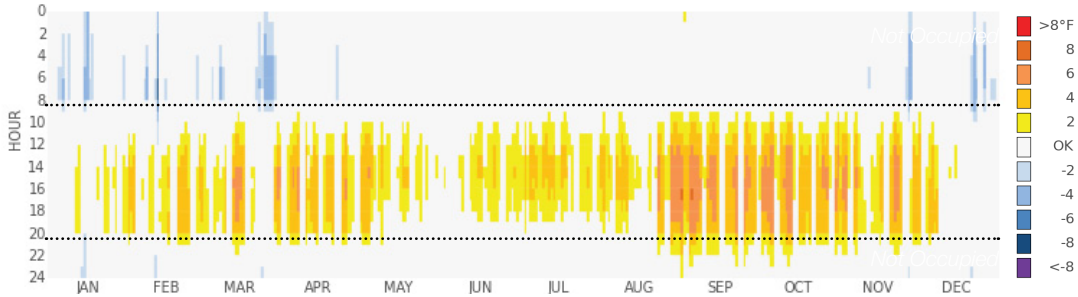
Equal to IMPROVED SUITE + IECC Walls



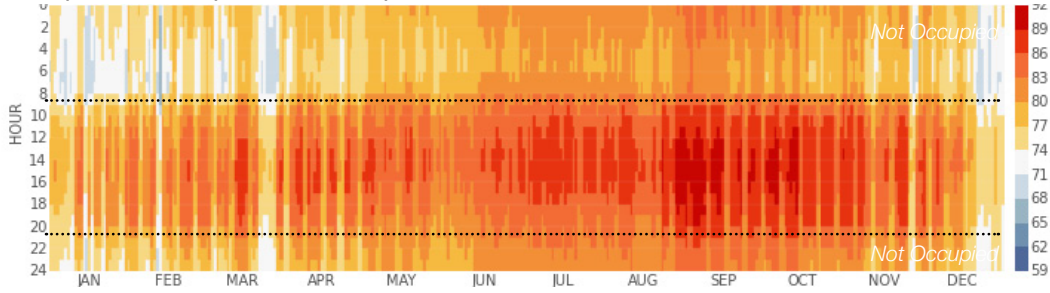
Operative temperature for bottom floor



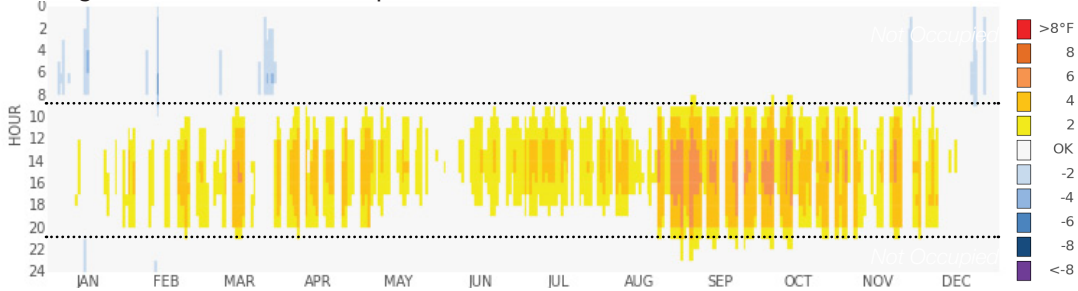
Degrees from comfort for bottom floor



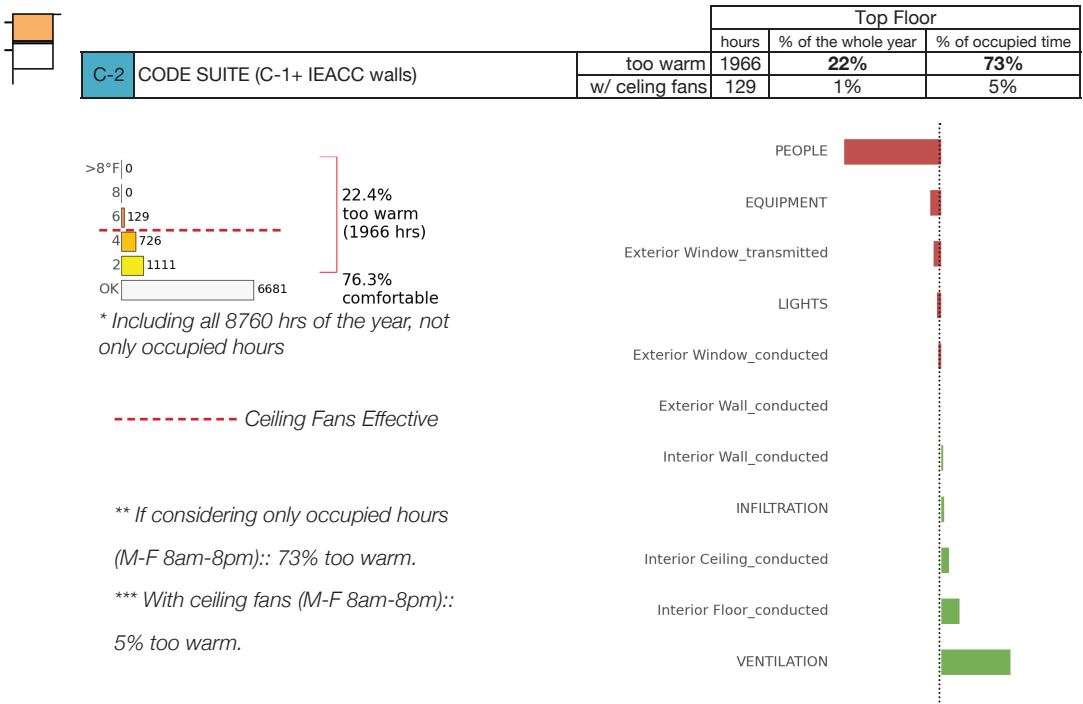
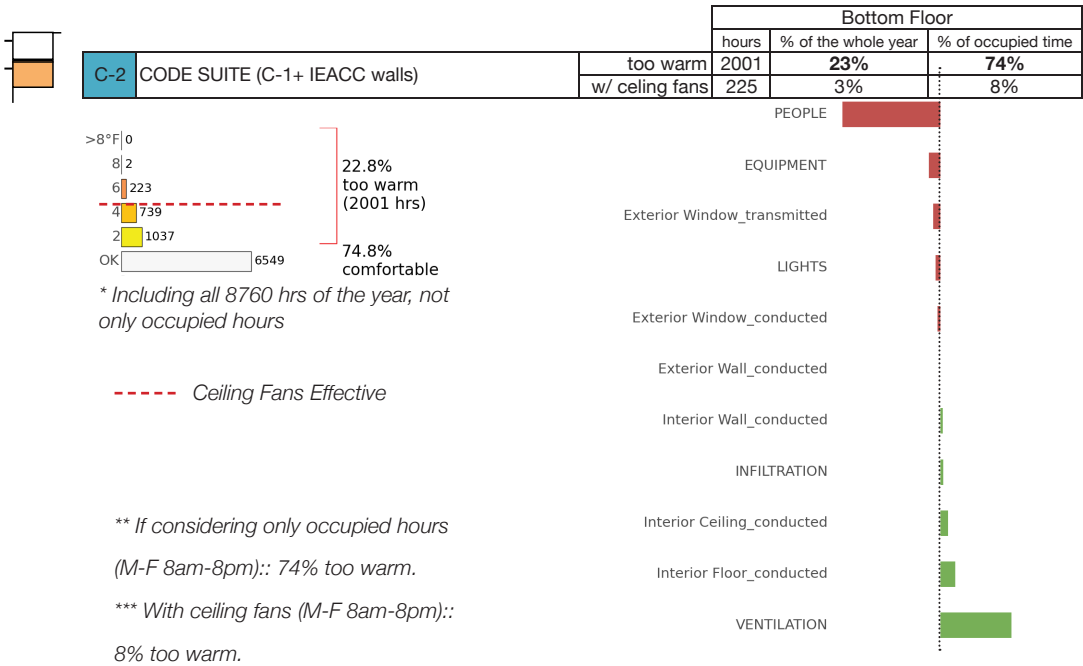
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.b.4 Classroom Analysis:: North Facing (Continued)



Add/C.3.b CLASSROOM ANALYSIS:: NORTH FACING

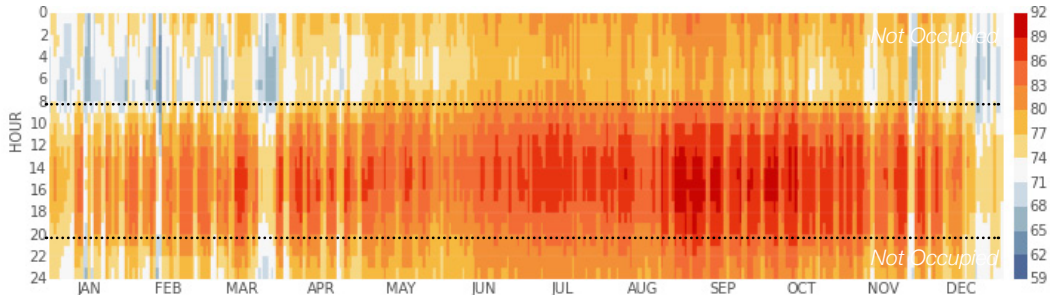


C.3.b.5. IMPROVED SUITE WITH VENTILATION

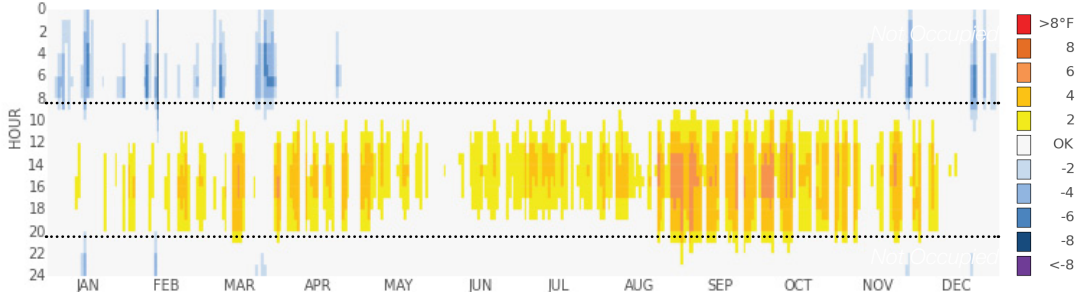
Equal to IMPROVED SUITE +2ACH



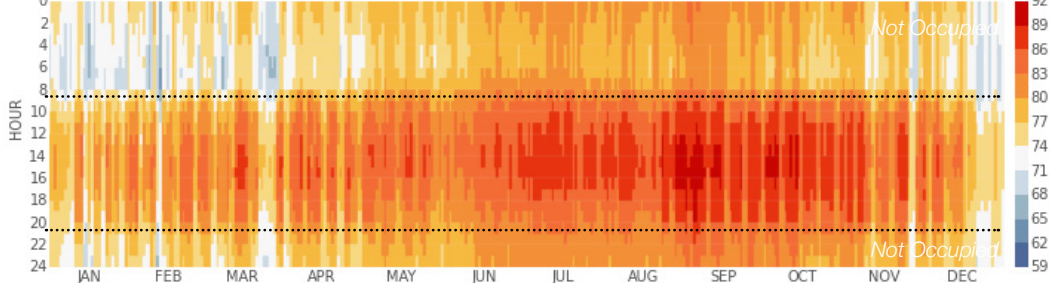
Operative temperature for bottom floor



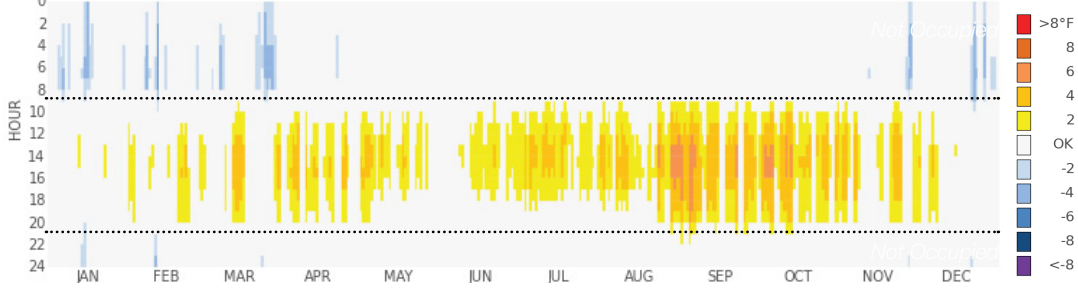
Degrees from comfort for bottom floor



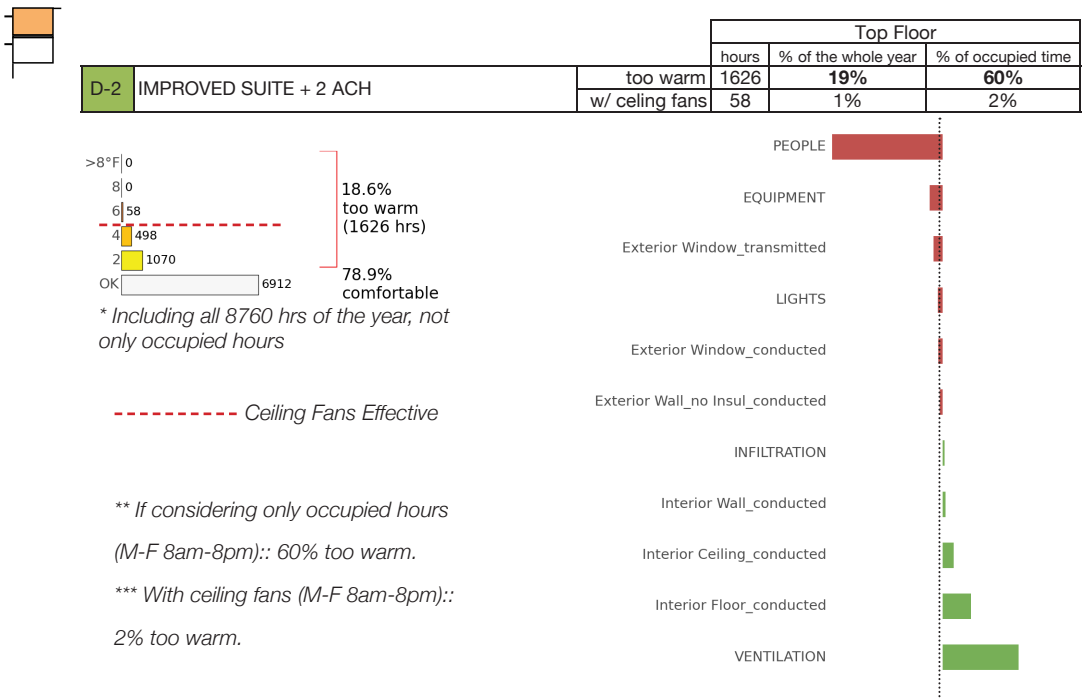
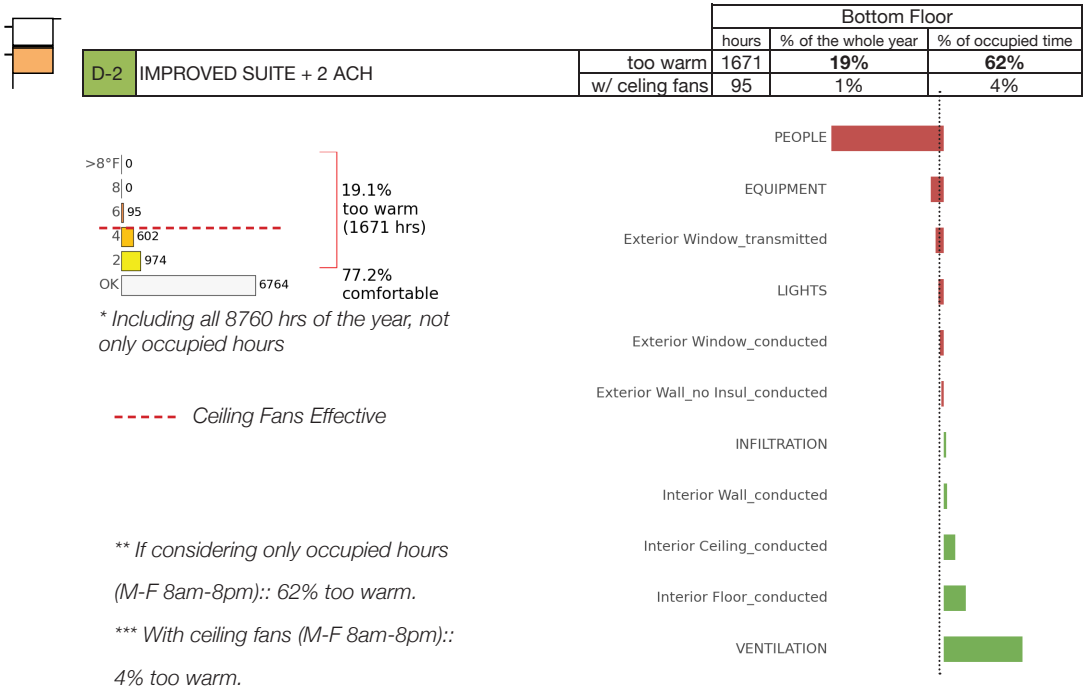
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.b.5 Classroom Analysis:: North Facing (Continued)



Add/C.3.b CLASSROOM ANALYSIS:: NORTH FACING

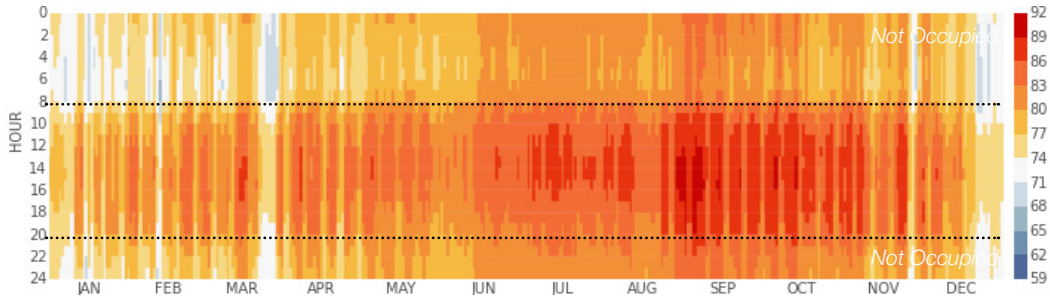


C.3.b.6. IDEAL SUITE

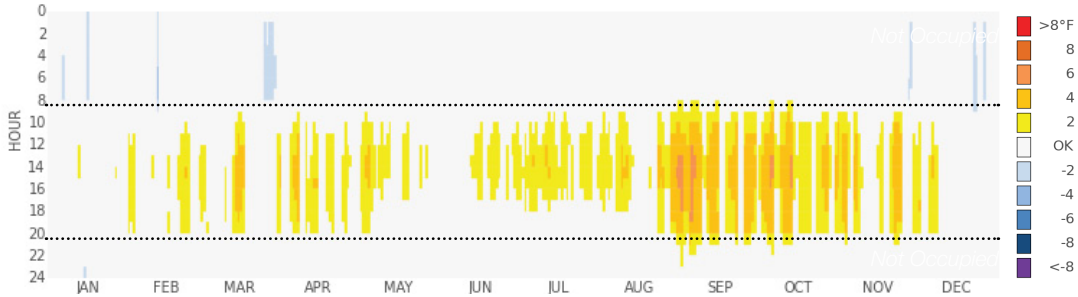
Equal to CODE SUITE + Thermal Mass



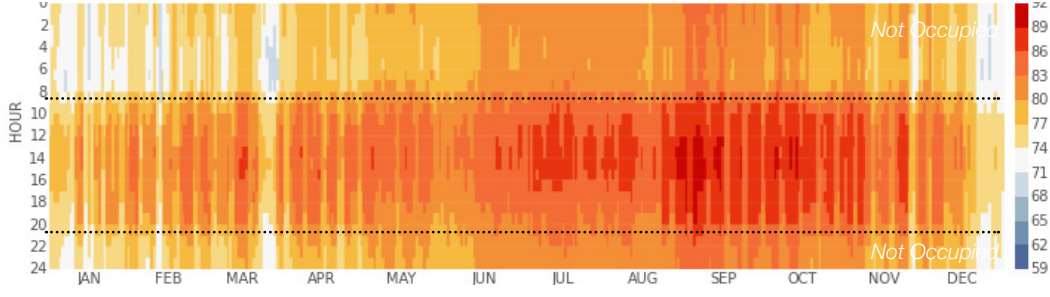
Operative temperature for bottom floor



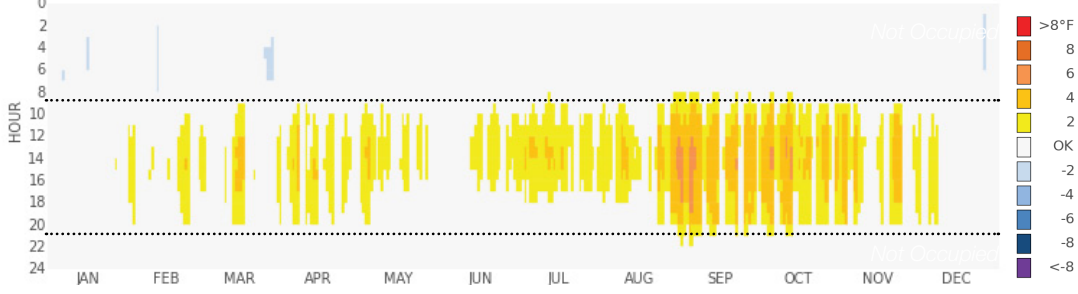
Degrees from comfort for bottom floor



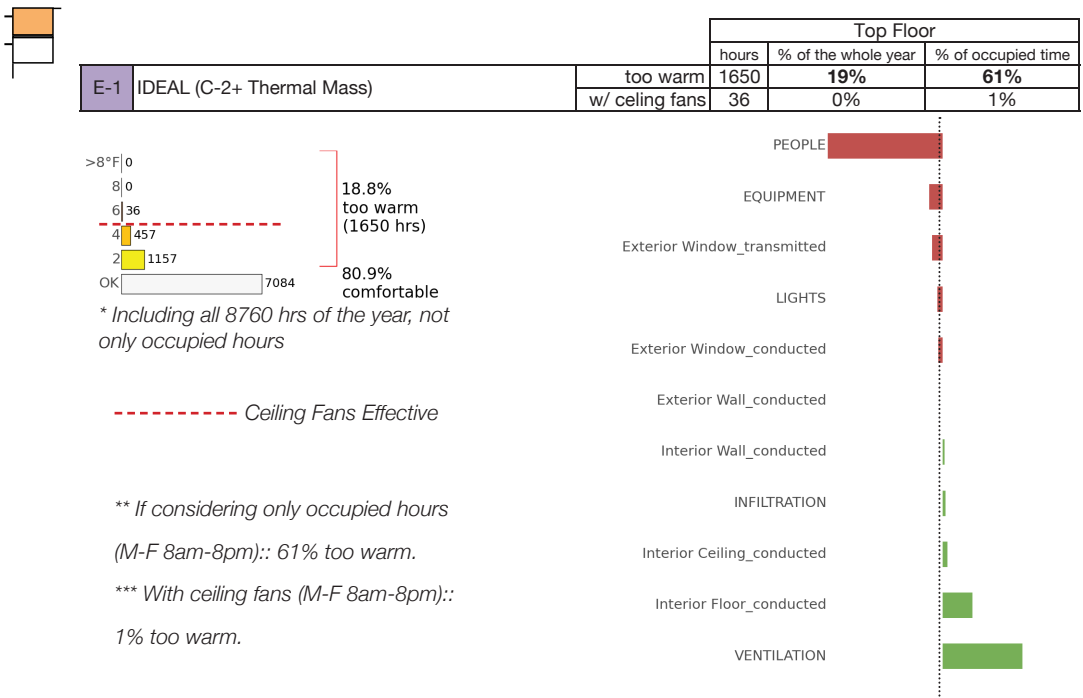
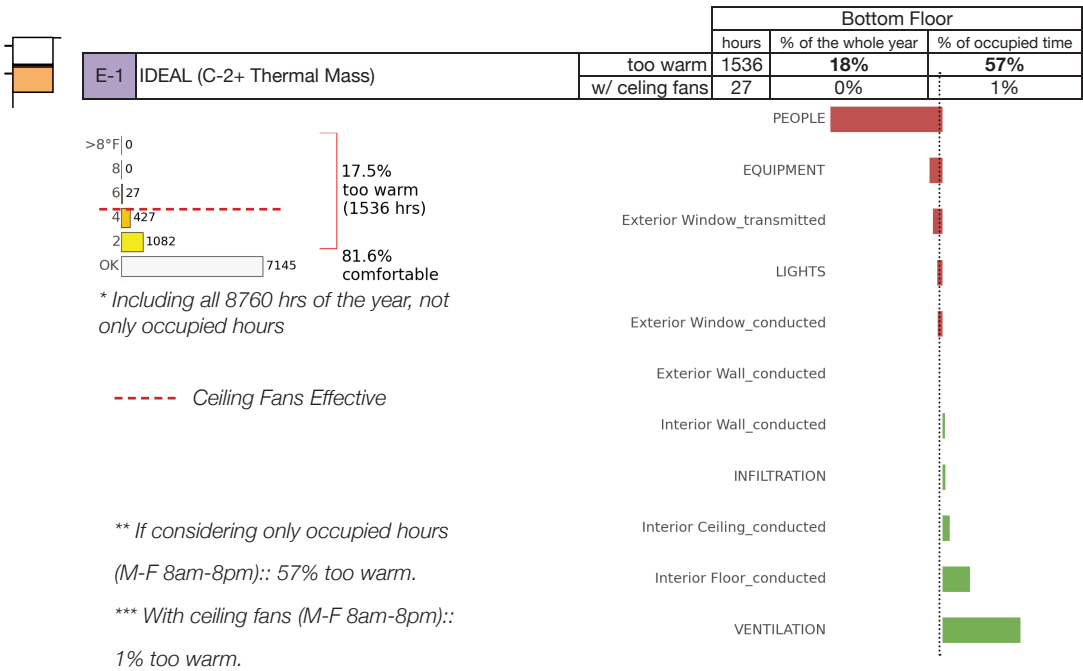
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.b.6 Classroom Analysis:: North Facing (Continued)



Add/C.3.b CLASSROOM ANALYSIS:: NORTH FACING

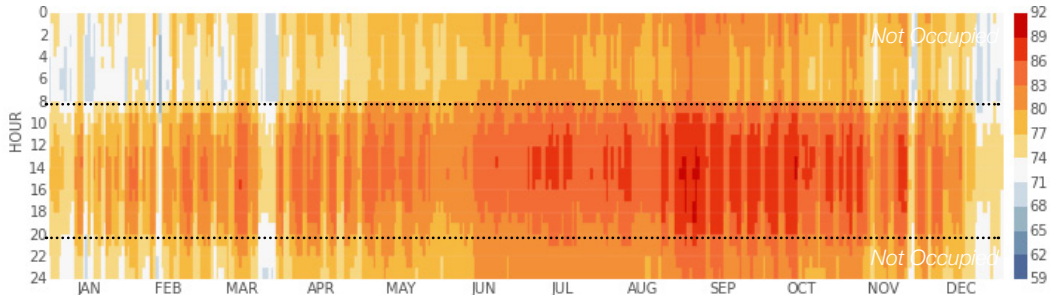


C.3.b.7. IDEAI SUITE WITH VENTILATION

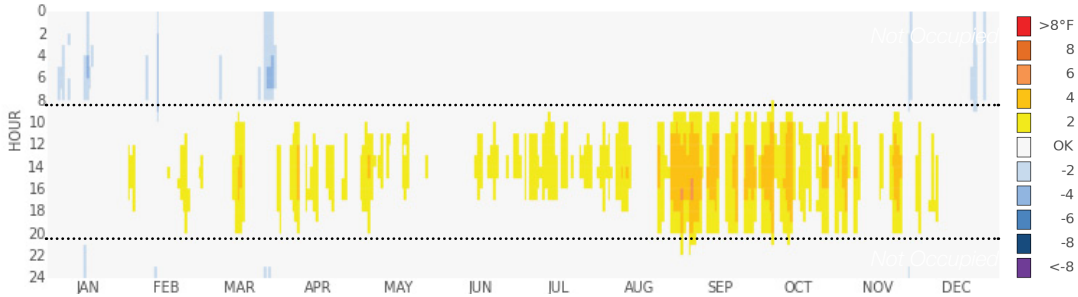
Equal to IDEAL SUITE + 2ACH



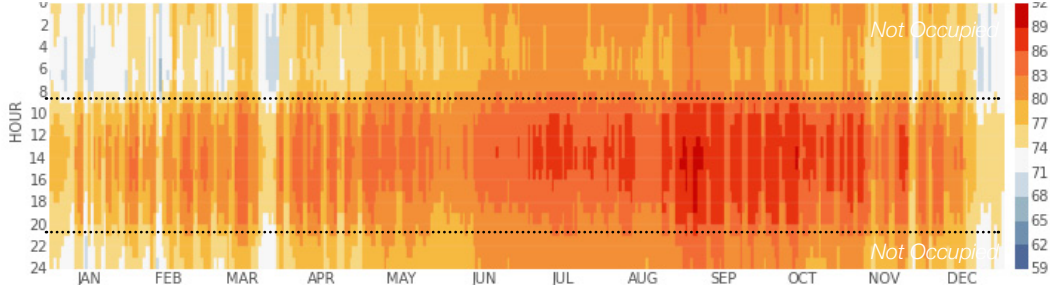
Operative temperature for bottom floor



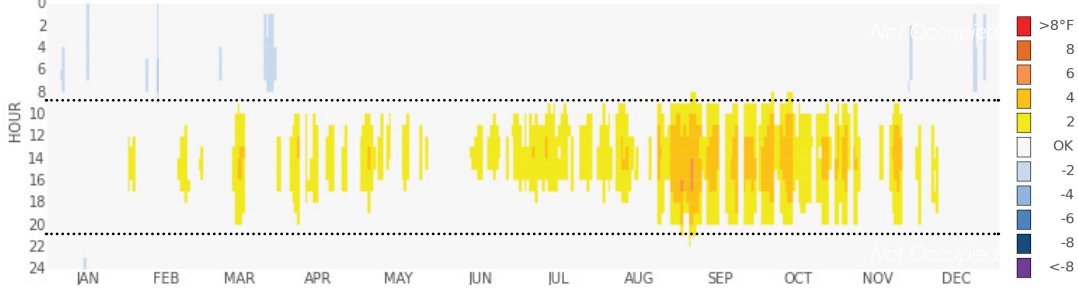
Degrees from comfort for bottom floor



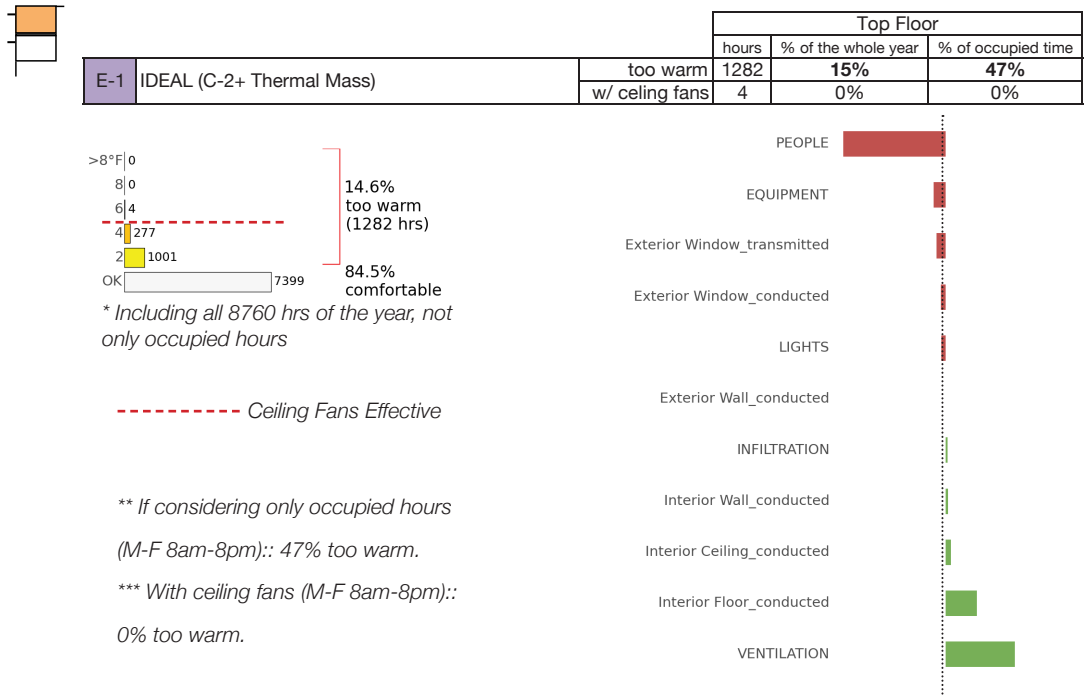
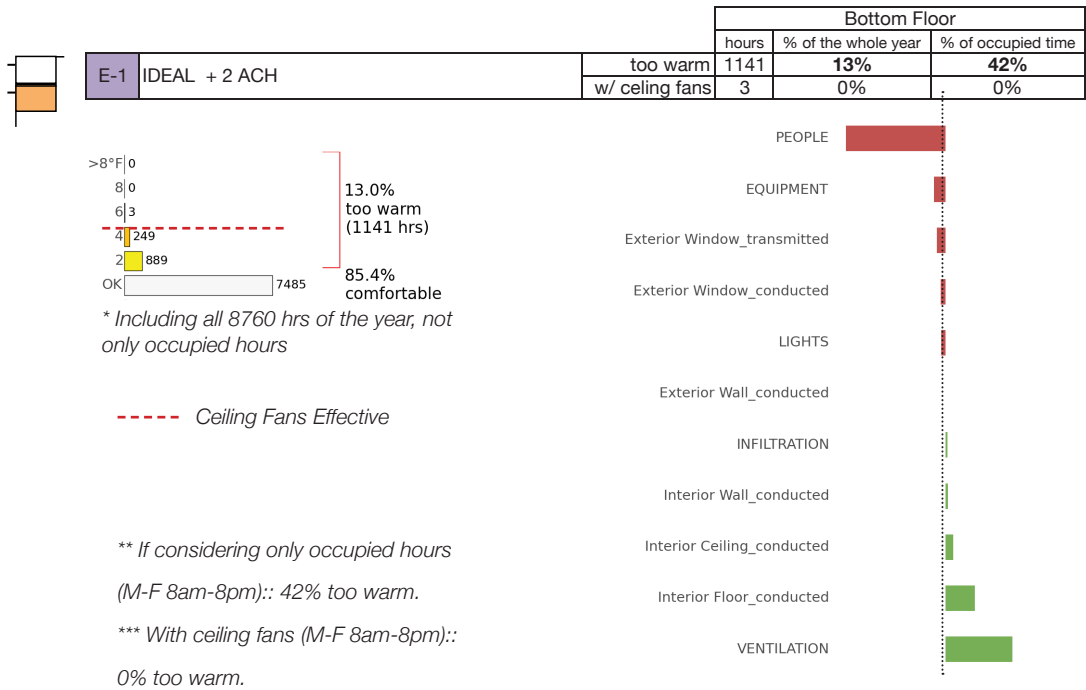
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.b.7 Classroom Analysis:: North Facing (Continued)



Add/C.3.c CLASSROOM ANALYSIS:: EAST FACING

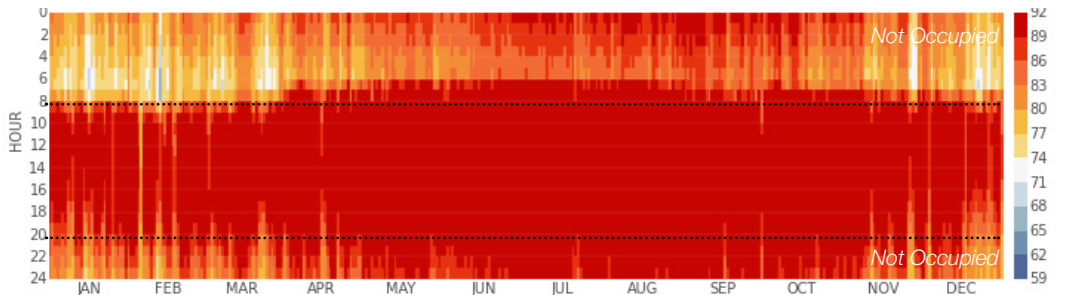


C.3.c.0. TYPICAL EXISTING

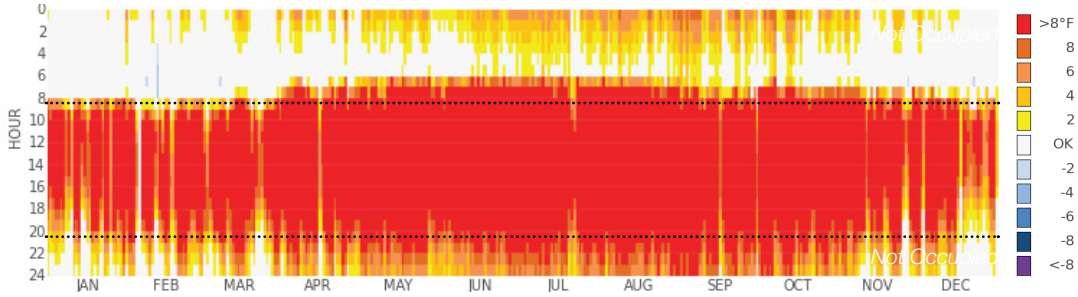
No Insulation in Opaque Surfaces and Single Pane Glass



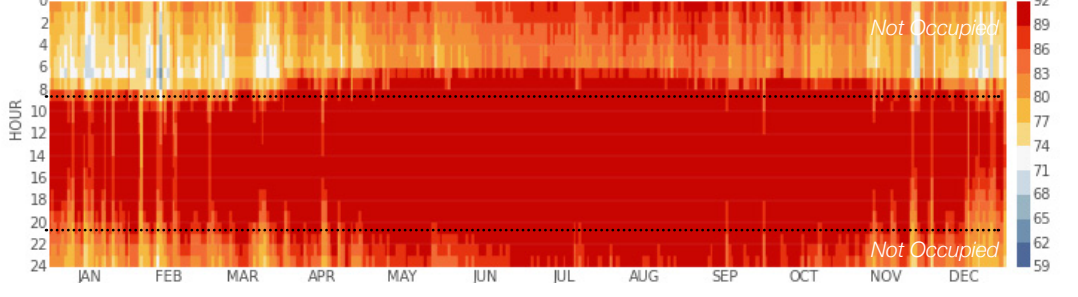
Operative temperature for bottom floor



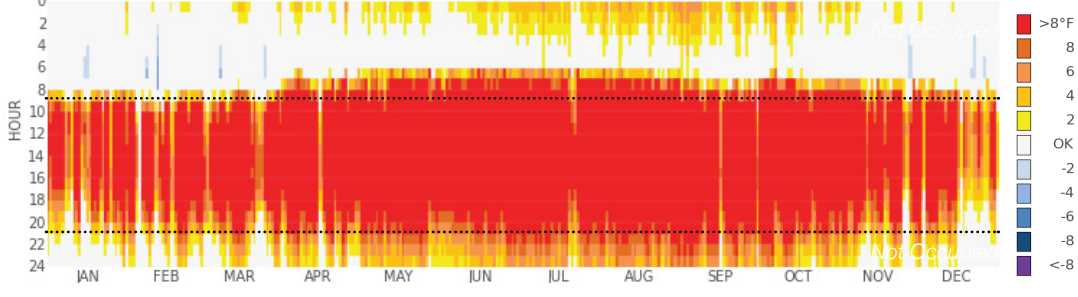
Degrees from comfort for bottom floor



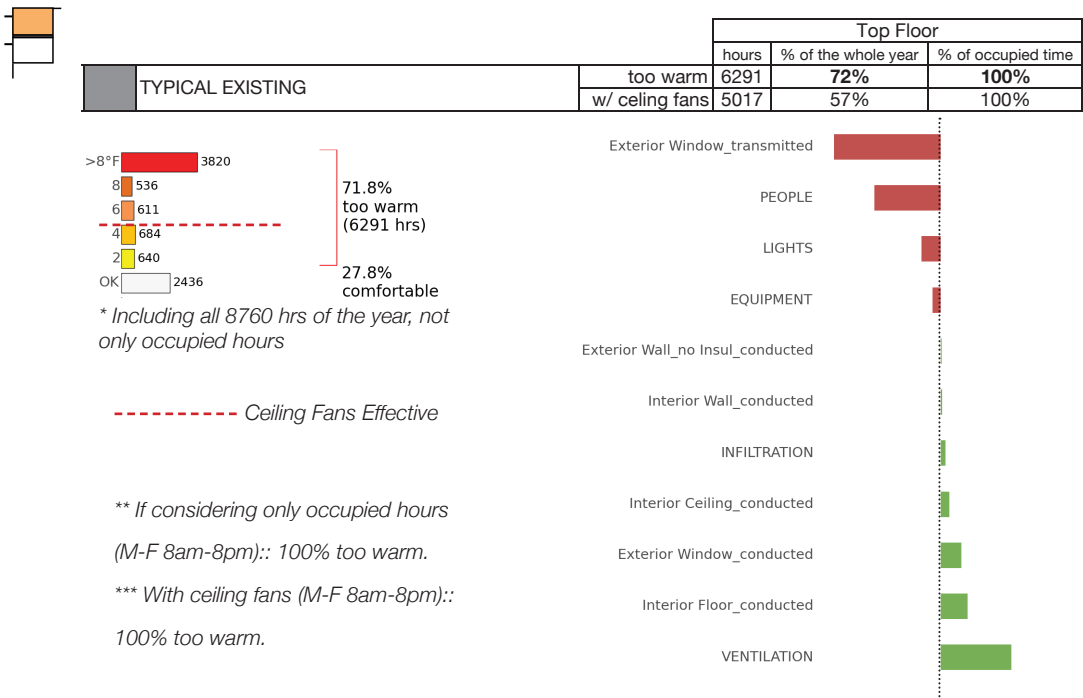
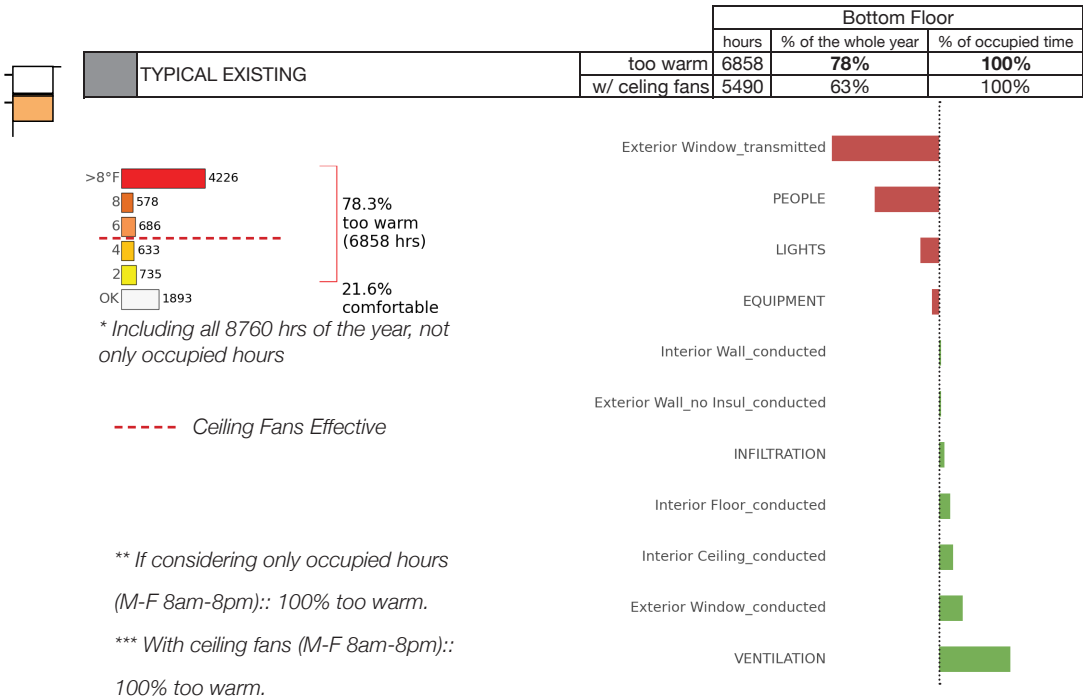
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.c.0 Classroom Analysis:: East Facing (Continued)



Add/C.3.c CLASSROOM ANALYSIS:: EAST FACING

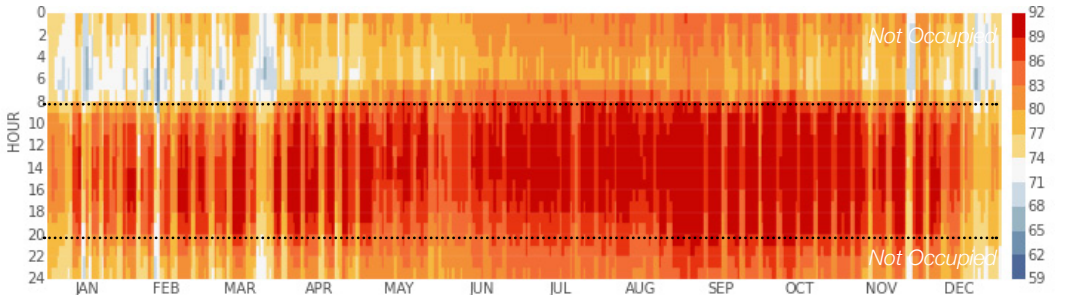


C.3.c.1. TYPICAL WITH WINDOW IMPROVEMENTS

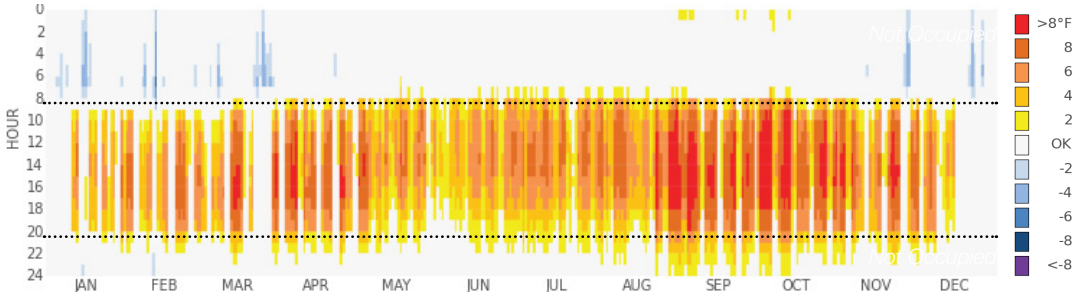
Equal to TYPICAL + 1ACH + Shading + IECC 2015 Windows



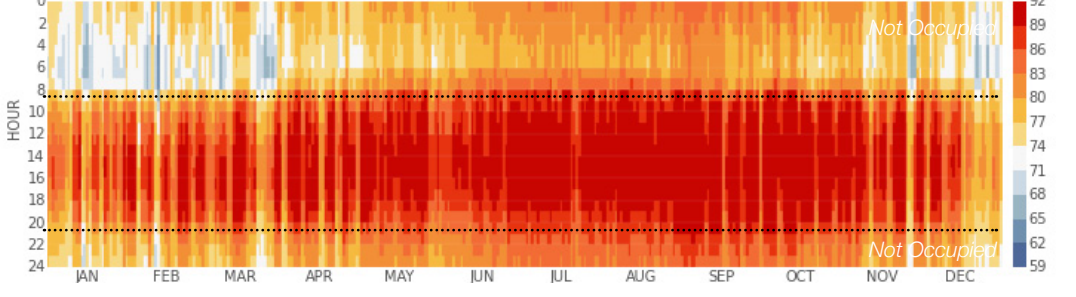
Operative temperature for bottom floor



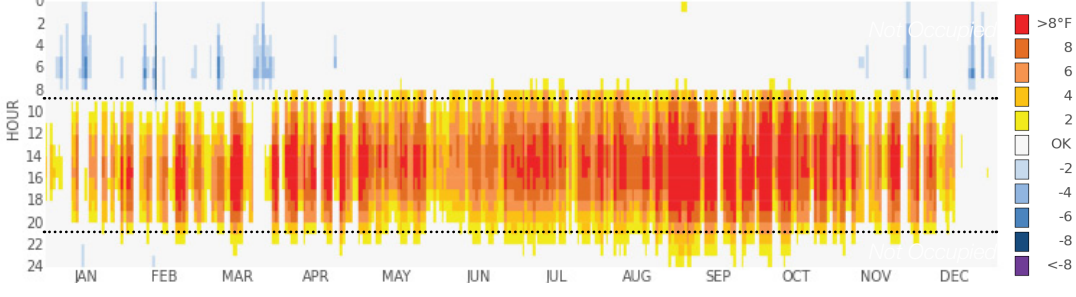
Degrees from comfort for bottom floor



Operative temperature for top floor



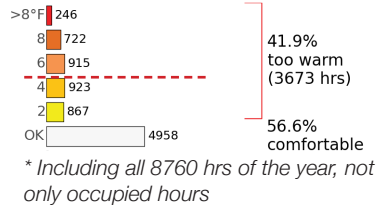
Degrees from comfort for top floor



Add/C.3.c.1 Classroom Analysis:: East Facing (Continued)

		Bottom Floor			
		hours	% of the whole year	% of occupied time	
A-3	TYPICAL +1ACH + SHADING + IECC WINDOWS	too warm	3673	42%	100%
		w/ celing fans	1883	21%	70%

A-3 TYPICAL +1ACH +



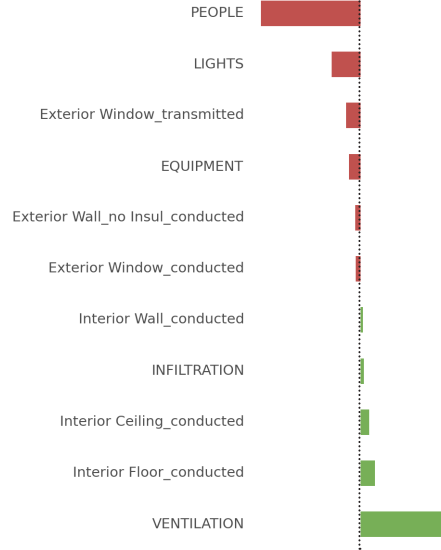
----- Ceiling Fans Effective

** If considering only occupied hours

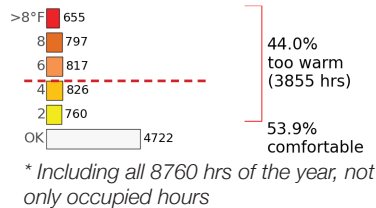
(M-F 8am-8pm):: 100% too warm.

*** With ceiling fans (M-F 8am-8pm)::

70% too warm.



		Top Floor			
		hours	% of the whole year	% of occupied time	
A-3	TYPICAL +1ACH + SHADING + IECC WINDOWS	too warm	3855	44%	100%
		w/ celing fans	2270	26%	84%



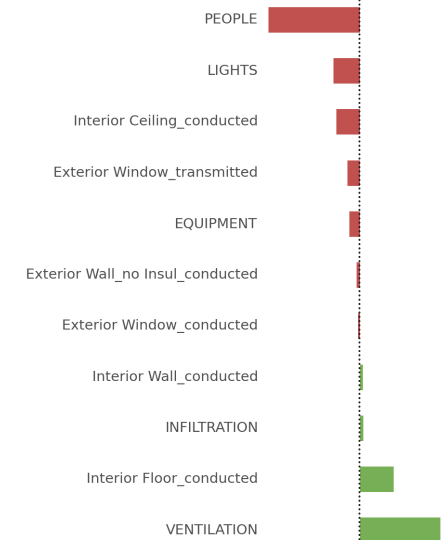
----- Ceiling Fans Effective

** If considering only occupied hours

(M-F 8am-8pm):: 100% too warm.

*** With ceiling fans (M-F 8am-8pm)::

84% too warm.



Add/C.3.c CLASSROOM ANALYSIS:: EAST FACING

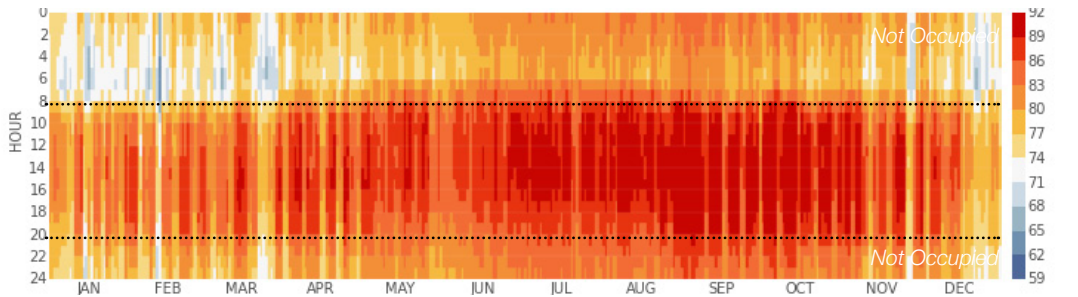


C.3.c.2. MINIMUM SUITE

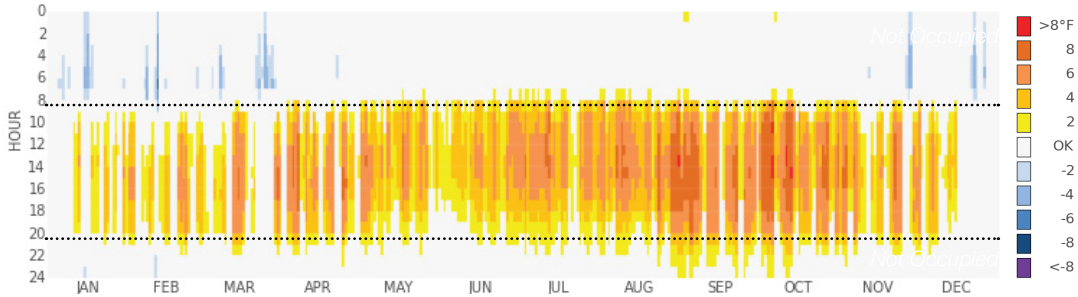
Equalt to TYPICAL + IECC Windows + Shading +lower LPD + Daylight Controls +1ACH



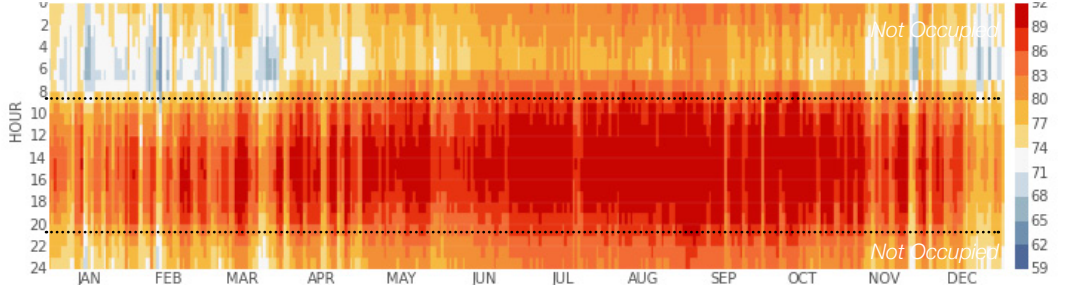
Operative temperature for bottom floor



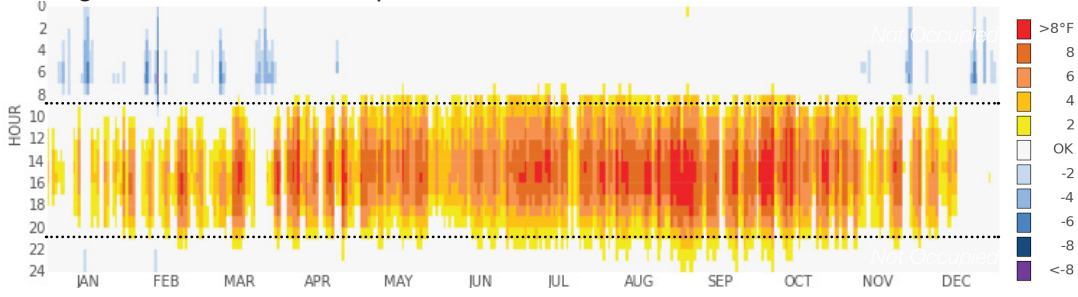
Degrees from comfort for bottom floor



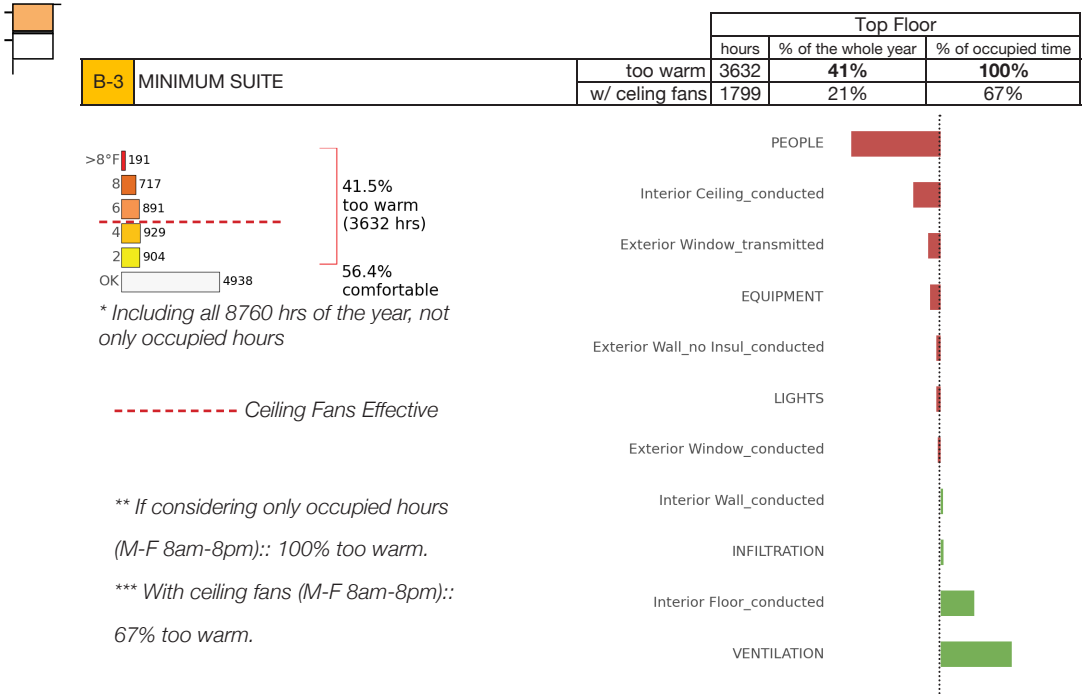
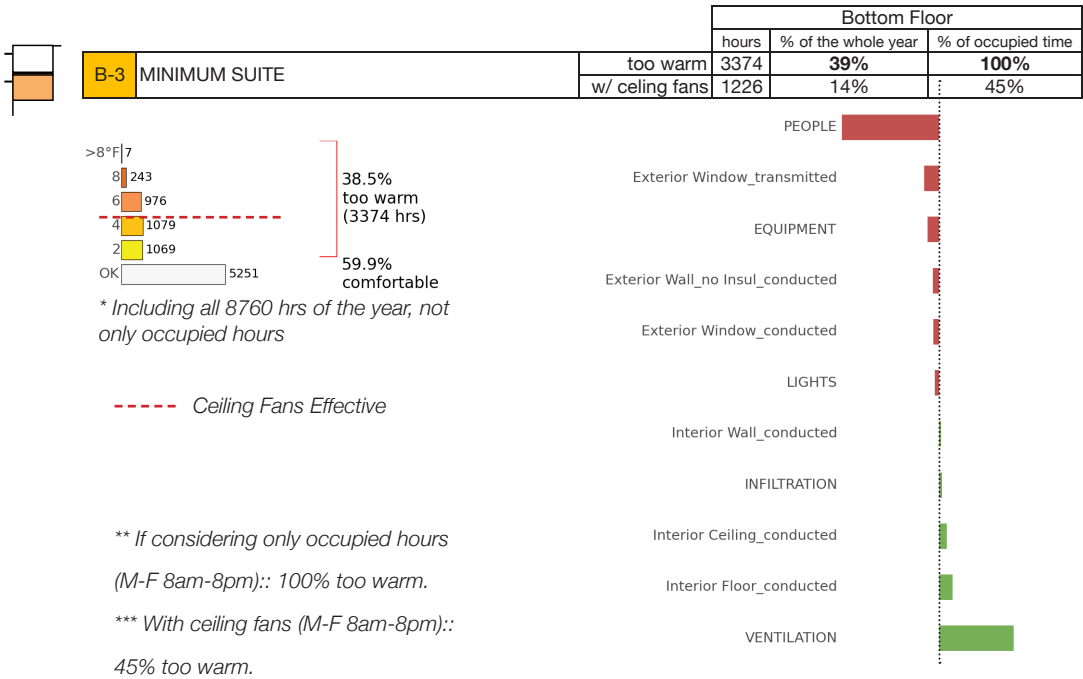
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.c.2 Classroom Analysis:: East Facing (Continued)



Add/C.3.c CLASSROOM ANALYSIS:: EAST FACING

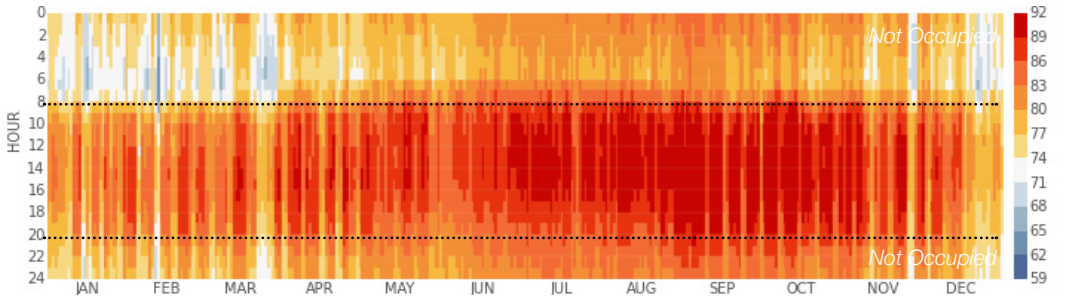


C.3.c.3. IMPROVED SUITE

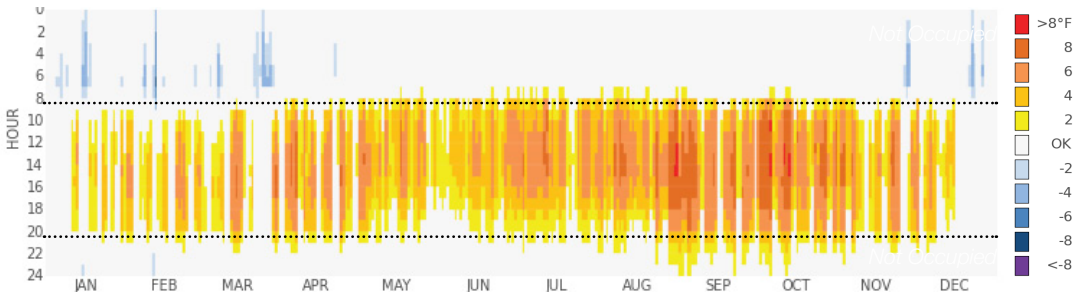
Equal to MINIMUM SUITE + IECC Roof



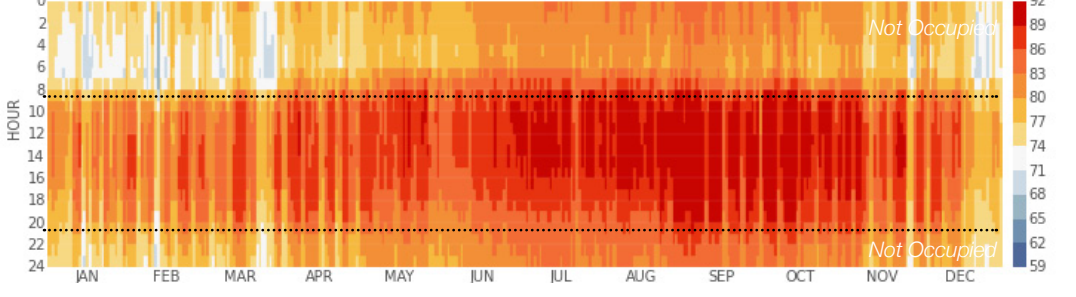
Operative temperature for bottom floor



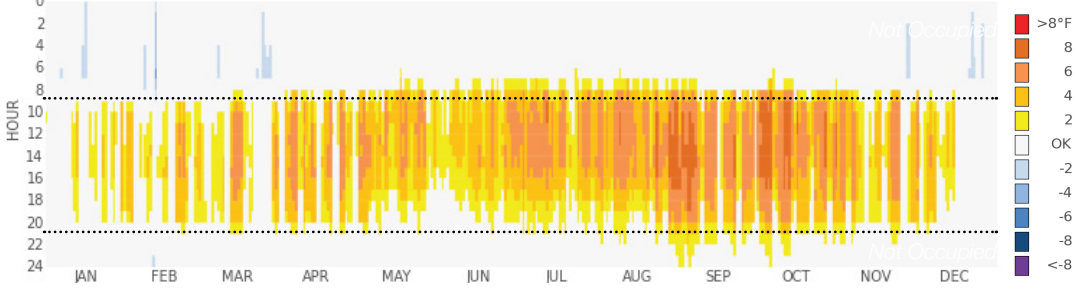
Degrees from comfort for bottom floor



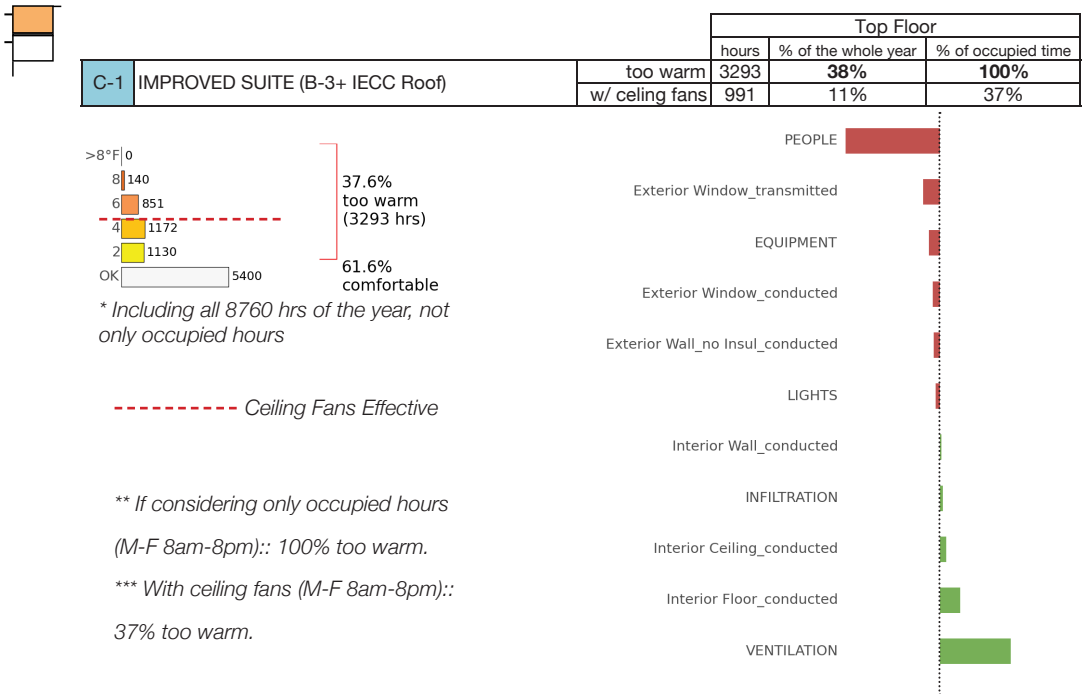
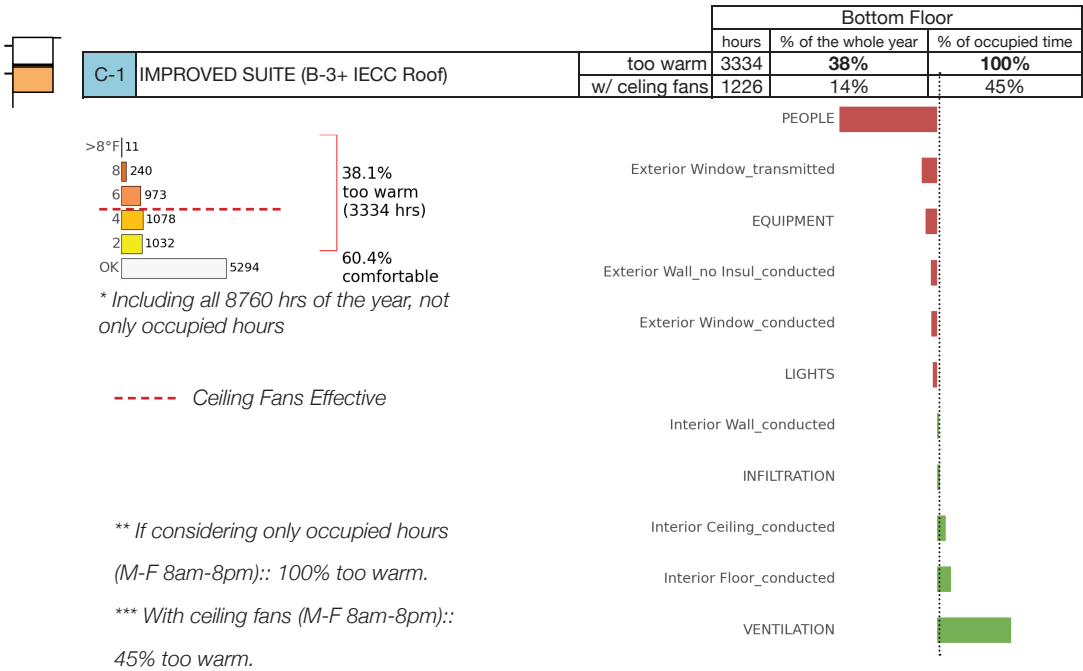
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.c.3 Classroom Analysis:: East Facing (Continued)



Add/C.3.c CLASSROOM ANALYSIS:: EAST FACING

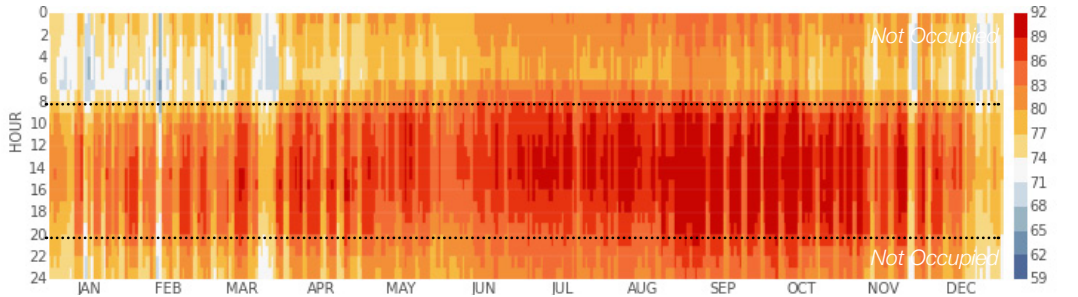


C.3.c.4. CODE SUITE

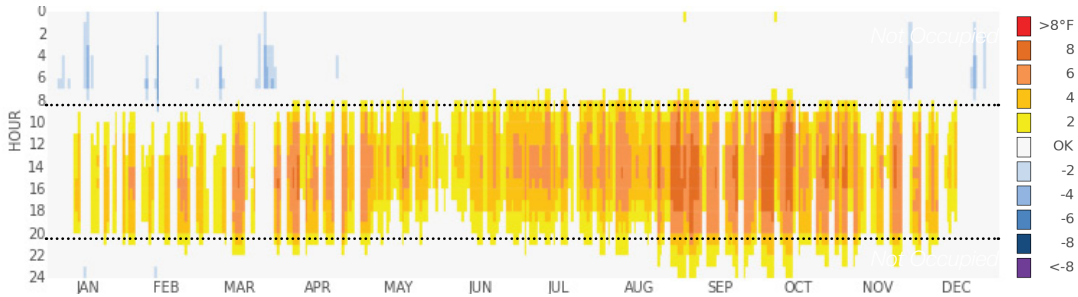
Equal to IMPROVED SUITE + IECC Walls



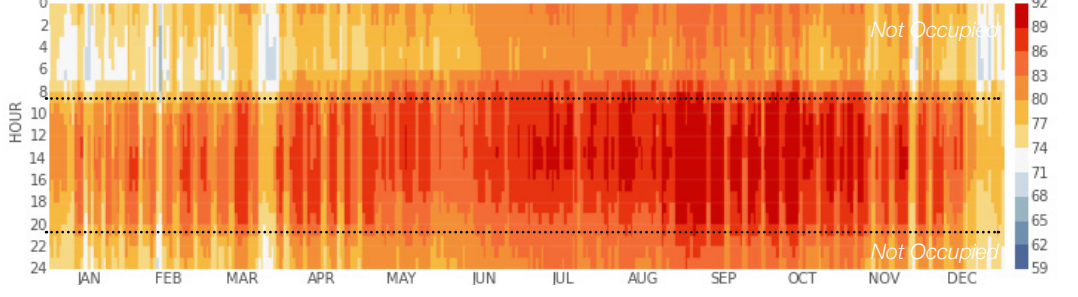
Operative temperature for bottom floor



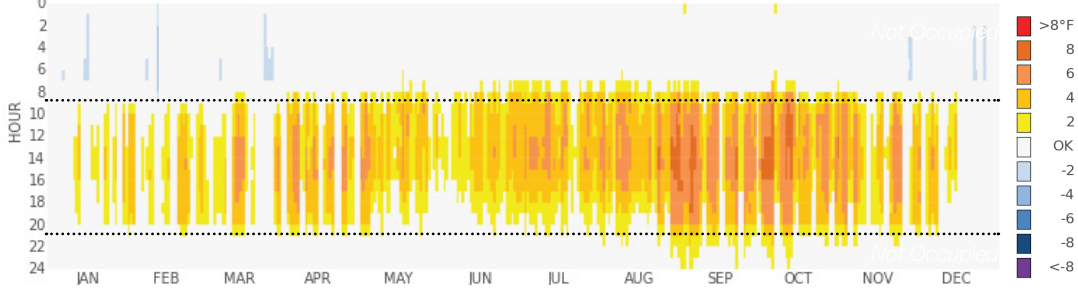
Degrees from comfort for bottom floor



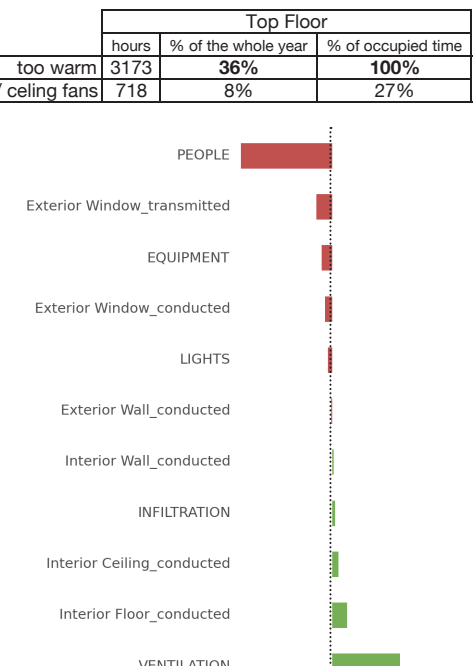
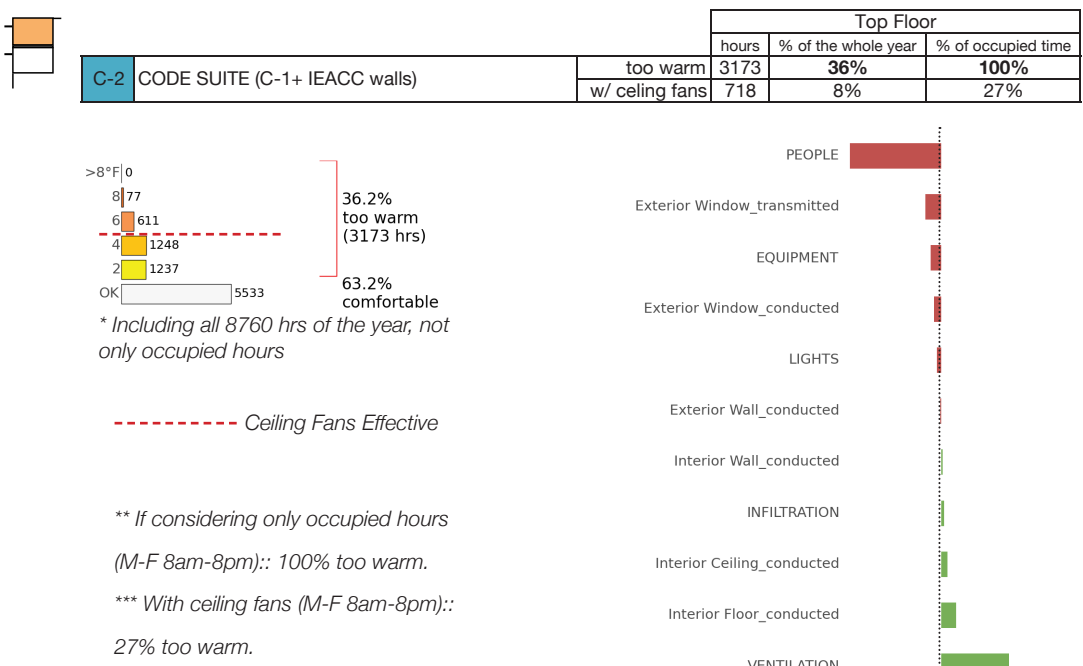
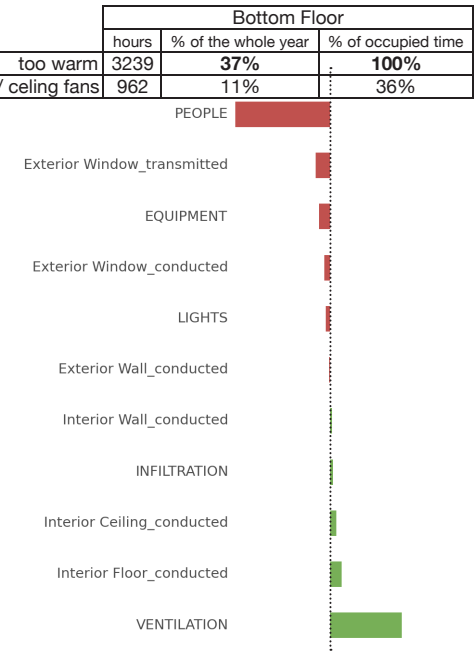
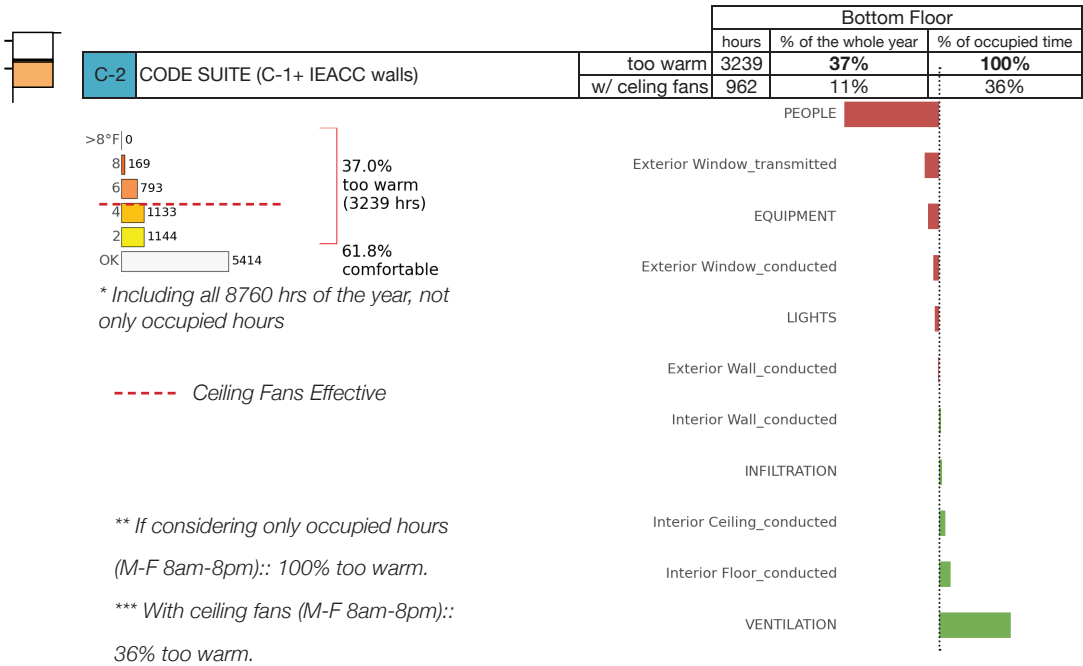
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.c.4 Classroom Analysis:: East Facing (Continued)



Add/C.3.c CLASSROOM ANALYSIS:: EAST FACING

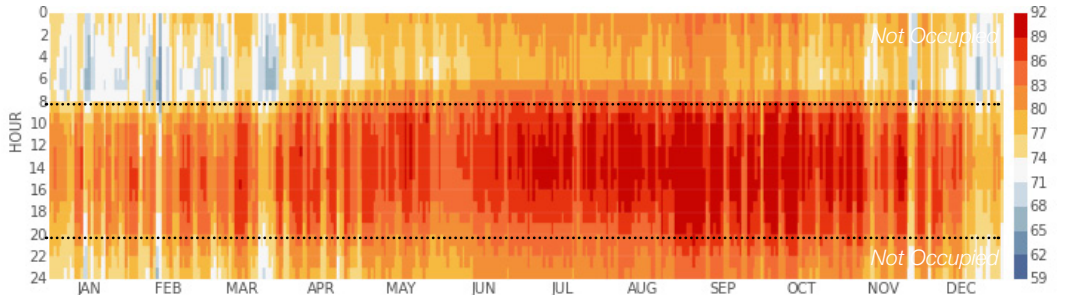


C.3.c.5. IMPROVED SUITE WITH VENTILATION

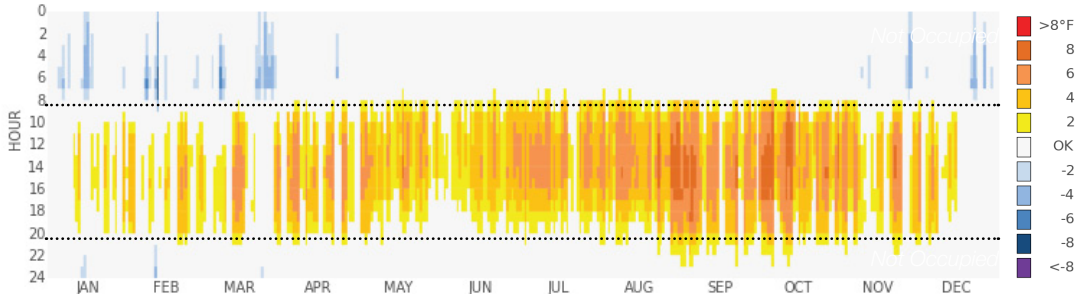
Equal to IMPROVED SUITE +2ACH



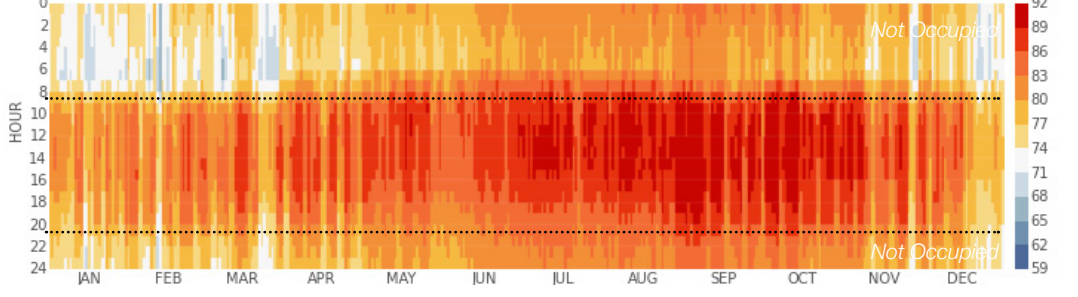
Operative temperature for bottom floor



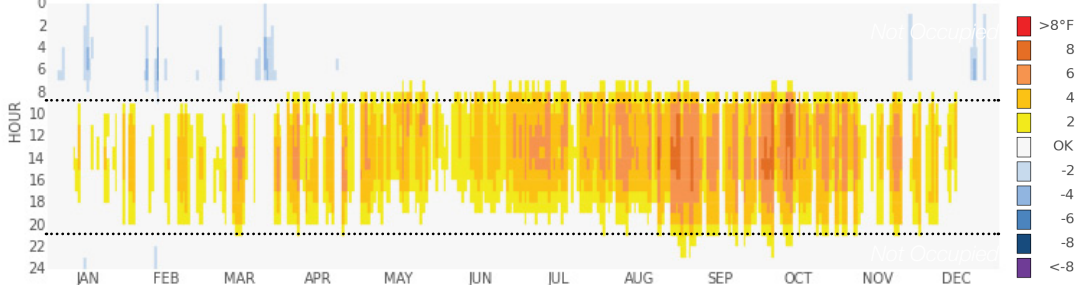
Degrees from comfort for bottom floor



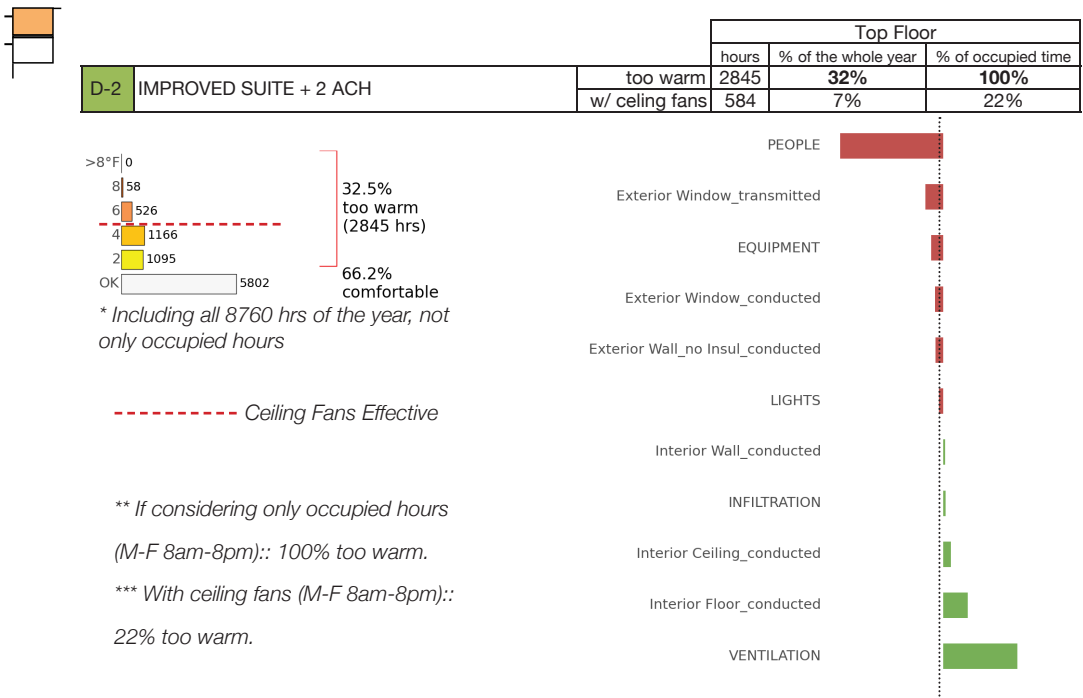
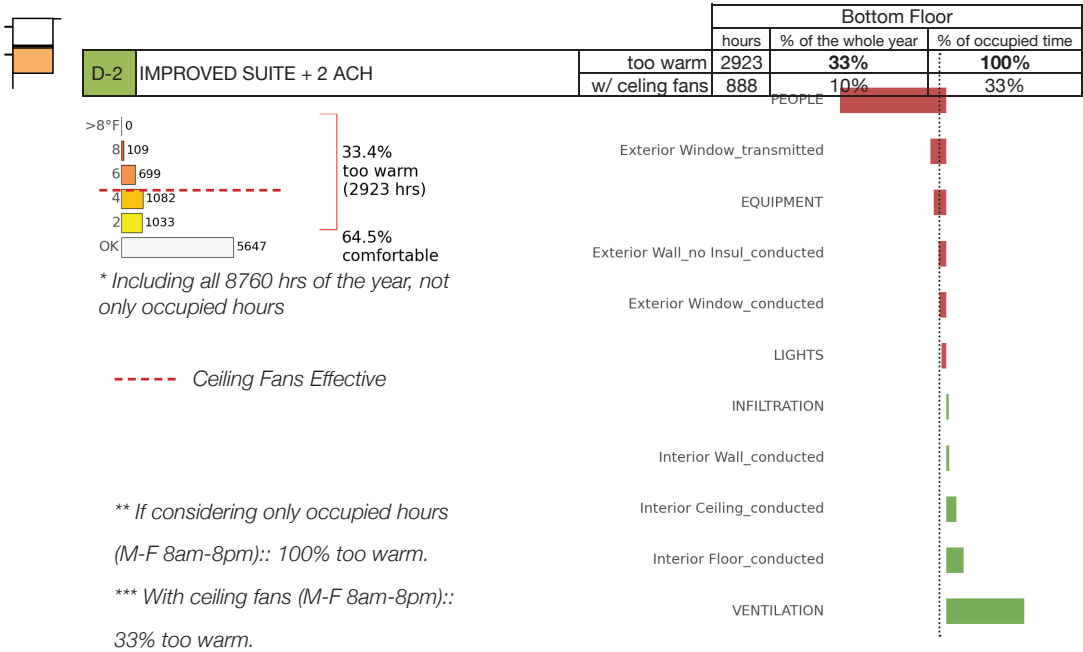
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.c.5 Classroom Analysis:: East Facing (Continued)



Add/C.3.c CLASSROOM ANALYSIS:: EAST FACING

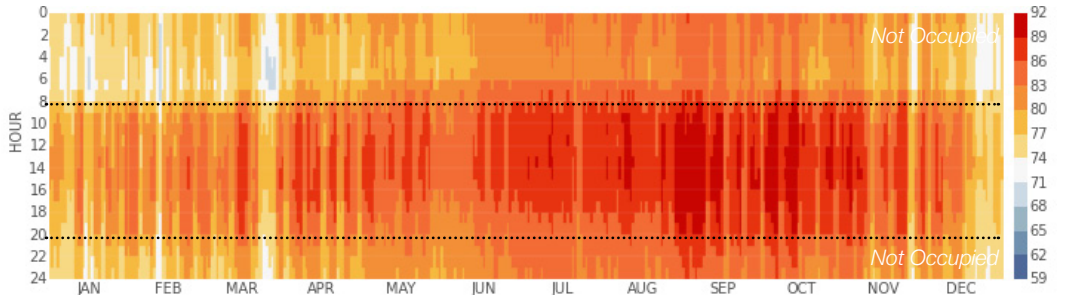


C.3.c.6. IDEAL SUITE

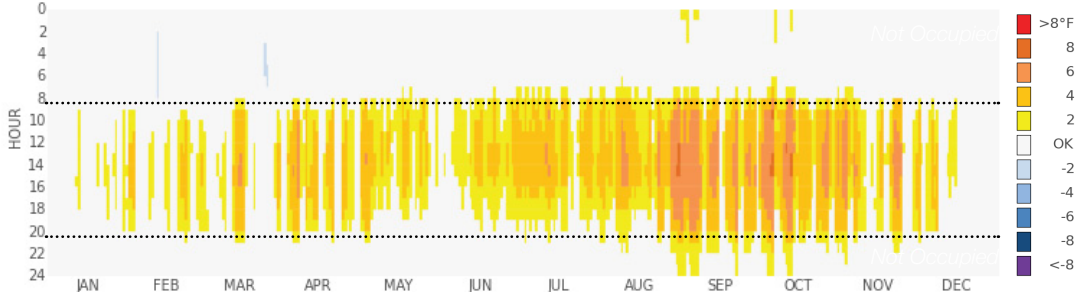
Equal to CODE SUITE + Thermal Mass



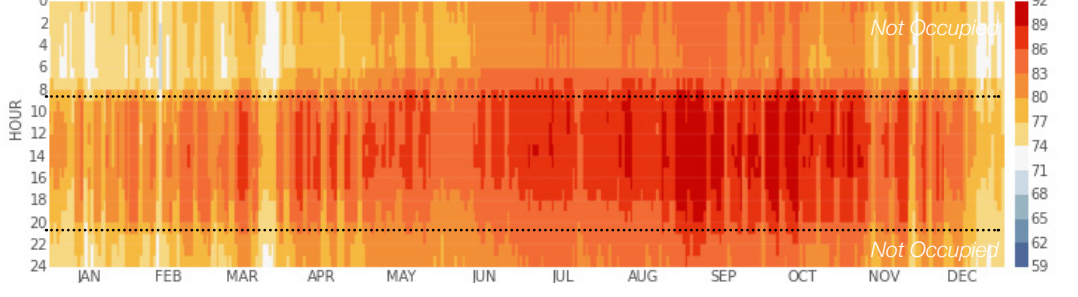
Operative temperature for bottom floor



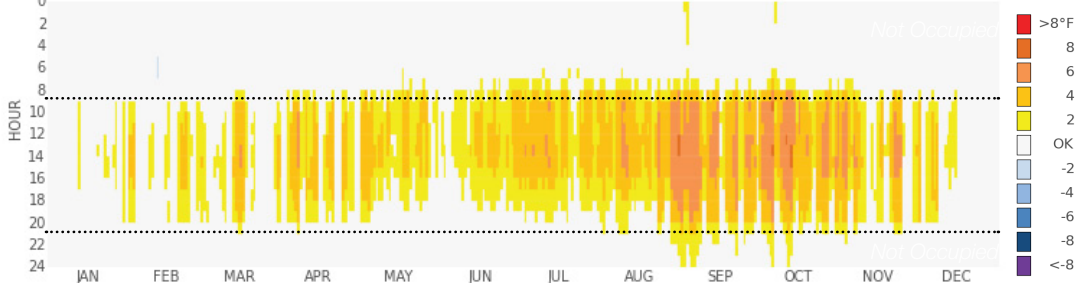
Degrees from comfort for bottom floor



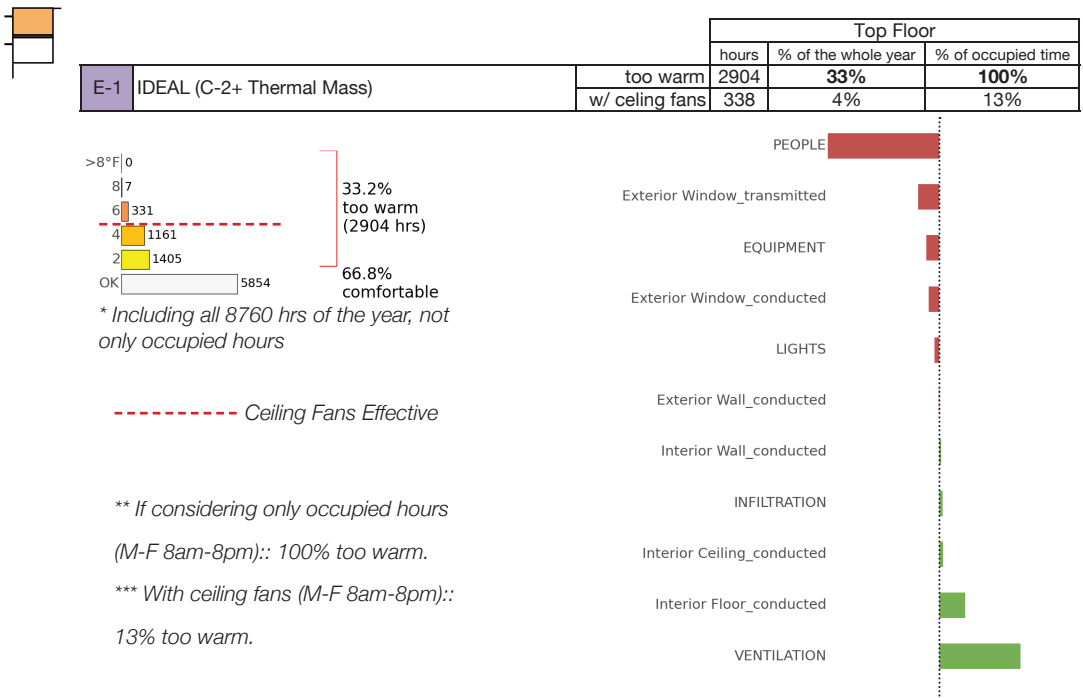
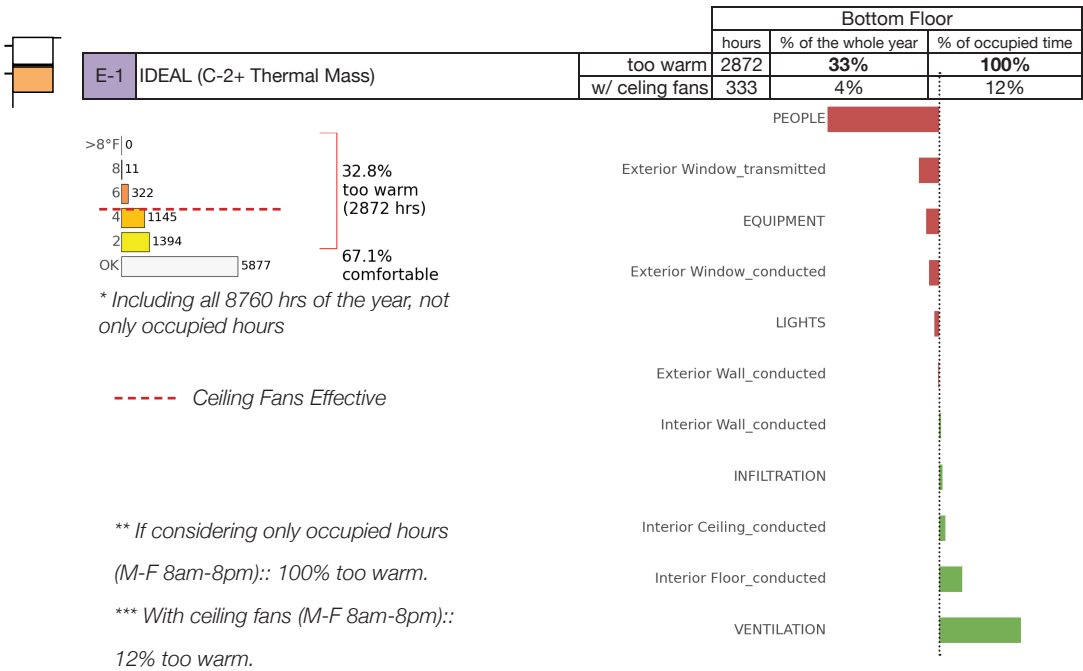
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.c.6 Classroom Analysis:: East Facing (Continued)



Add/C.3.c CLASSROOM ANALYSIS:: EAST FACING

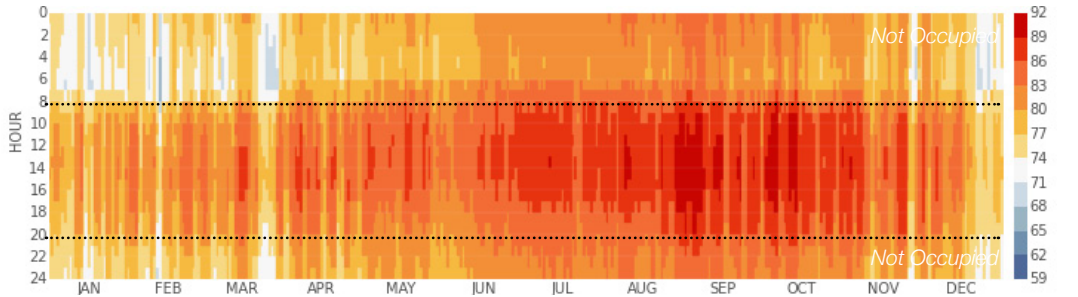


C.3.c.7. IDEAL SUITE WITH VENTILATION

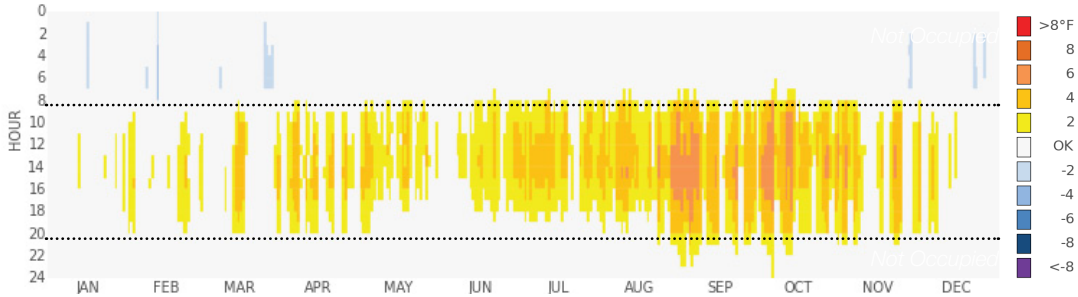
Equal to IDEAL SUITE + 2ACH



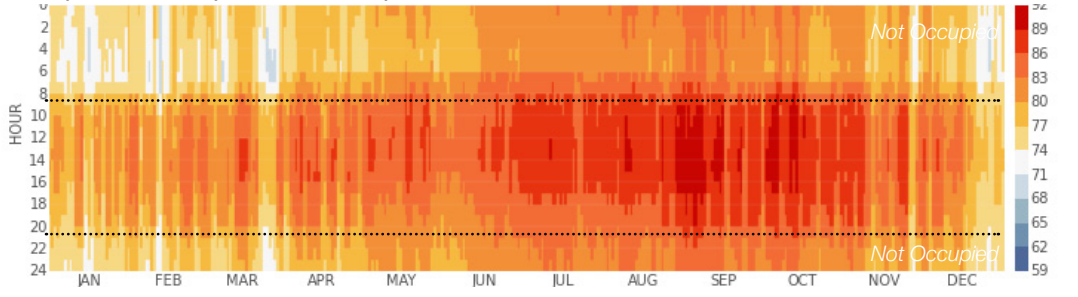
Operative temperature for bottom floor



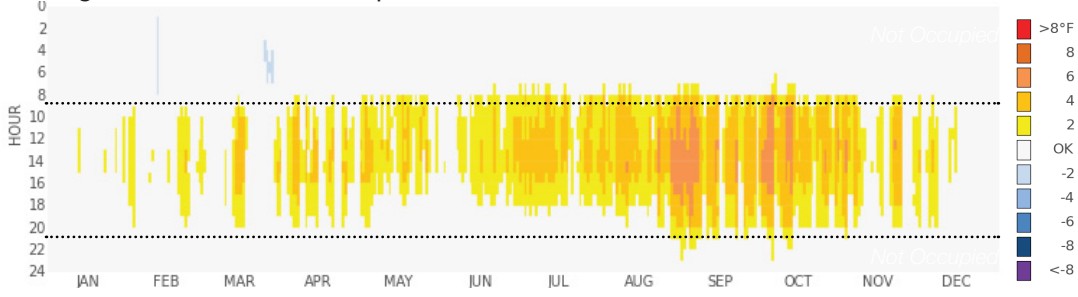
Degrees from comfort for bottom floor



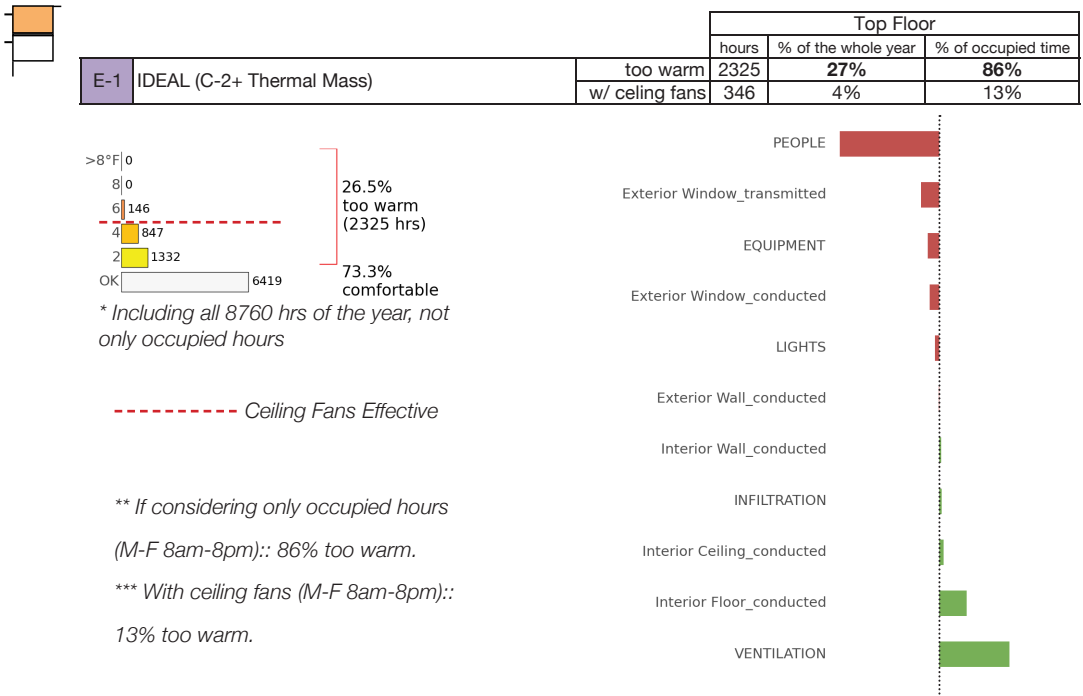
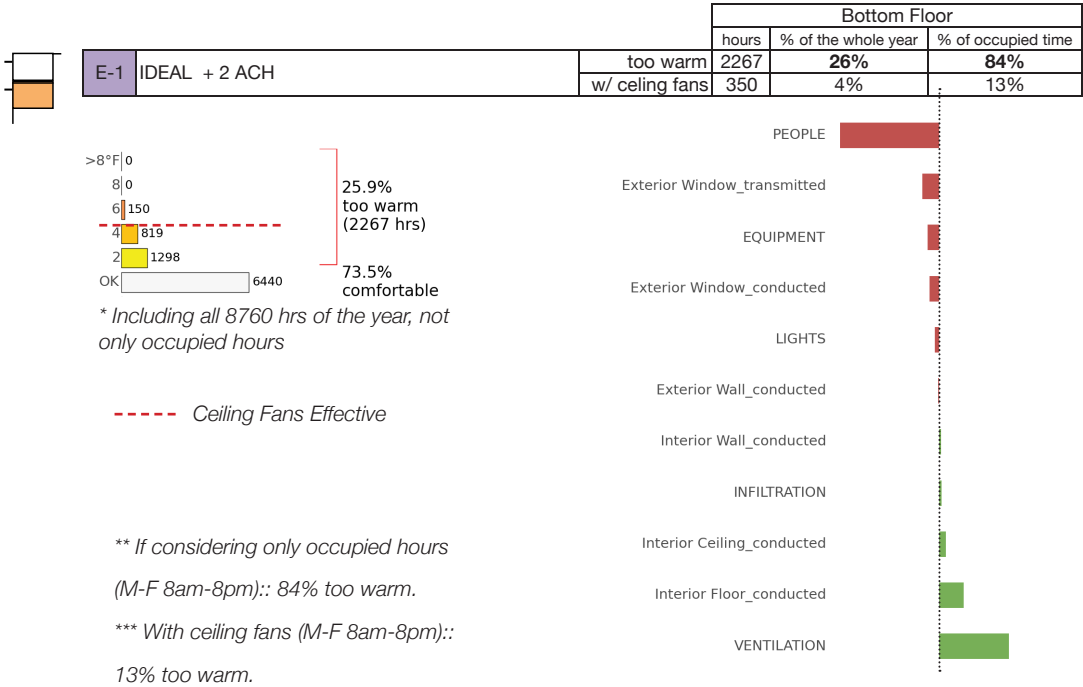
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.c.7 Classroom Analysis:: East Facing (Continued)



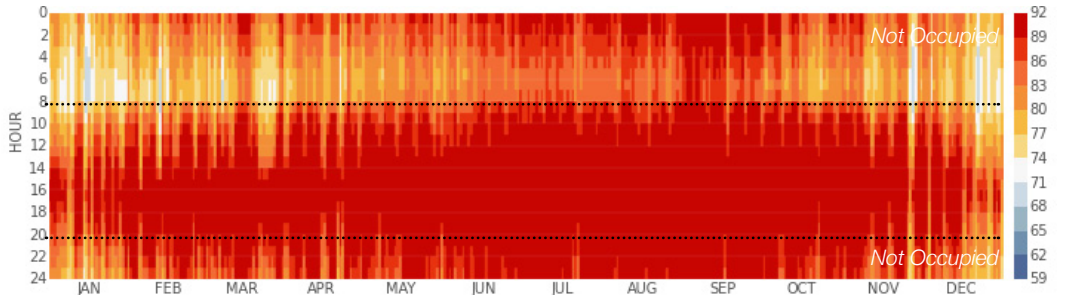
Add/C.3.d CLASSROOM ANALYSIS:: WEST FACING

C.3.d.0. TYPICAL EXISTING

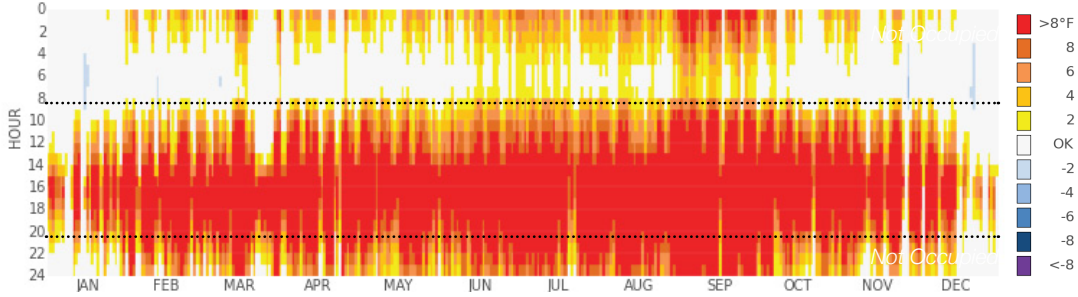
No Insulation in Opaque Surfaces and Single Pane Glass



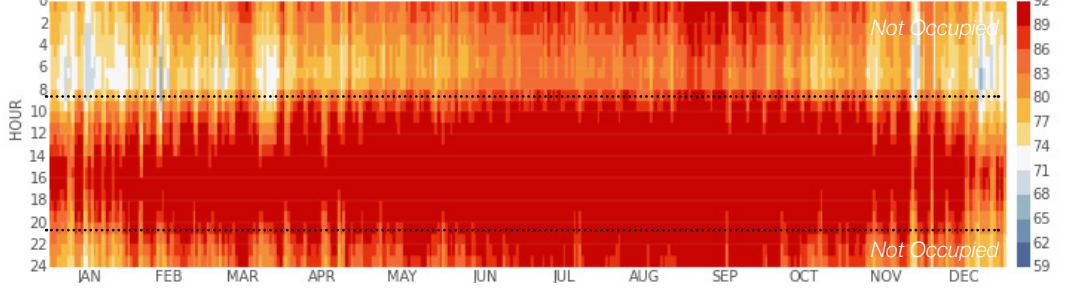
Operative temperature for bottom floor



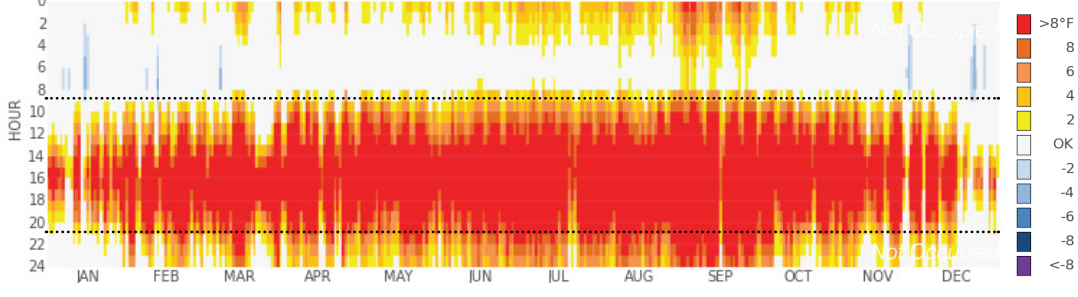
Degrees from comfort for bottom floor



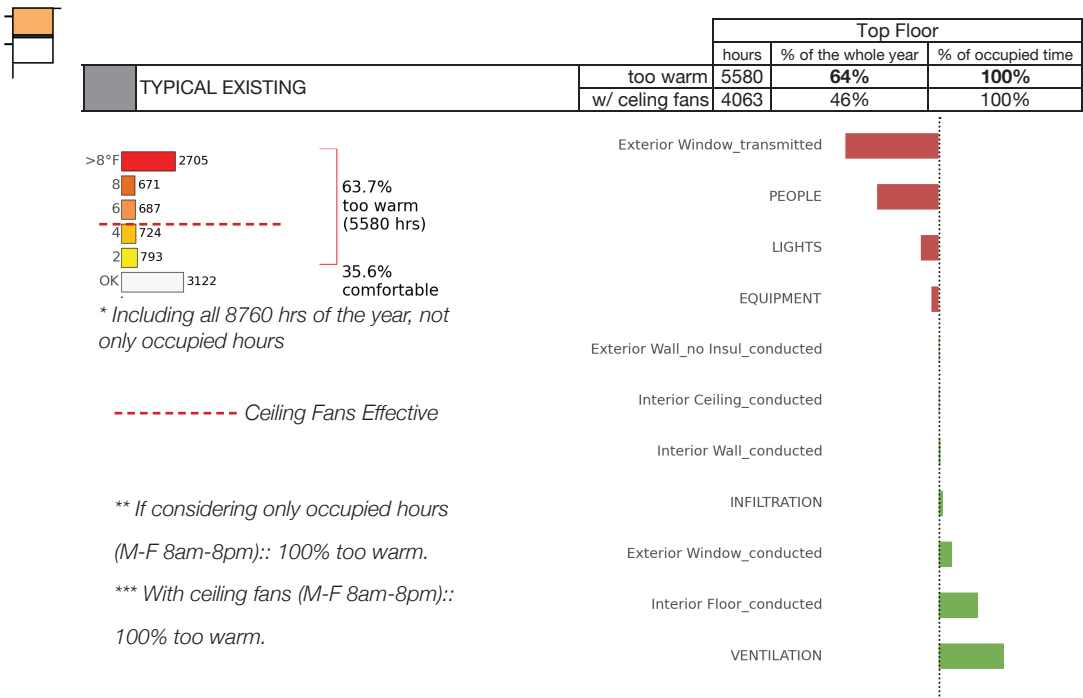
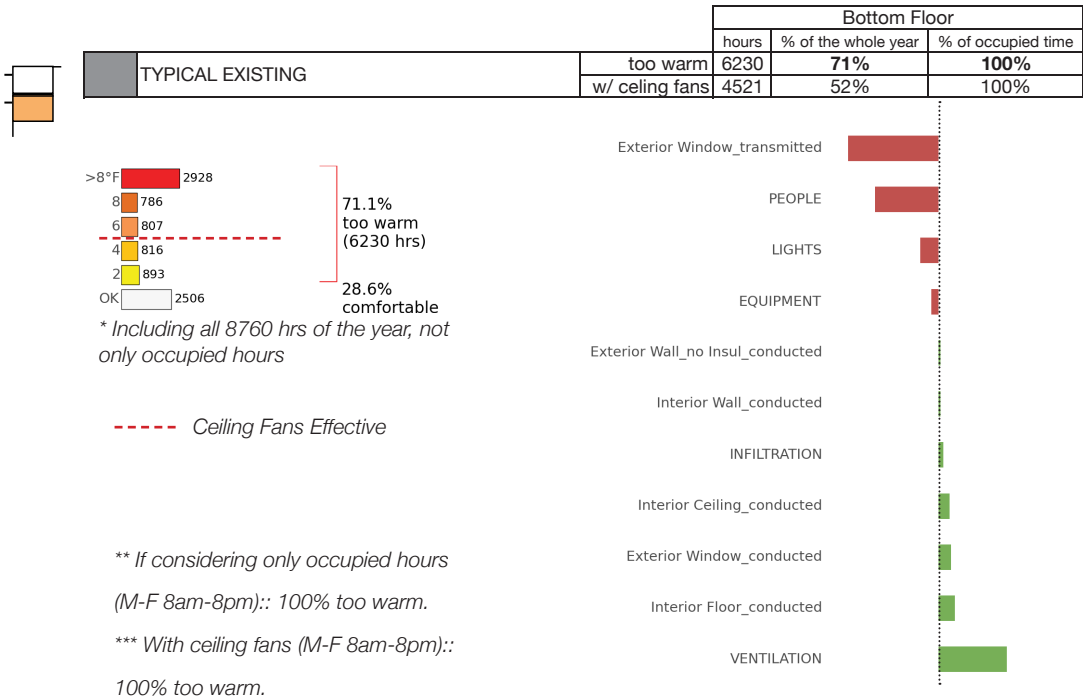
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.d.0 Classroom Analysis:: West Facing (Continued)



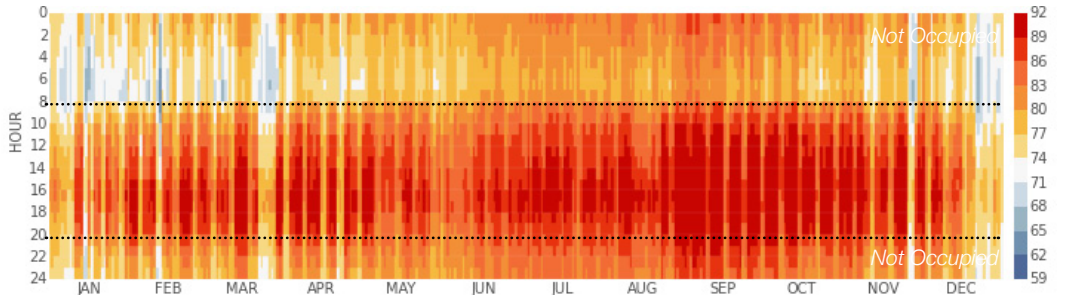
Add/C.3.d CLASSROOM ANALYSIS:: WEST FACING

C.3.d.1. TYPICAL WITH WINDOW IMPROVEMENTS

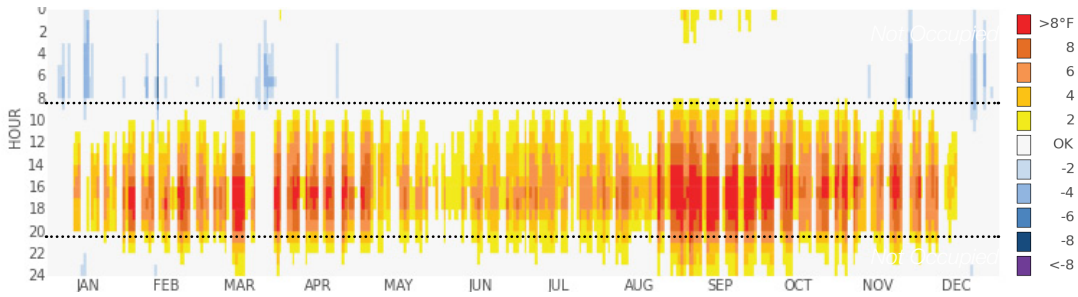
TYPICAL + 1ACH + Shading + IECC 2015 Windows



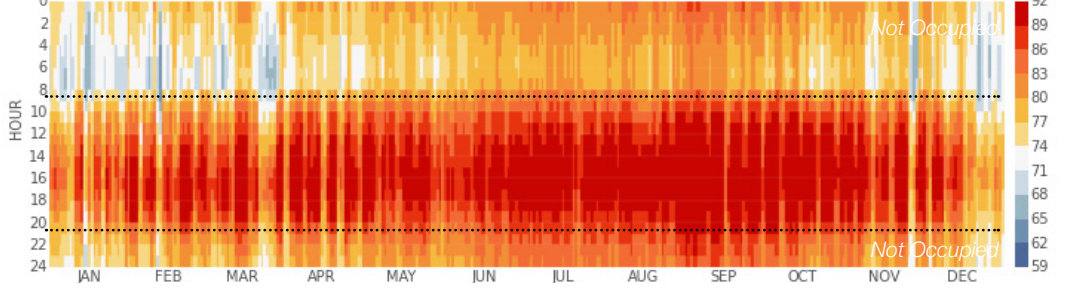
Operative temperature for bottom floor



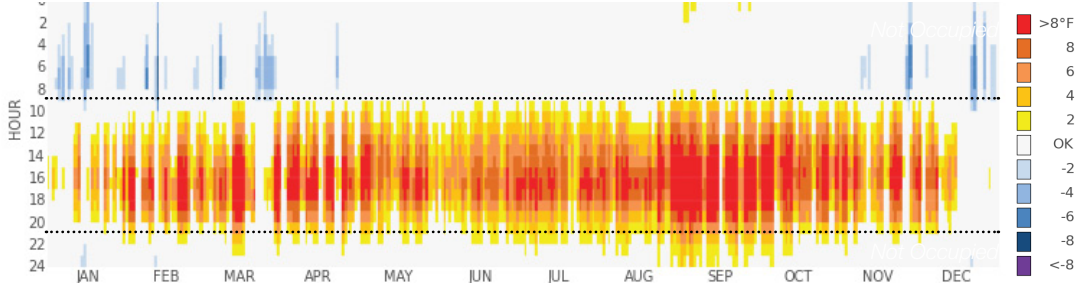
Degrees from comfort for bottom floor



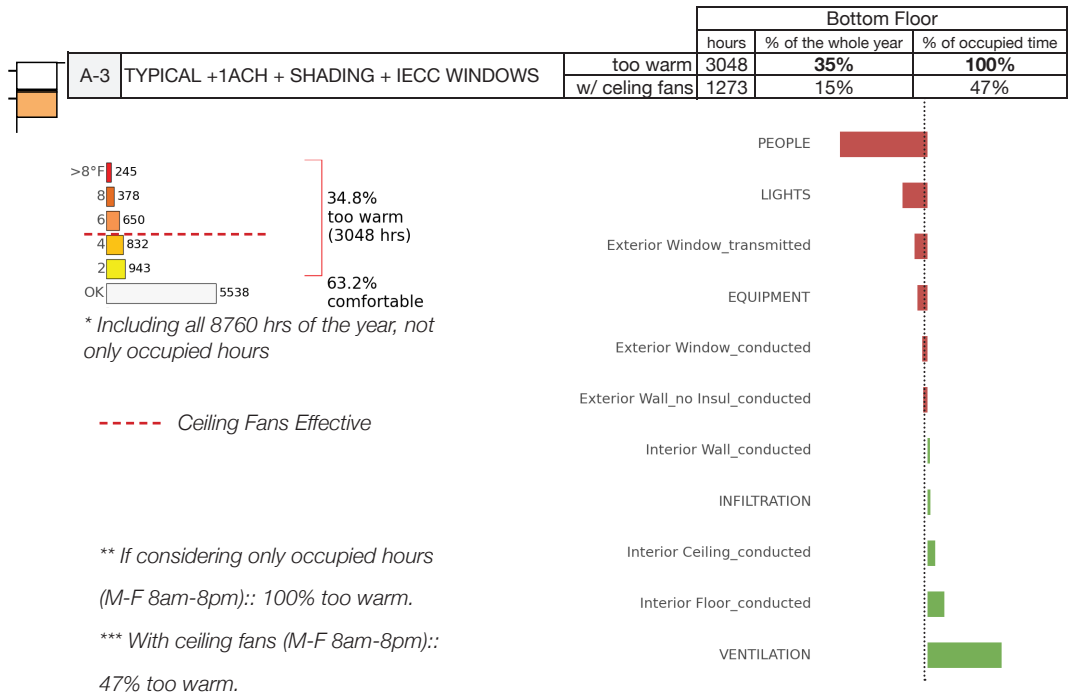
Operative temperature for top floor



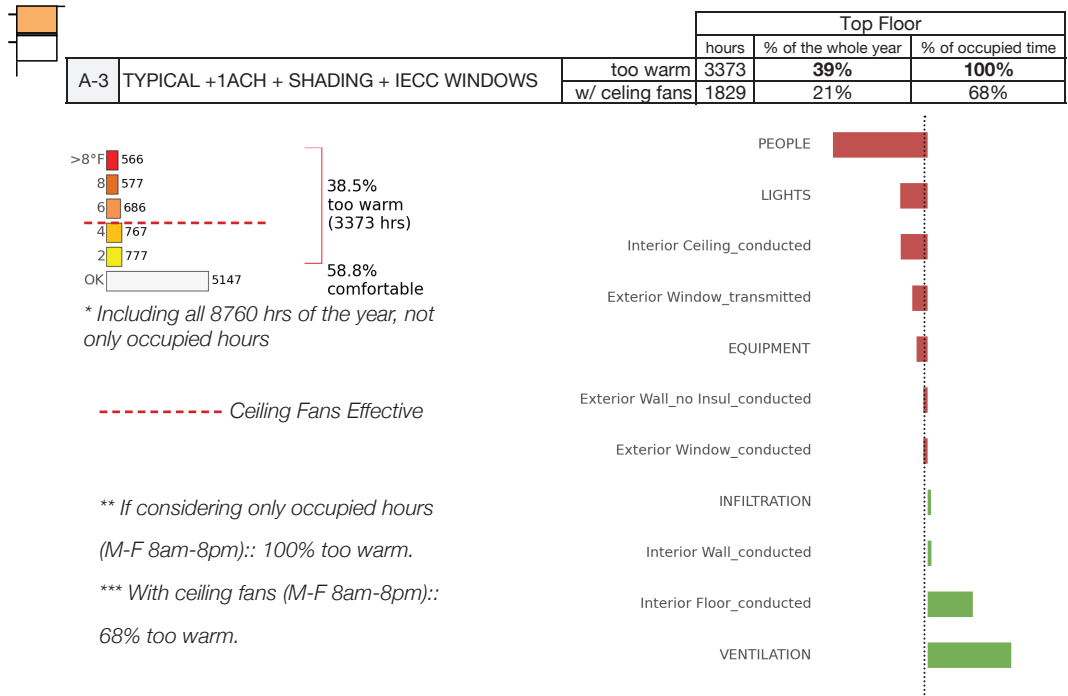
Degrees from comfort for top floor



Add/C.3.d.1 Classroom Analysis:: West Facing (Continued)



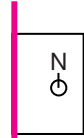
A-3 TYPICAL +1ACH +



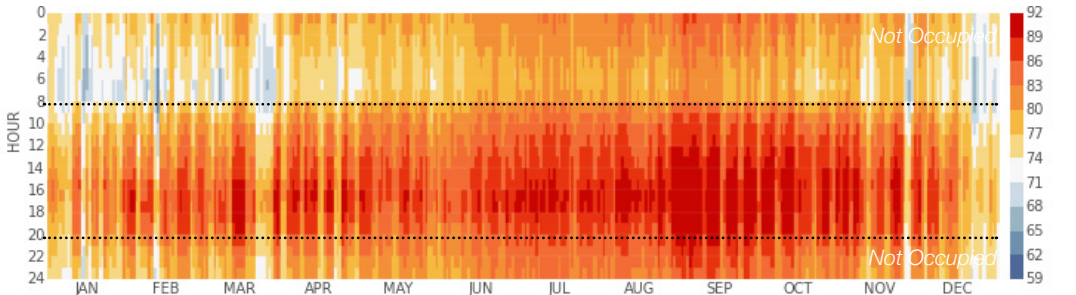
Add/C.3.d CLASSROOM ANALYSIS:: WEST FACING

C.3.d.2. MINIMUM SUITE

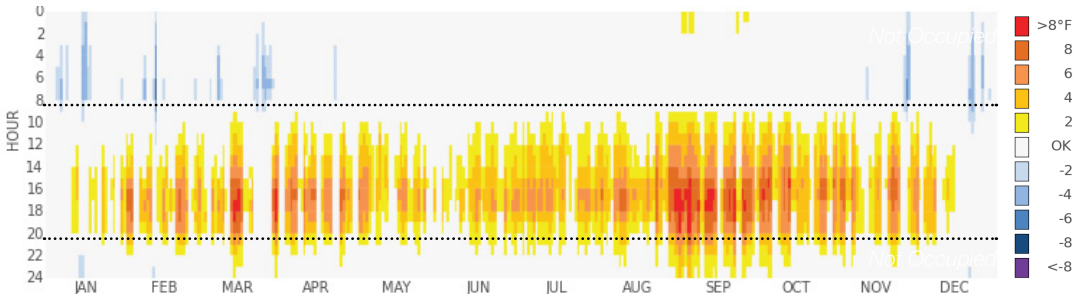
Equal to TYPICAL + IECC Windows + Shading +lower LPD + Daylight Controls +1ACH



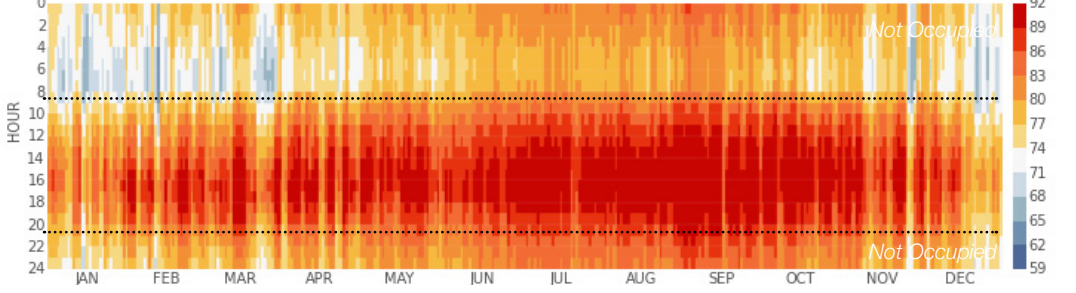
Operative temperature for bottom floor



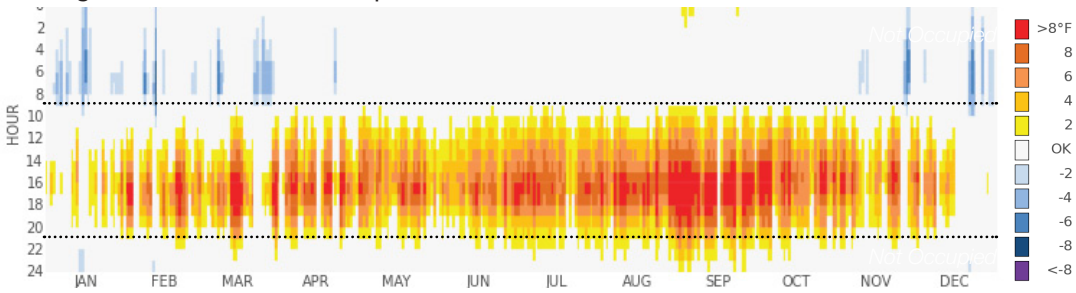
Degrees from comfort for bottom floor



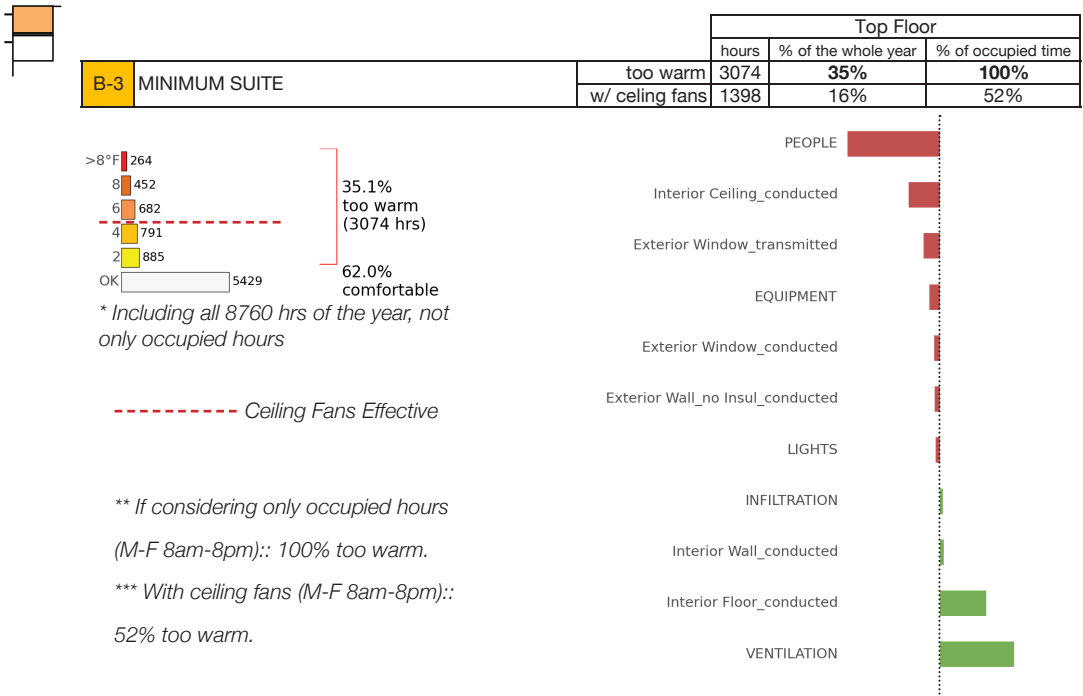
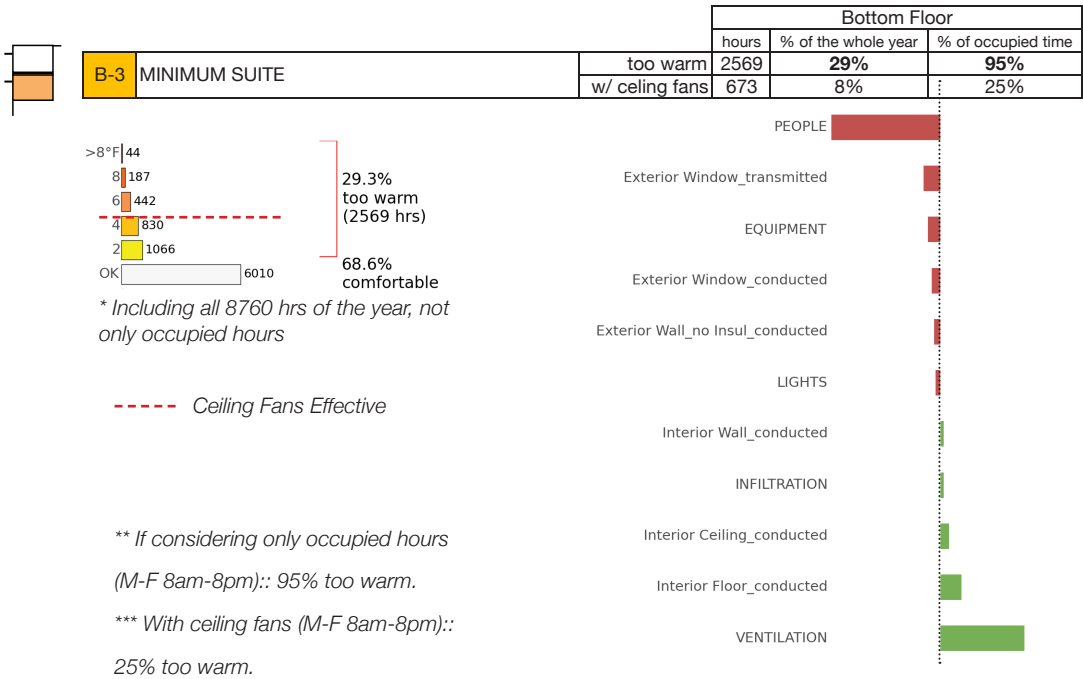
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.d.2 Classroom Analysis:: West Facing (Continued)



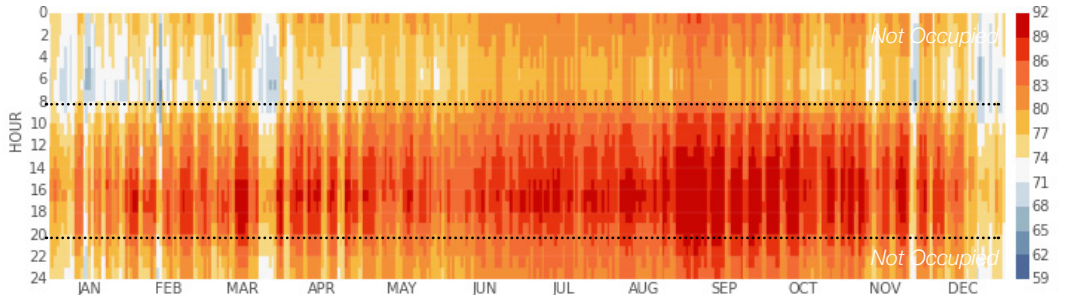
Add/C.3.d CLASSROOM ANALYSIS:: WEST FACING

C.3.d.3. IMPROVED SUITE

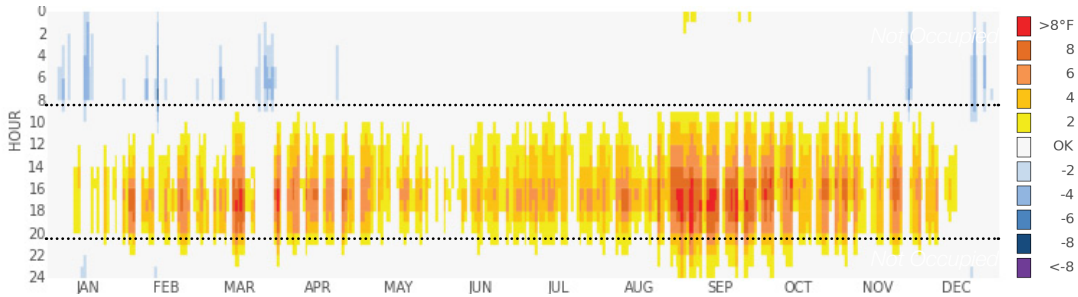
Equal to MINIMUM SUITE + IECC Roof



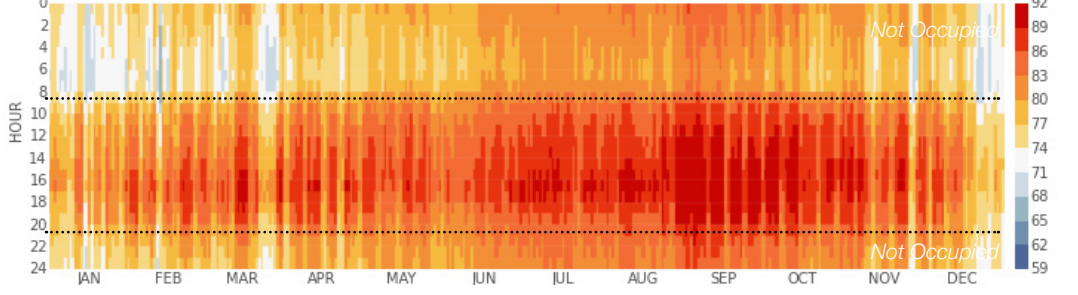
Operative temperature for bottom floor



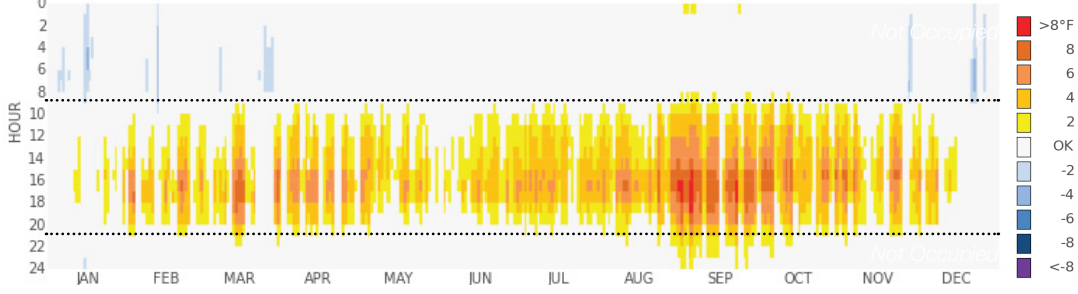
Degrees from comfort for bottom floor



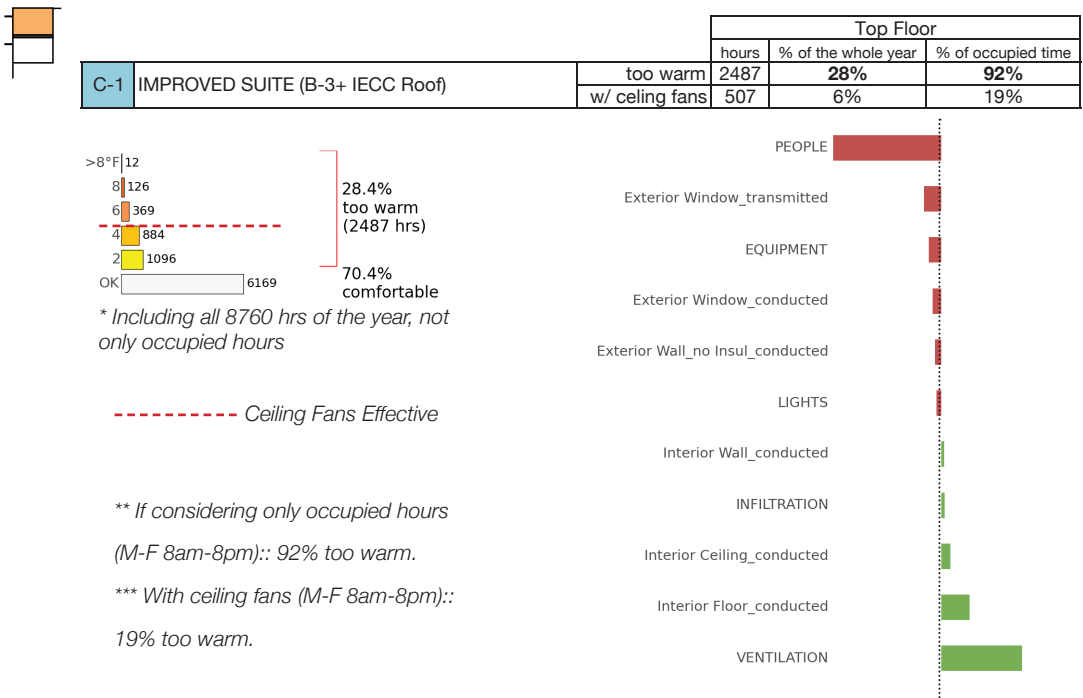
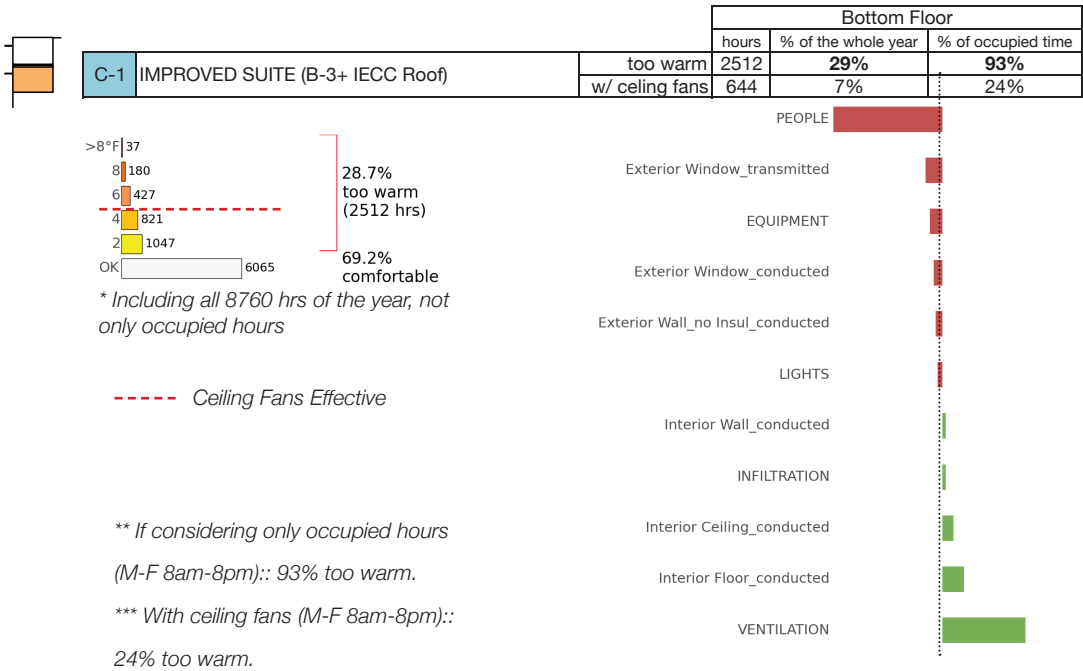
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.d.3 Classroom Analysis:: West Facing (Continued)



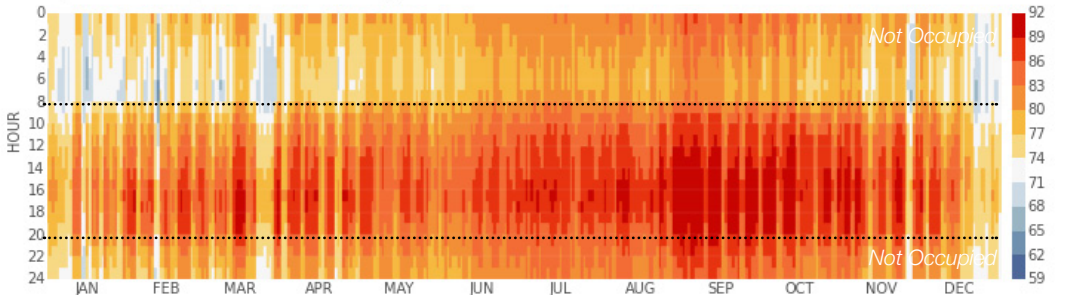
Add/C.3.d CLASSROOM ANALYSIS:: WEST FACING

C.3.d.4. CODE SUITE

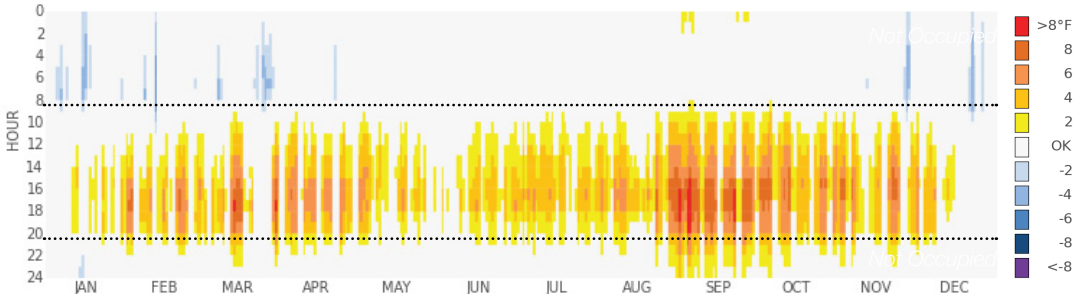
Equal to IMPROVED SUITE + IECC Walls



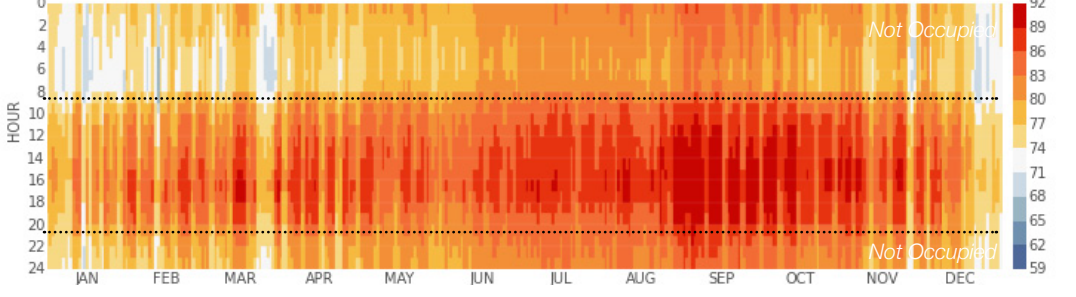
Operative temperature for bottom floor



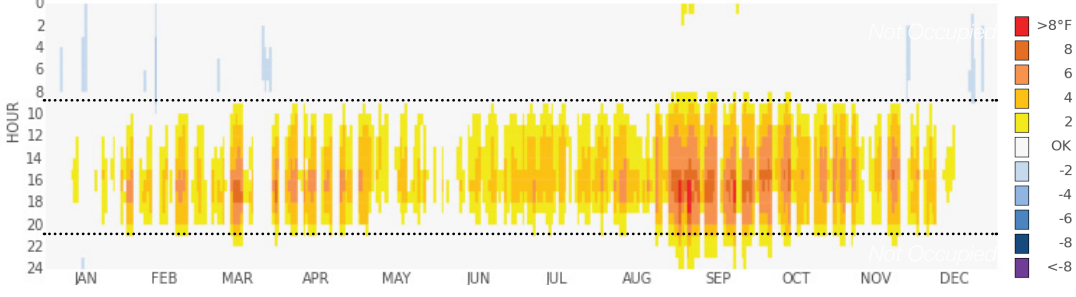
Degrees from comfort for bottom floor



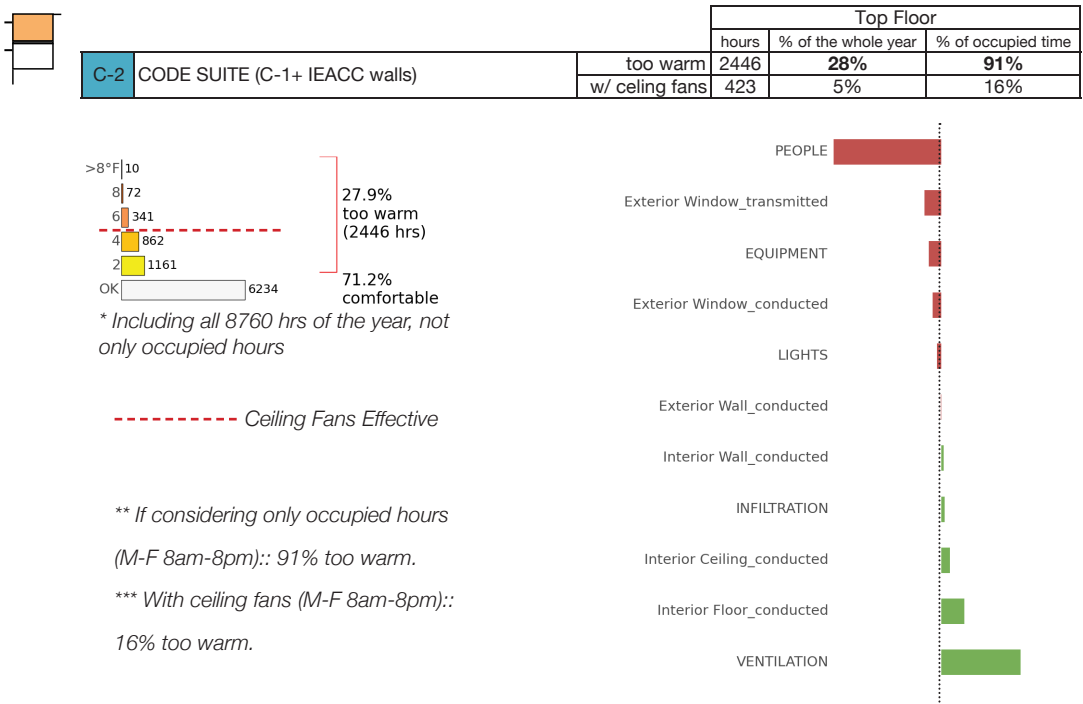
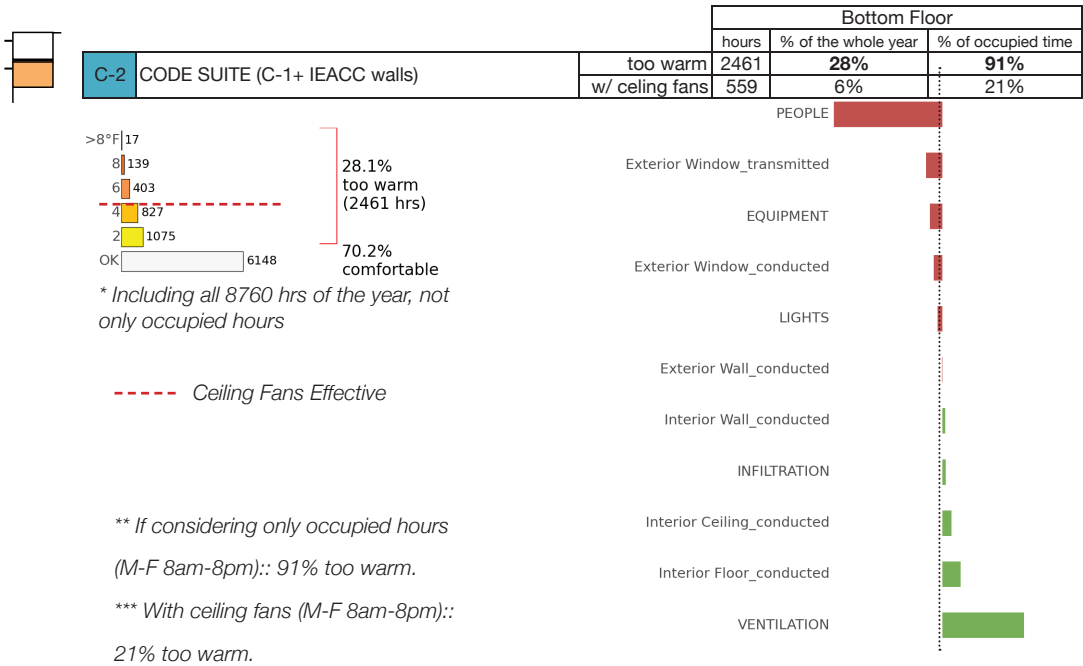
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.d.4 Classroom Analysis:: West Facing (Continued)



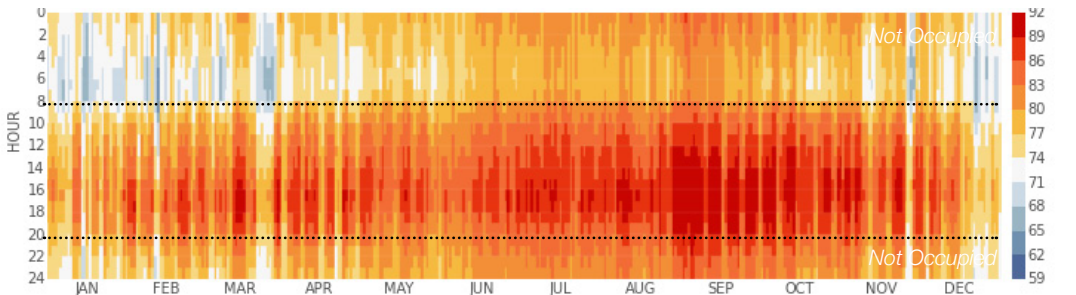
Add/C.3.d CLASSROOM ANALYSIS:: WEST FACING

C.3.d.5. IMPROVED SUITE WITH VENTILATION

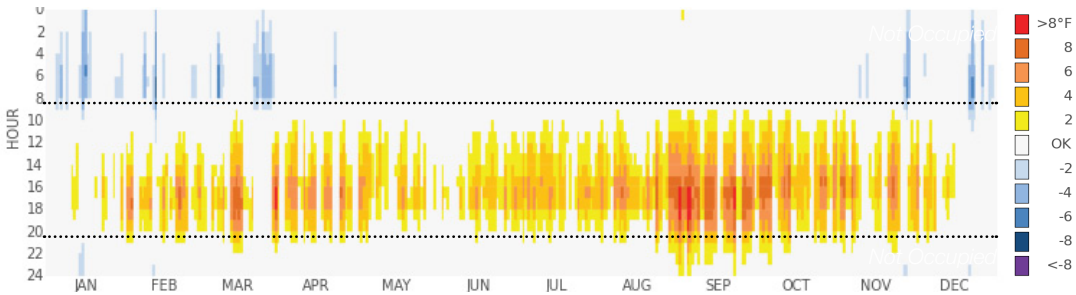
Equal to IMPROVED SUITE +2ACH



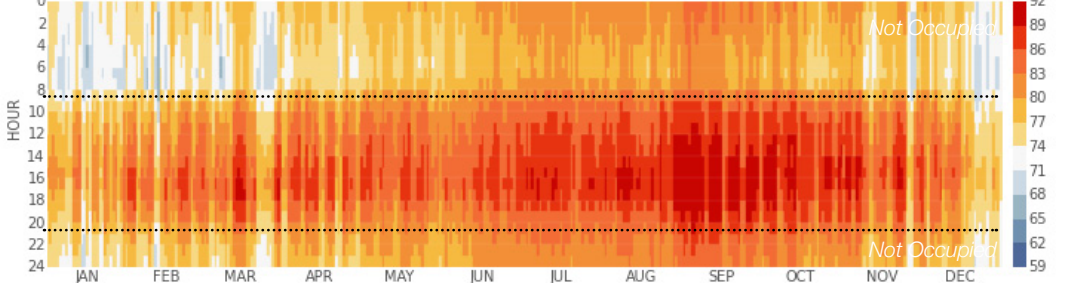
Operative temperature for bottom floor



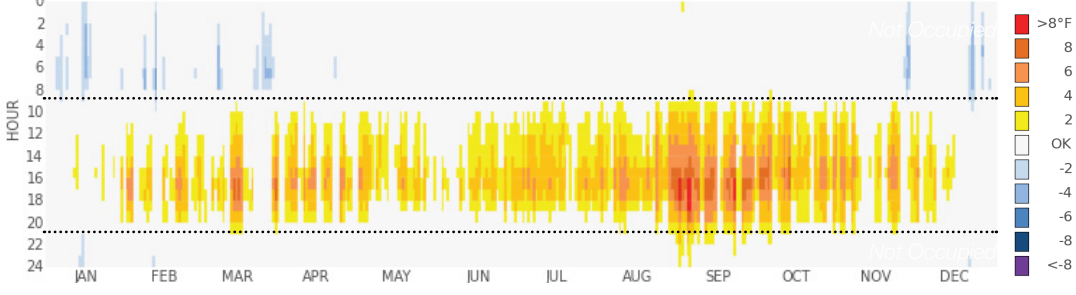
Degrees from comfort for bottom floor



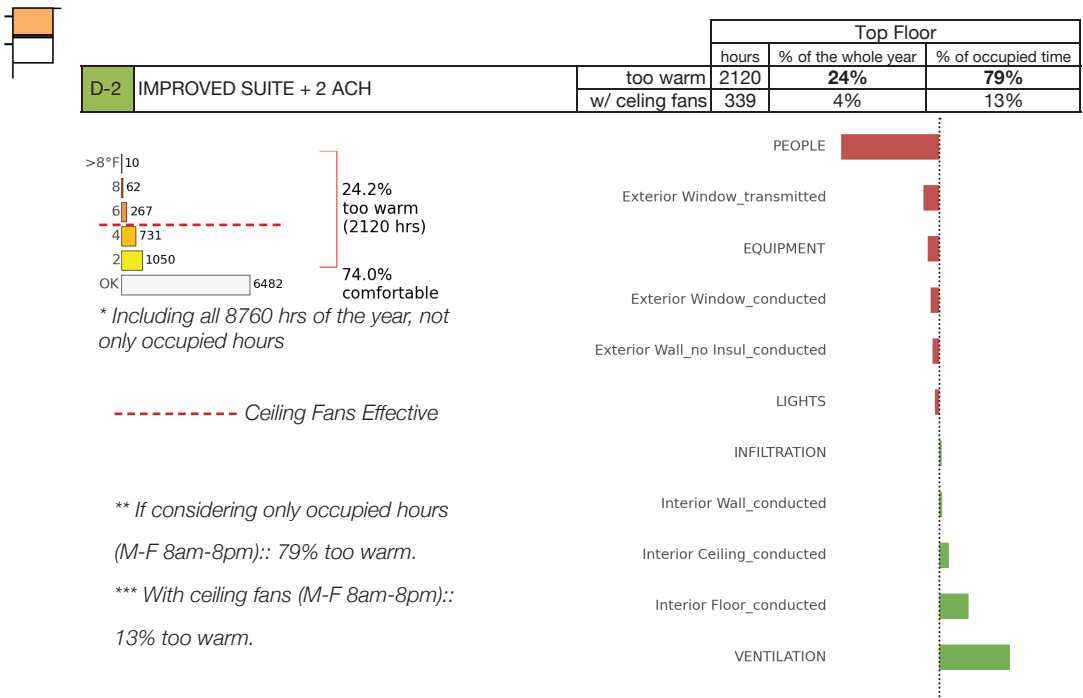
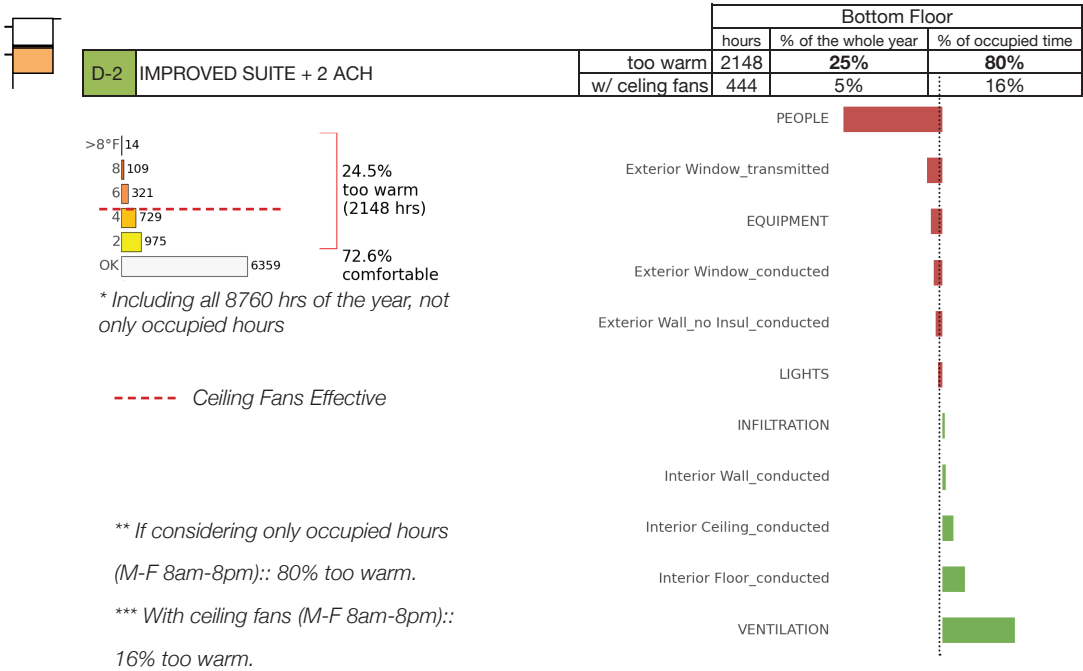
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.d.5 Classroom Analysis:: West Facing (Continued)



Add/C.3.d CLASSROOM ANALYSIS:: WEST FACING

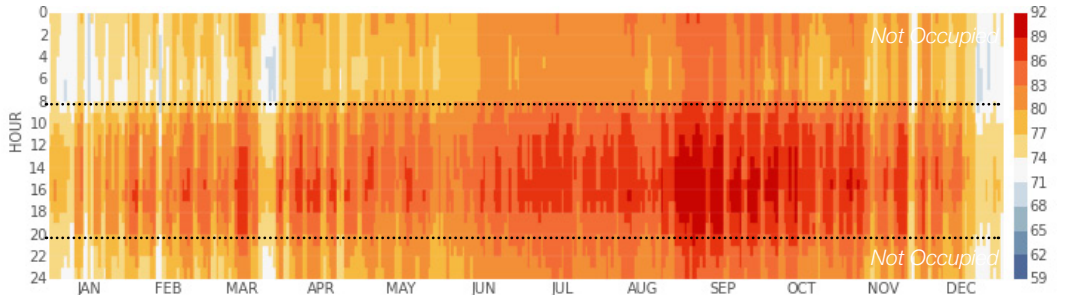


C.3.d.6. IDEAL SUITE

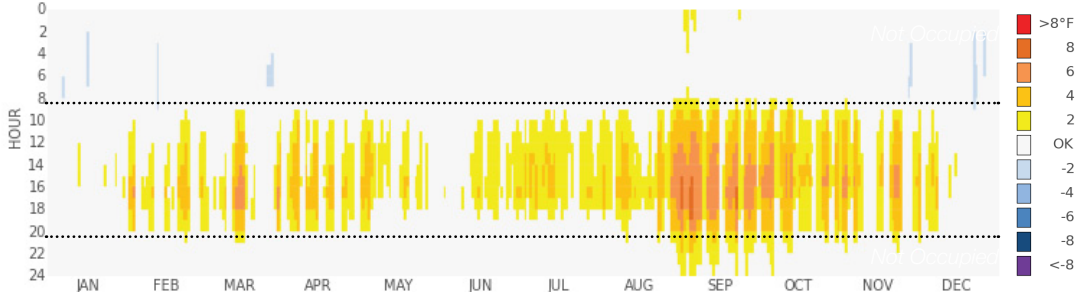
Equal to CODE SUITE + Thermal Mass



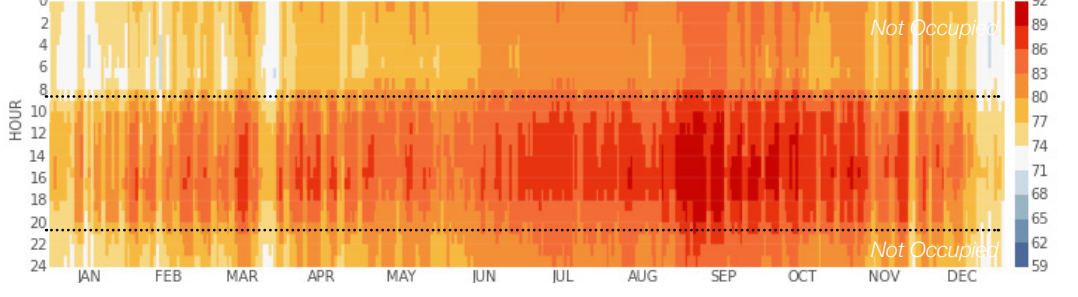
Operative temperature for bottom floor



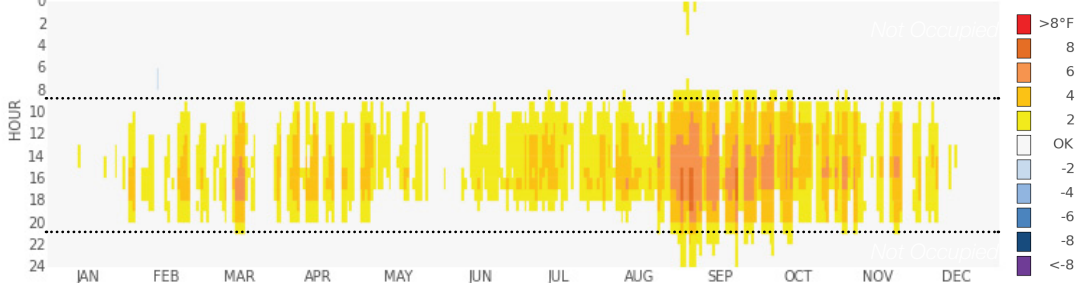
Degrees from comfort for bottom floor



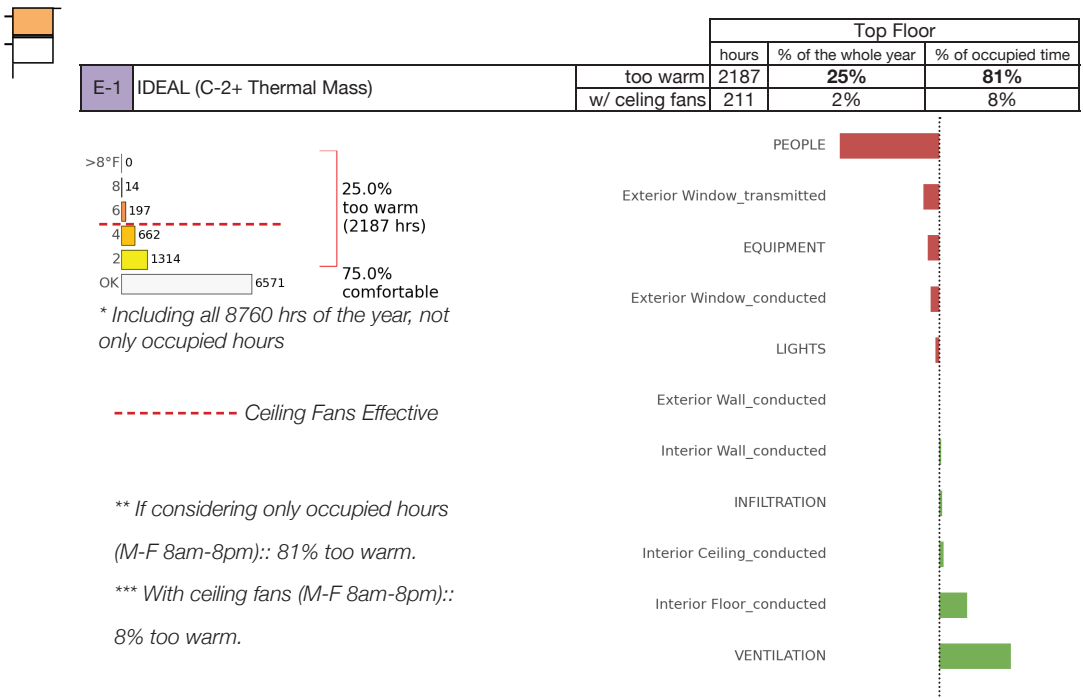
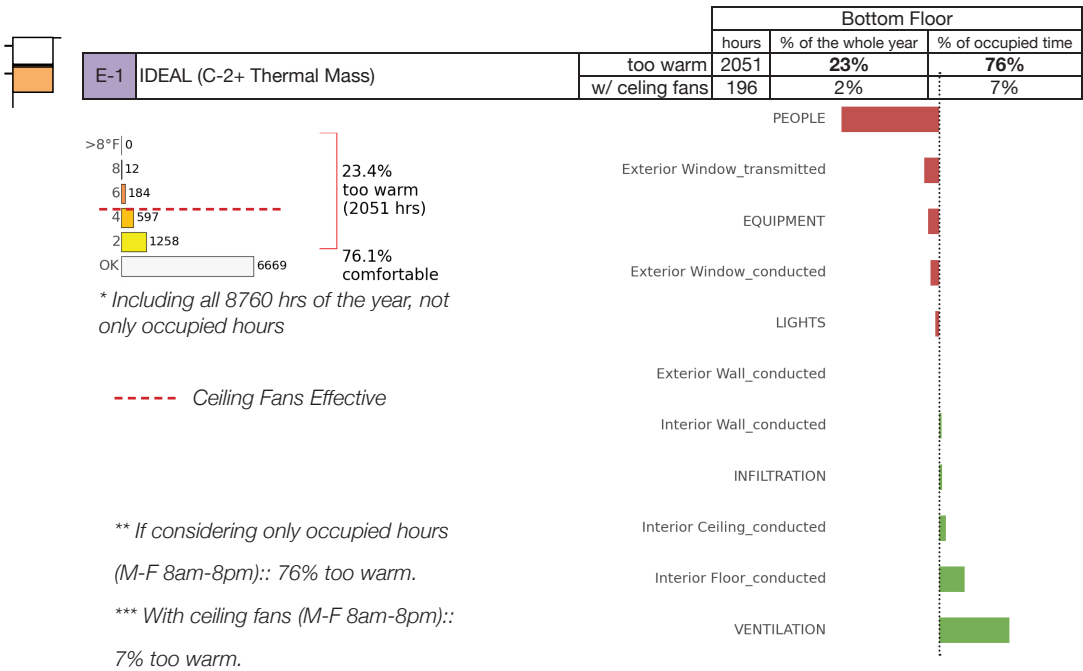
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.d.6 Classroom Analysis:: West Facing (Continued)



Add/C.3.d CLASSROOM ANALYSIS:: WEST FACING

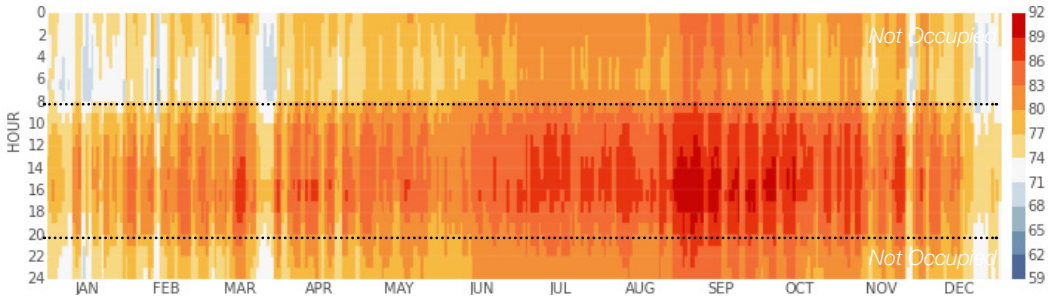


C.3.d.7. IDEAL SUITE WITH VENTILATION

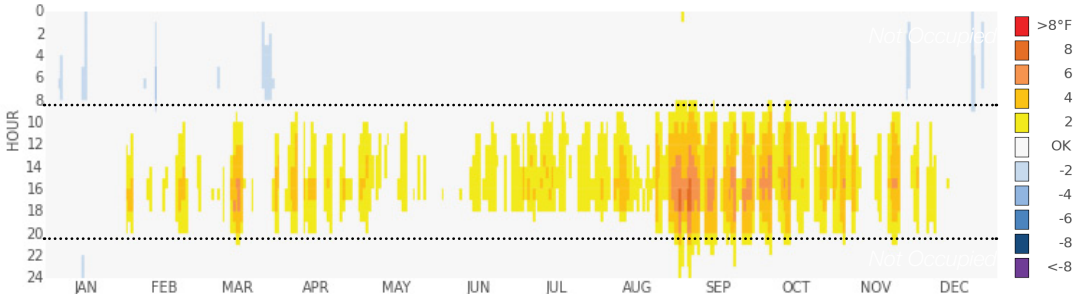
Equal to IDEAL SUITE + 2ACH



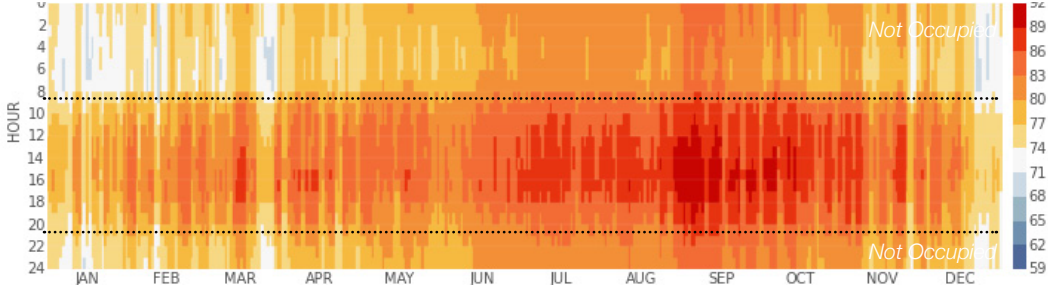
Operative temperature for bottom floor



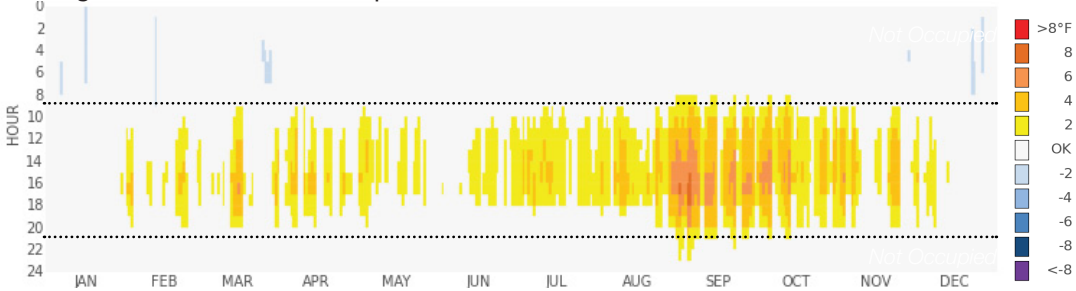
Degrees from comfort for bottom floor



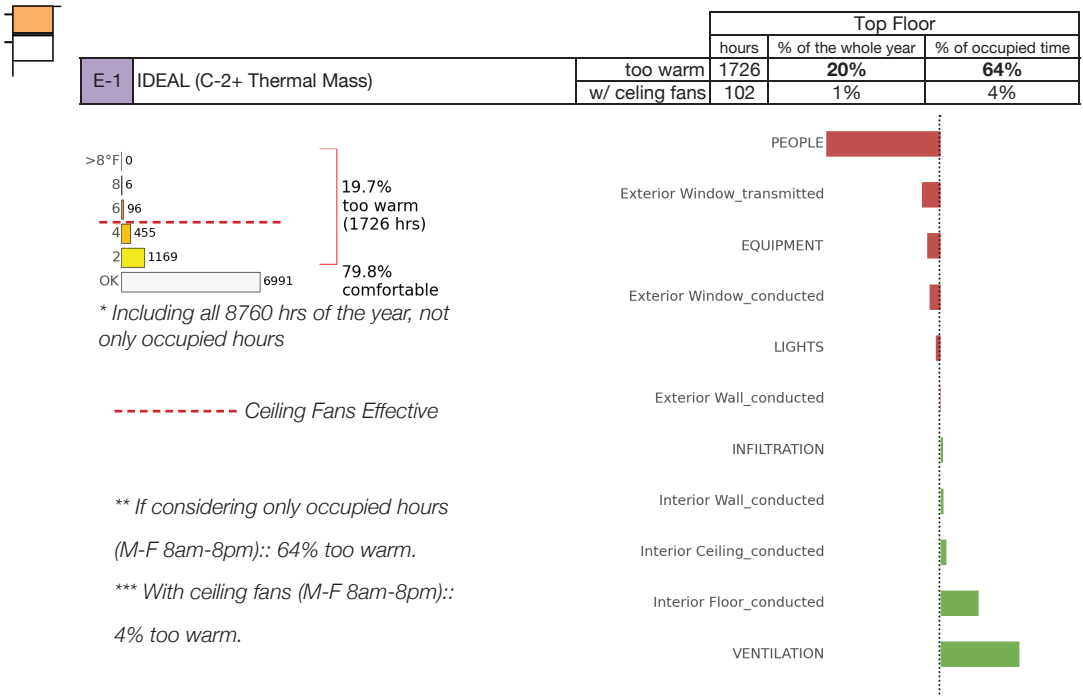
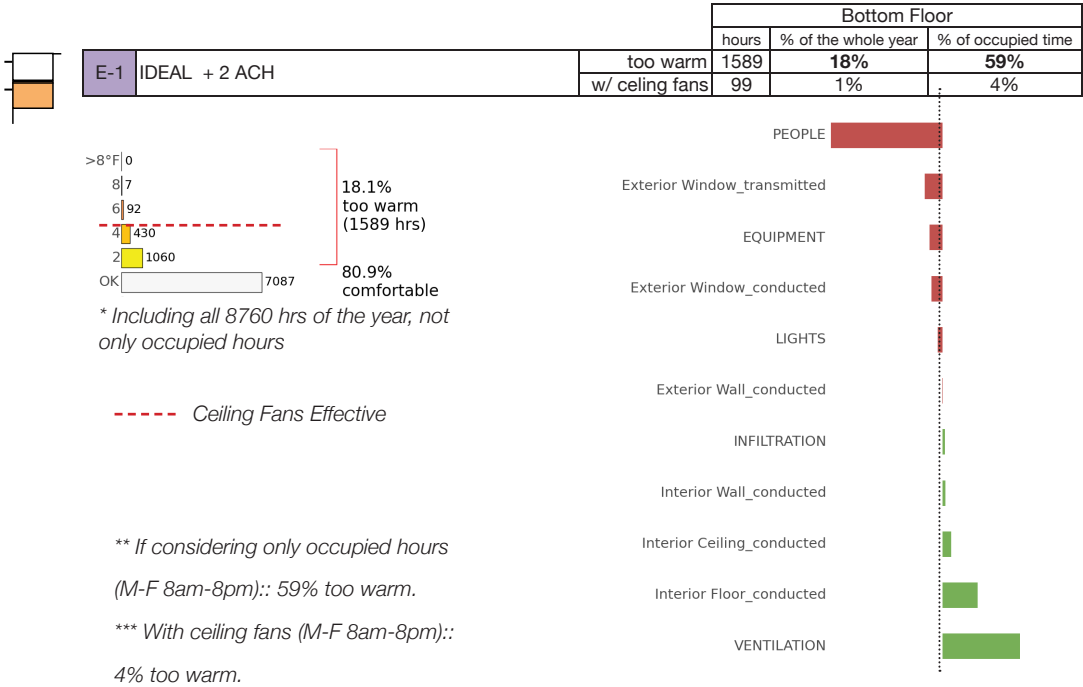
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.3.d.7 Classroom Analysis:: West Facing (Continued)



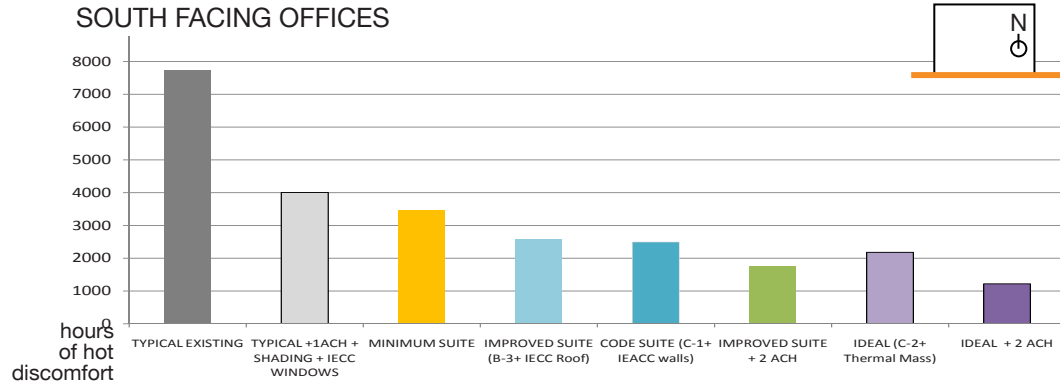
[BLANK]

Add/C. HVAC AUTONOMY AND THERMAL COMFORT STUDIES**4. OFFICE ANALYSIS**

FOR EACH ORIENTATION (a. SOUTH, b. NORTH, c. WEST AND d. EAST)**OPEN OFFICE**

0. **TYPICAL EXISTING**:: No Insulation in Opaque Surfaces, Single Pane Glass Windows
1. TYPICAL + 1ACH + Shading + IECC Glazing
2. **MINIMUM SUITE**:: TYPICAL + 1ACH + IECC Glazing + Shading + lower LPD + daylight controls
3. **IMPROVED SUITE**:: Minimum Suite + IECC Roof
4. **CODE SUITE**:: Improved Suite + IECC Walls
5. IMPROVED SUITE + 2ACH
6. **IDEAL SUITE**:: Code Suite + Thermal Mass
7. IDEAL SUITE + 2ACH

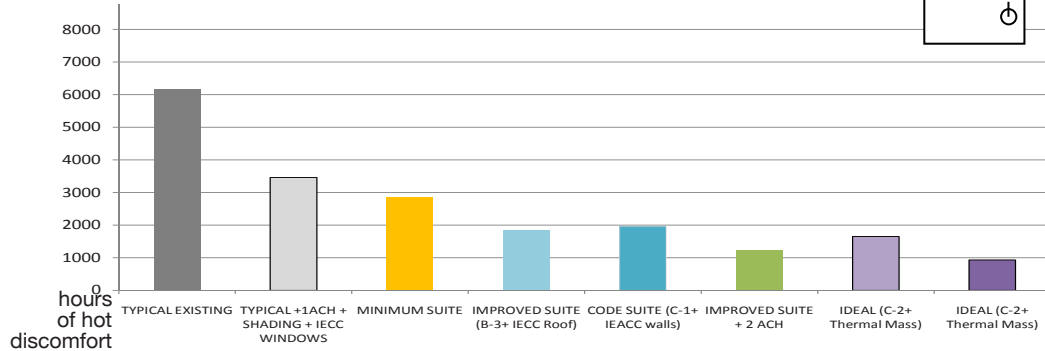
Add/C.4 Office Analysis (Continued)



Scenario	Category	Bottom Floor			Top Floor		
		hours	% of the whole year	% of occupied time	hours	% of the whole year	% of occupied time
TYPICAL EXISTING	too warm	8384	96%	100%	7736	88%	100%
	w/ ceiling fans	7209	82%	100%	6339	72%	100%
A-3 TYPICAL +1ACH + SHADING + IECC WINDOWS	too warm	3766	43%	100%	4003	46%	100%
	w/ ceiling fans	1865	19%	82%	2254	26%	100%
B-3 MINIMUM SUITE	too warm	2763	32%	100%	3452	39%	100%
	w/ ceiling fans	705	8%	35%	1623	19%	80%
C-1 IMPROVED SUITE (B-3+ IECC Roof)	too warm	2572	29%	100%	2593	30%	100%
	w/ ceiling fans	855	10%	42%	752	9%	37%
C-2 CODE SUITE (C-1+ IEACC walls)	too warm	2506	29%	100%	2493	28%	100%
	w/ ceiling fans	501	6%	25%	393	4%	19%
D-2 IMPROVED SUITE + 2 ACH	too warm	1739	20%	86%	1746	20%	86%
	w/ ceiling fans	269	3%	13%	212	2%	10%
E-1 IDEAL (C-2+ Thermal Mass)	too warm	2028	23%	100%	2180	25%	100%
	w/ ceiling fans	203	2%	10%	197	2%	10%
E-2 IDEAL + 2 ACH	too warm	1060	12%	52%	1216	14%	60%
	w/ ceiling fans	32	0%	2%	33	0%	2%

Add/C.4 Office Analysis (Continued)

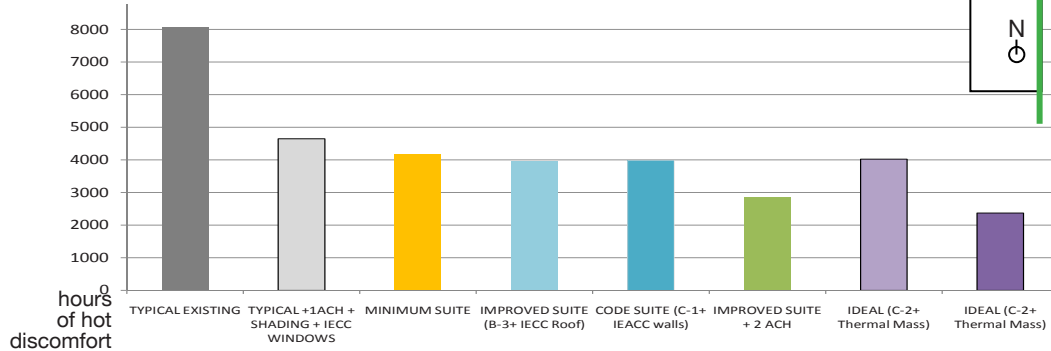
NORTH FACING OFFICES



Scenario	w/ ceiling fans	Bottom Floor			Top Floor		
		hours	% of the whole year	% of occupied time	hours	% of the whole year	% of occupied time
TYPICAL EXISTING	too warm	6863	78%	100%	6181	71%	100%
	w/ ceiling fans	3001	57%	100%	4365	50%	100%
A-3 TYPICAL +1ACH + SHADING + IECC WINDOWS	too warm	3026	35%	100%	3458	39%	100%
	w/ ceiling fans	1077	12%	53%	1792	20%	88%
B-3 MINIMUM SUITE	too warm	2007	23%	99%	2850	33%	100%
	w/ ceiling fans	169	2%	8%	1162	13%	57%
C-1 IMPROVED SUITE (B-3+ IECC Roof)	too warm	1814	21%	90%	1835	21%	91%
	w/ ceiling fans	122	1%	6%	172	2%	8%
C-2 CODE SUITE (C-1+ IEACC walls)	too warm	1881	21%	93%	1949	22%	96%
	w/ ceiling fans	149	2%	7%	120	1%	6%
D-2 IMPROVED SUITE + 2 ACH	too warm	1175	13%	58%	1217	14%	60%
	w/ ceiling fans	29	0%	1%	17	0%	1%
E-1 IDEAL (C-2+ Thermal Mass)	too warm	1462	17%	72%	1653	19%	82%
	w/ ceiling fans	32	0%	2%	40	0%	2%
E-1 IDEAL + 2 ACH	too warm	728	8%	36%	934	11%	46%
	w/ ceiling fans	0	0%	0%	0	0%	0%

Add/C.4 Office Analysis (Continued)

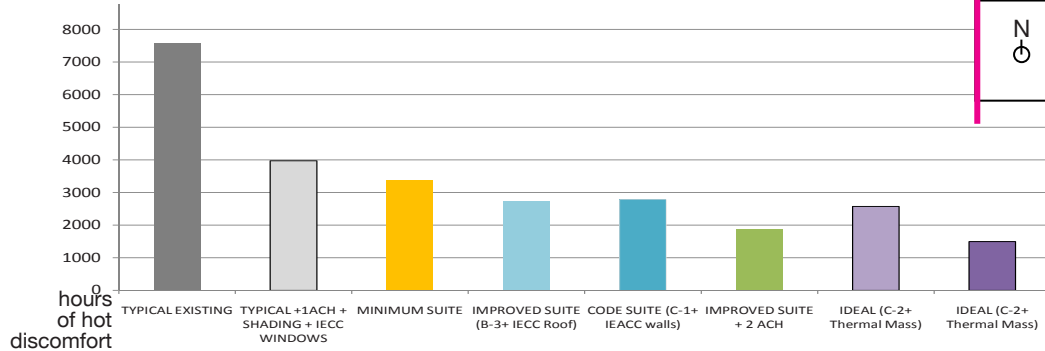
EAST FACING OFFICES



Scenario	Bottom Floor			Top Floor				
	hours	% of the whole year	% of occupied time	hours	% of the whole year	% of occupied time		
TYPICAL EXISTING	too warm	8497	97%	100%	too warm	8064	92%	100%
	w/ ceiling fans	7948	91%	100%	w/ ceiling fans	7175	82%	100%
A-3 TYPICAL +1ACH + SHADING + IECC WINDOWS	too warm	4801	55%	100%	too warm	4547	53%	100%
	w/ ceiling fans	2582	29%	100%	w/ ceiling fans	2876	33%	100%
B-3 MINIMUM SUITE	too warm	4035	46%	100%	too warm	4158	47%	100%
	w/ ceiling fans	1795	20%	89%	w/ ceiling fans	2298	26%	100%
C-1 IMPROVED SUITE (B-3+ IECC Roof)	too warm	3934	45%	100%	too warm	3951	45%	100%
	w/ ceiling fans	1700	19%	84%	w/ ceiling fans	1533	18%	76%
C-2 CODE SUITE (C-1+ IEACC walls)	too warm	3928	45%	100%	too warm	3975	45%	100%
	w/ ceiling fans	1561	18%	77%	w/ ceiling fans	1366	16%	67%
D-2 IMPROVED SUITE + 2 ACH	too warm	2870	33%	100%	too warm	2847	33%	100%
	w/ ceiling fans	830	9%	41%	w/ ceiling fans	680	8%	34%
E-1 IDEAL (C-2+ Thermal Mass)	too warm	3964	45%	100%	too warm	4020	46%	100%
	w/ ceiling fans	932	11%	46%	w/ ceiling fans	945	11%	47%
E-1 IDEAL + 2 ACH	too warm	2339	27%	100%	too warm	2372	27%	100%
	w/ ceiling fans	184	2%	9%	w/ ceiling fans	194	2%	10%

Add/C.4 Office Analysis (Continued)

WEST FACING OFFICES



Scenario	Floor	Condition	Bottom Floor			Top Floor		
			hours	% of the whole year	% of occupied time	hours	% of the whole year	% of occupied time
TYPICAL EXISTING		too warm	8202	94%	100%	7591	87%	100%
		w/ ceiling fans	7303	83%	100%	6271	72%	100%
A-3 TYPICAL +1ACH + SHADING + IECC WINDOWS		too warm	3857	44%	100%	3972	45%	100%
		w/ ceiling fans	1677	19%	83%	2258	26%	100%
B-3 MINIMUM SUITE		too warm	2879	33%	100%	3380	39%	100%
		w/ ceiling fans	787	9%	39%	1641	19%	81%
C-1 IMPROVED SUITE (B-3 + IECC Roof)		too warm	2717	31%	100%	2742	31%	100%
		w/ ceiling fans	653	7%	32%	571	7%	28%
C-2 CODE SUITE (C-1 + IEACC walls)		too warm	2723	31%	100%	2779	32%	100%
		w/ ceiling fans	575	7%	28%	498	6%	25%
D-2 IMPROVED SUITE + 2 ACH		too warm	1862	21%	92%	1879	21%	93%
		w/ ceiling fans	310	4%	15%	253	3%	12%
E-1 IDEAL (C-2+ Thermal Mass)		too warm	2449	28%	100%	2573	29%	100%
		w/ ceiling fans	282	3%	14%	304	3%	15%
E-1 IDEAL + 2 ACH		too warm	1332	15%	66%	1493	17%	74%
		w/ ceiling fans	74	1%	4%	84	1%	4%

Add/C.4.a. OFFICE ANALYSIS:: SOUTH FACING

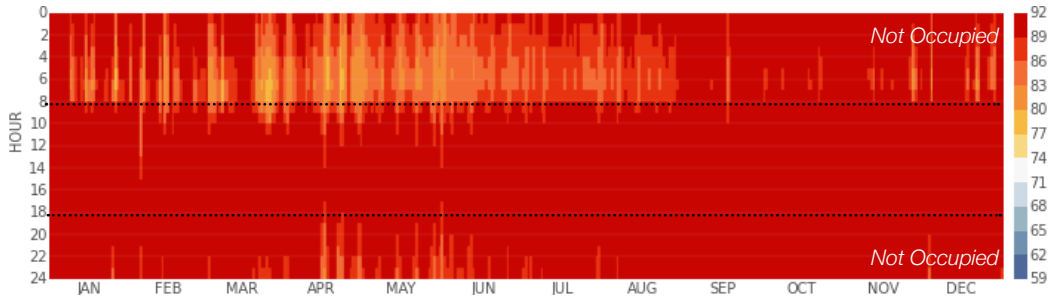
C.4.a.0. TYPICAL EXISTING



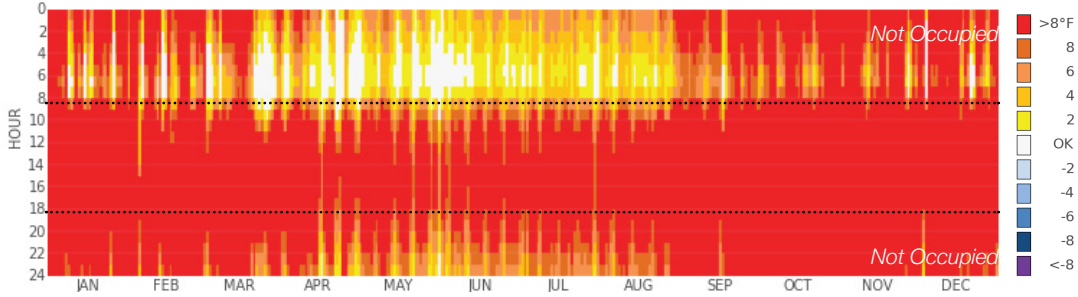
No Insulation in Opaque Surfaces and Single Pane Glass



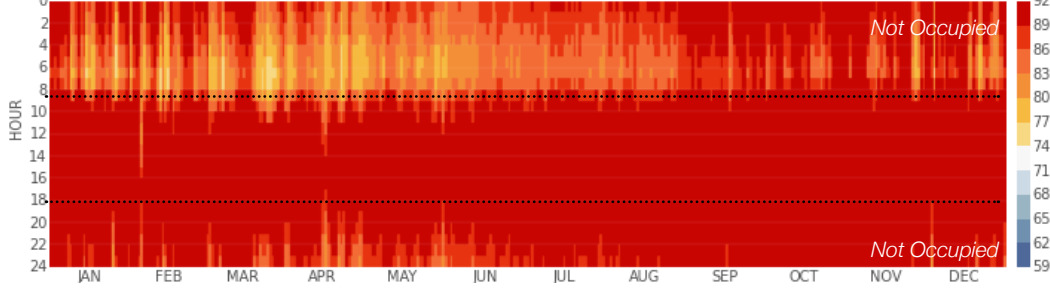
Operative temperature for bottom floor



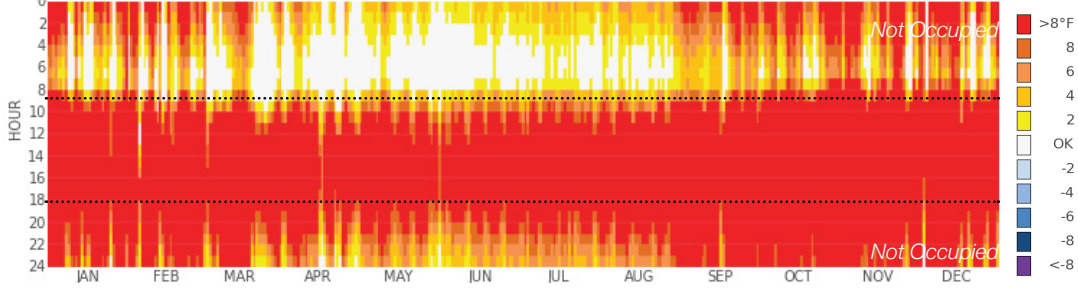
Degrees from comfort for bottom floor



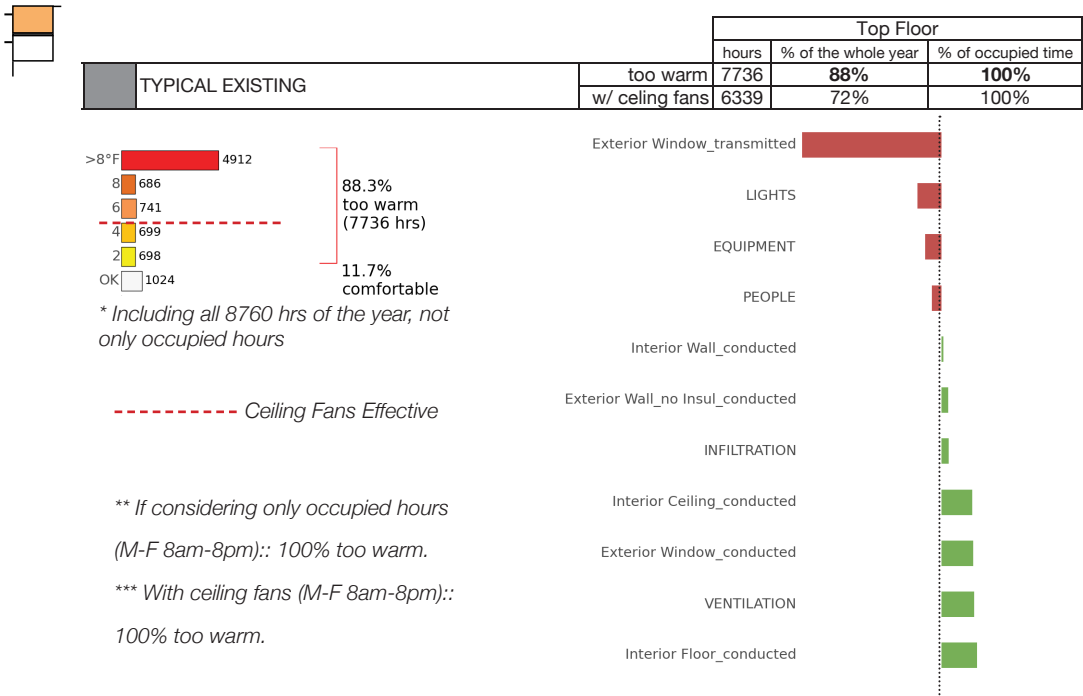
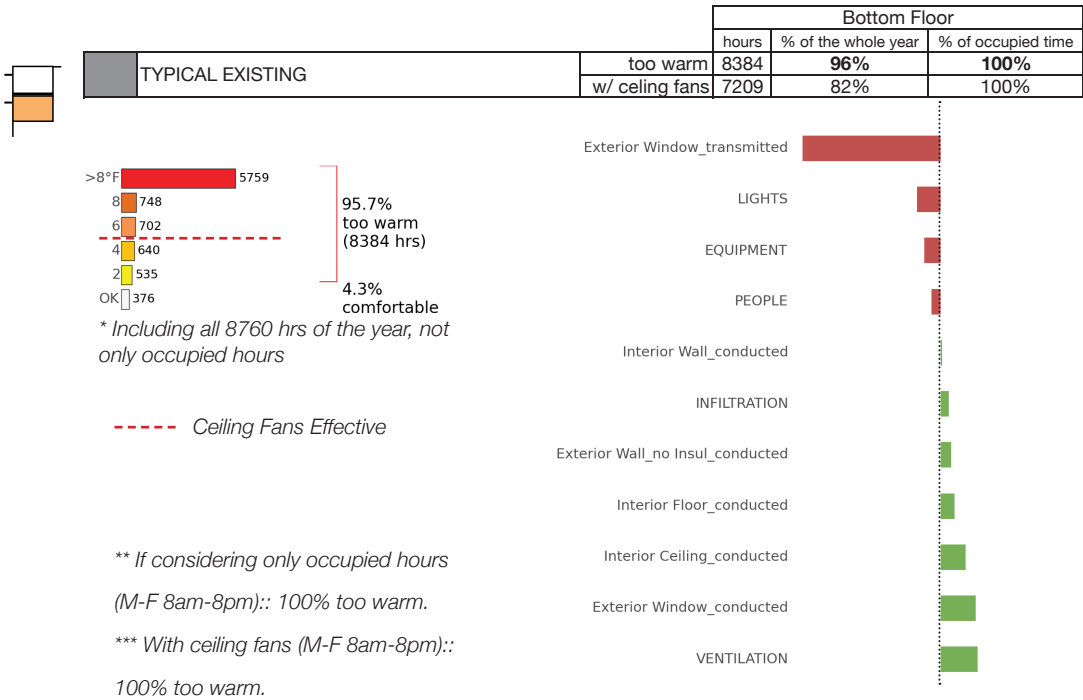
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.a.0 Office Analysis:: South Facing (Continued)



Add/C.4.a. OFFICE ANALYSIS:: SOUTH FACING

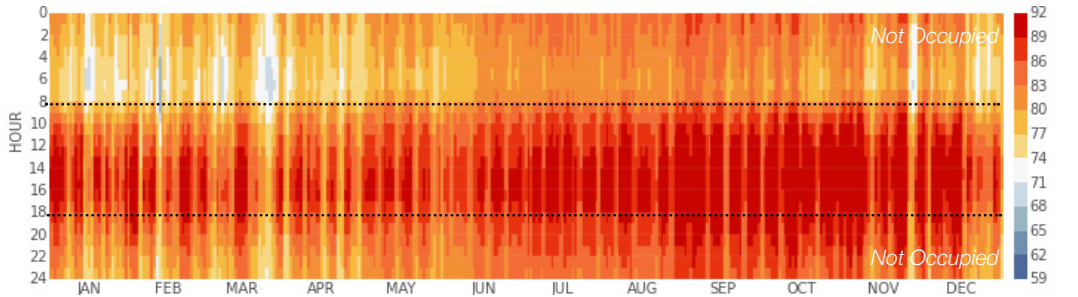
C.4.a.1.TYPICAL WITH WINDOW IMPROVEMENTS



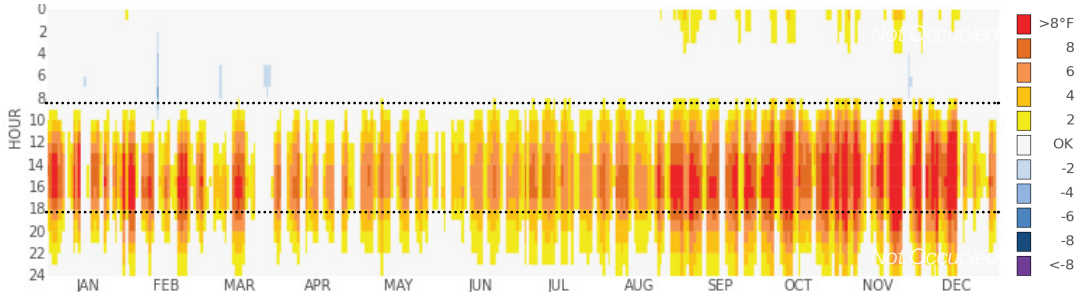
Equal to TYPICAL + 1ACH + Shading + IECC 2015 Windows



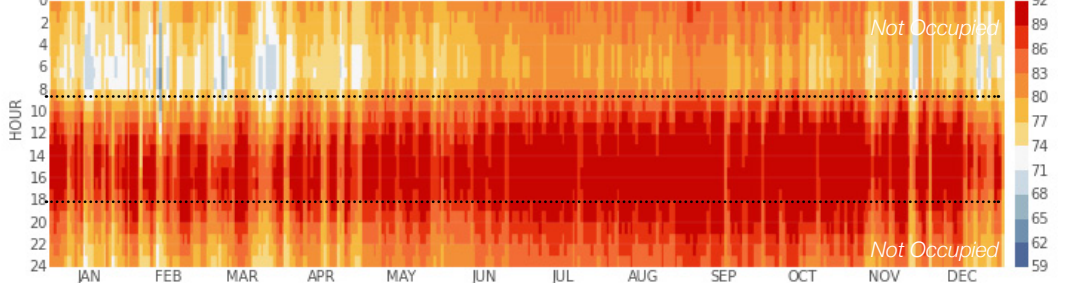
Operative temperature for bottom floor



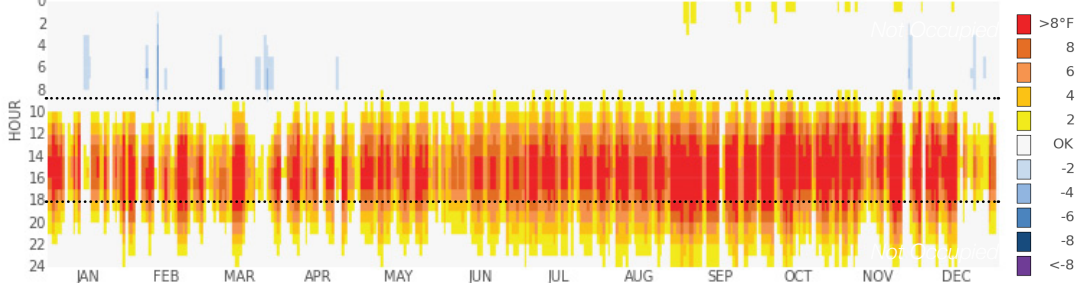
Degrees from comfort for bottom floor



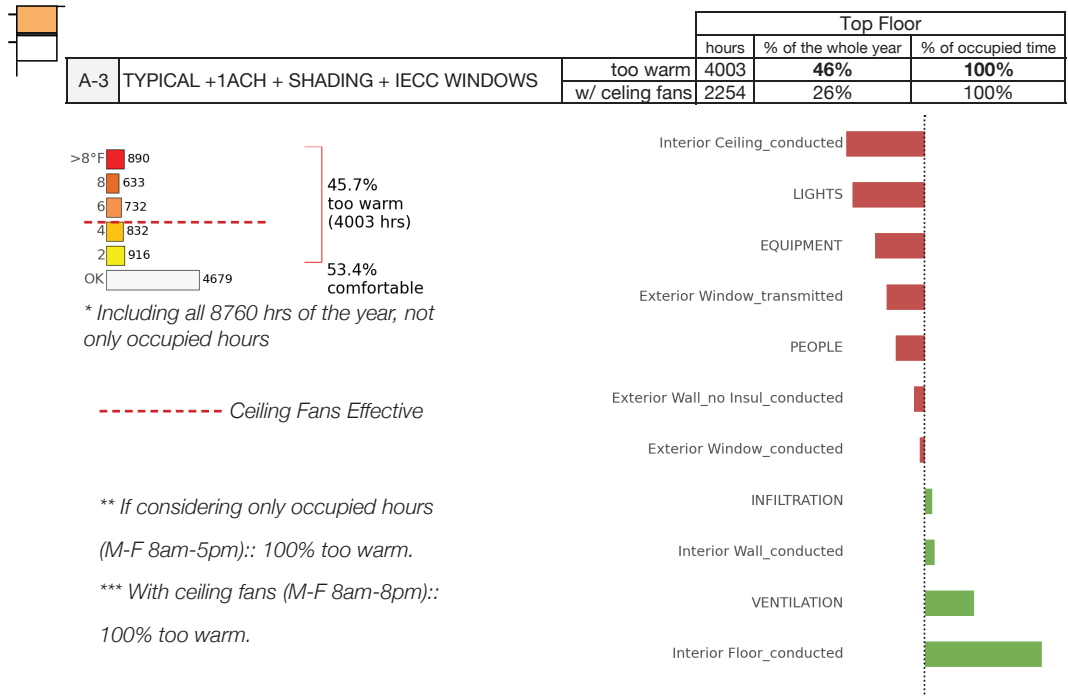
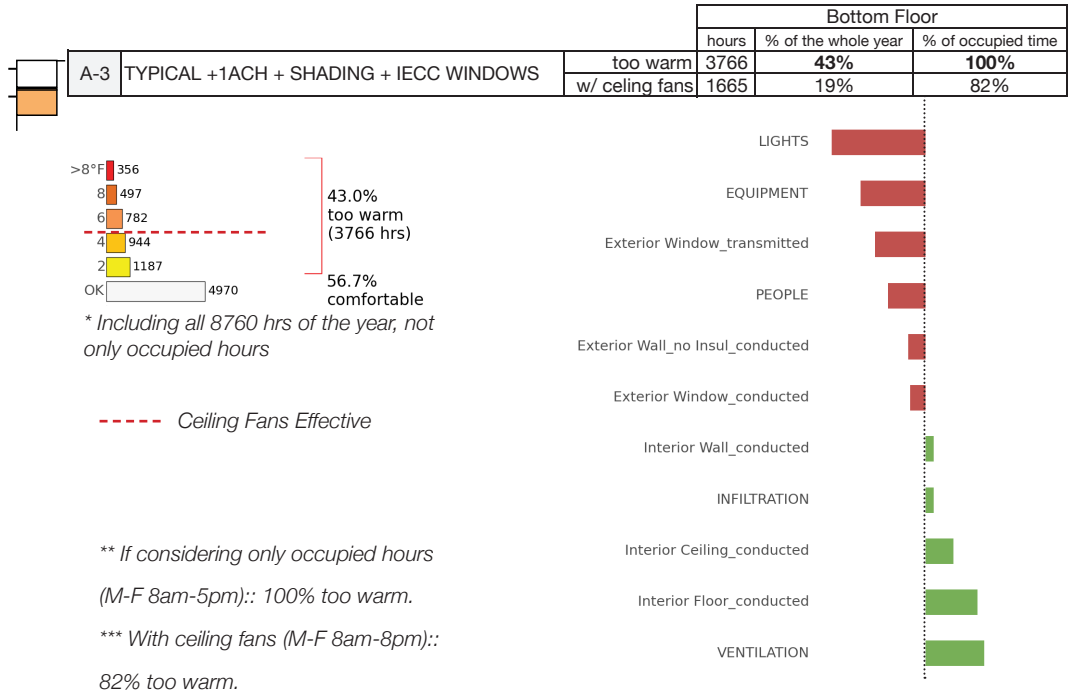
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.a.1 Office Analysis:: South Facing (Continued)



Add/C.4.a. OFFICE ANALYSIS:: SOUTH FACING

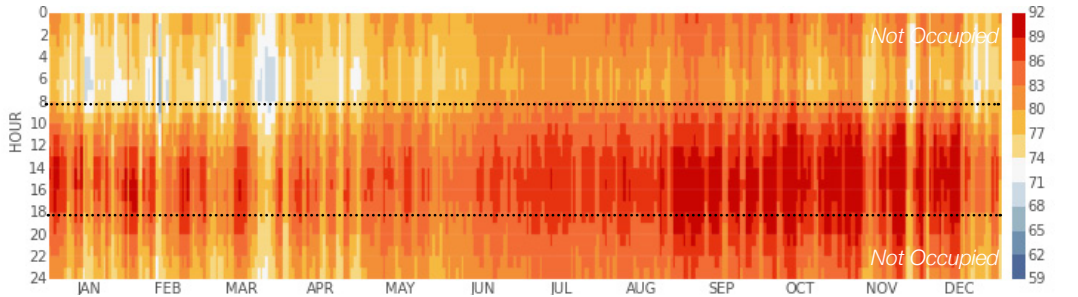
C.4.a.2. MINIMUM SUITE



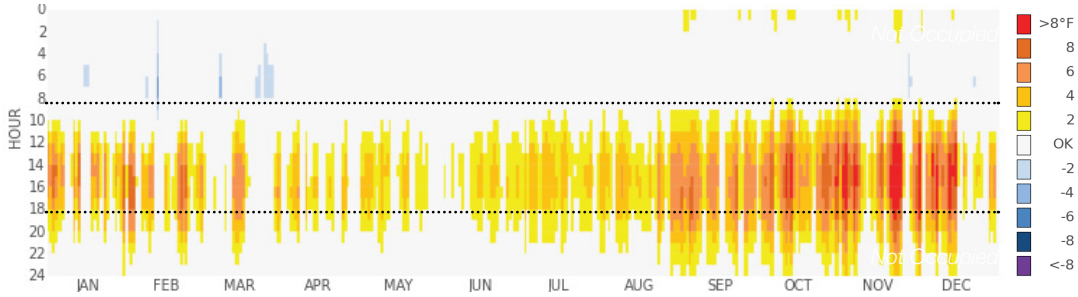
Equal to TYPICAL + IECC Windows + Shading +lower LPD + Daylight Controls +1ACH



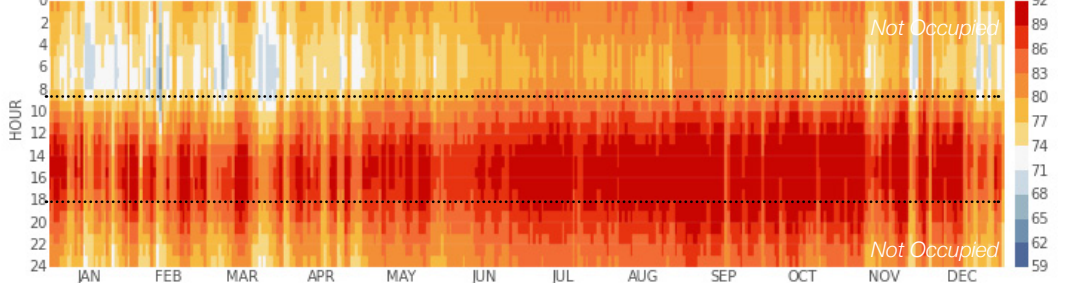
Operative temperature for bottom floor



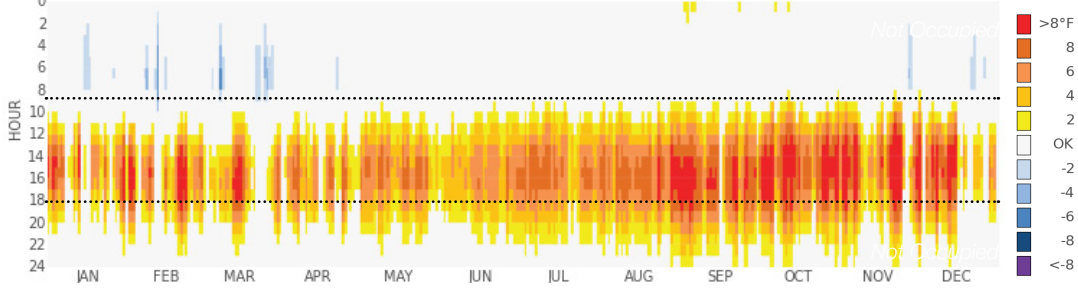
Degrees from comfort for bottom floor



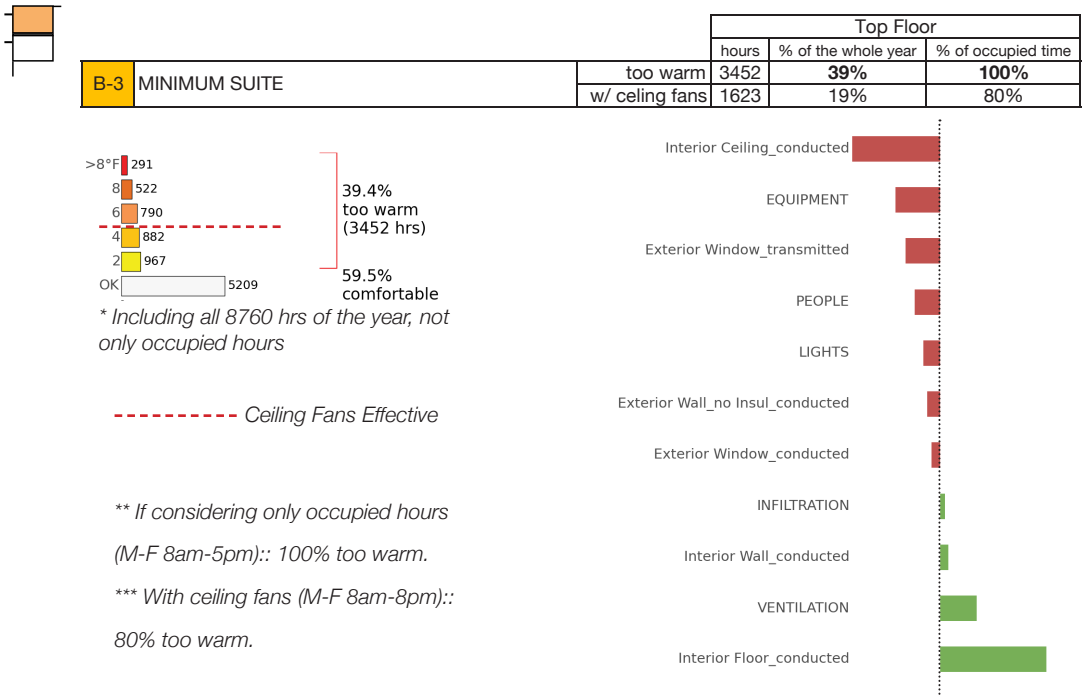
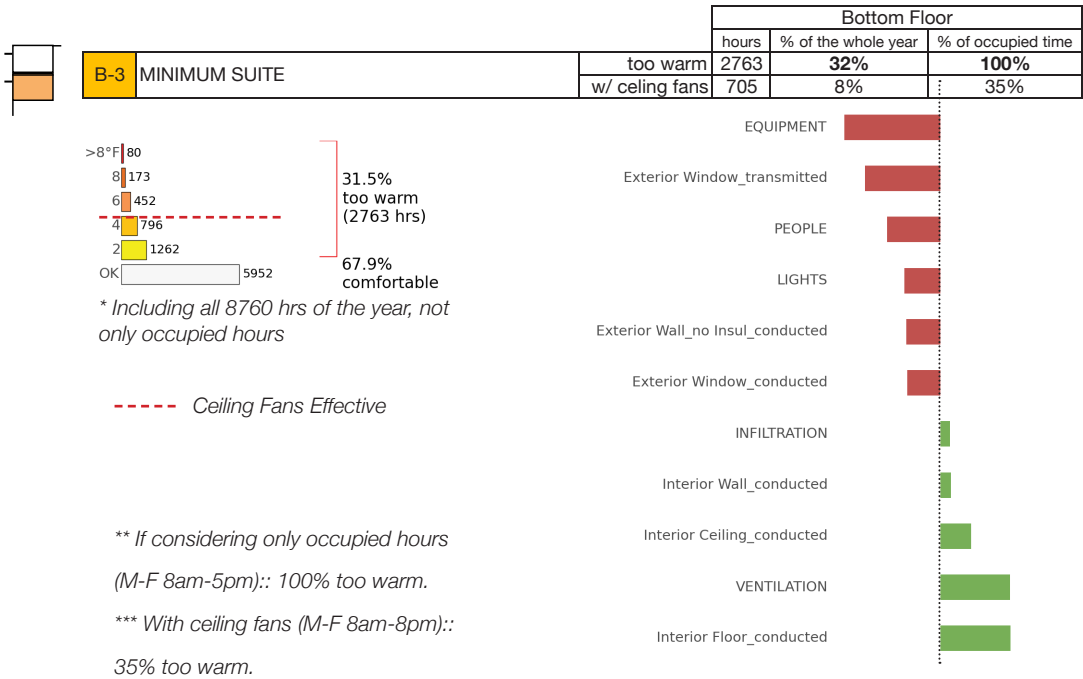
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.a.2 Office Analysis:: South Facing (Continued)



Add/C.4.a. OFFICE ANALYSIS:: SOUTH FACING

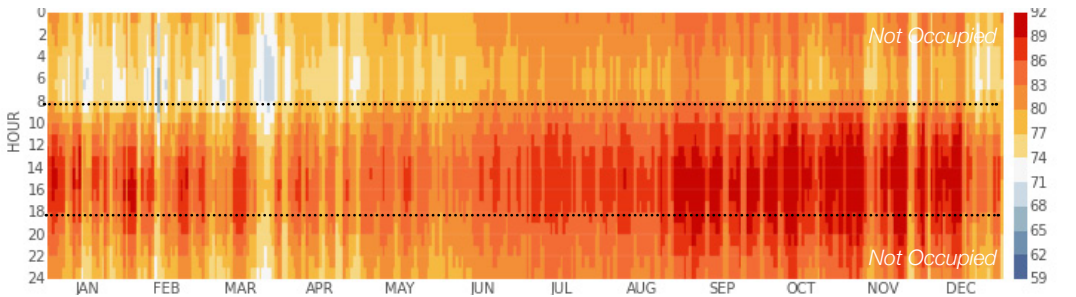
C.4.a.3. IMPROVED SUITE



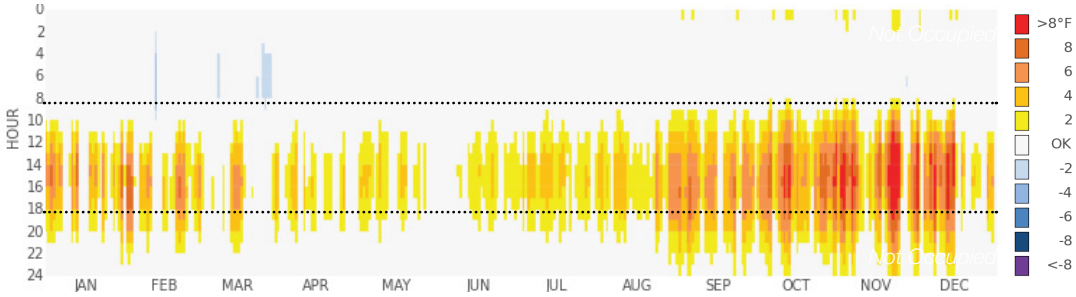
Equal to MINIMUM SUITE + IECC Roof



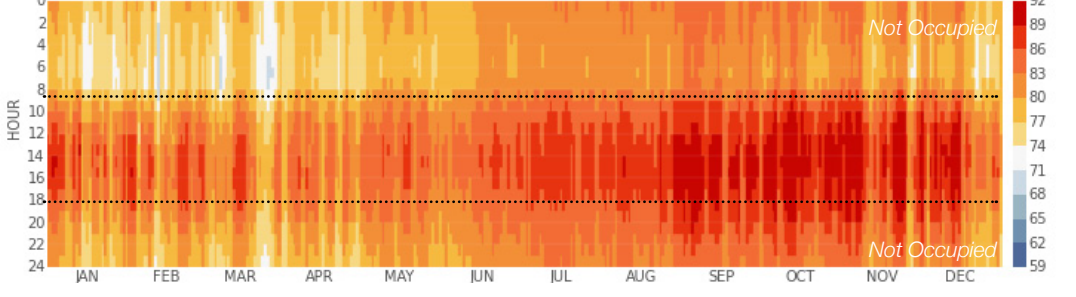
Operative temperature for bottom floor



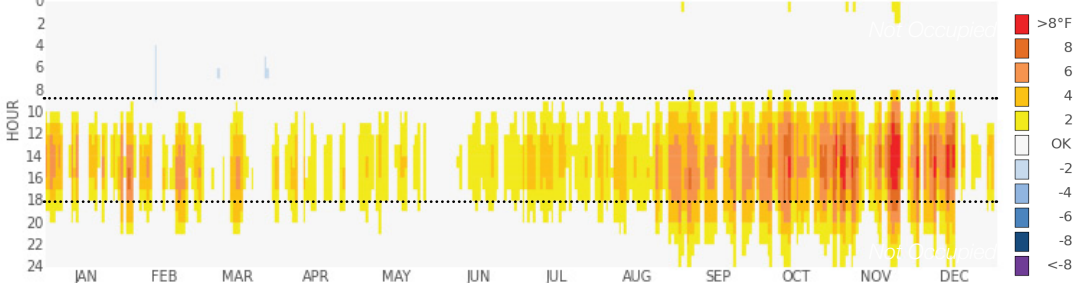
Degrees from comfort for bottom floor



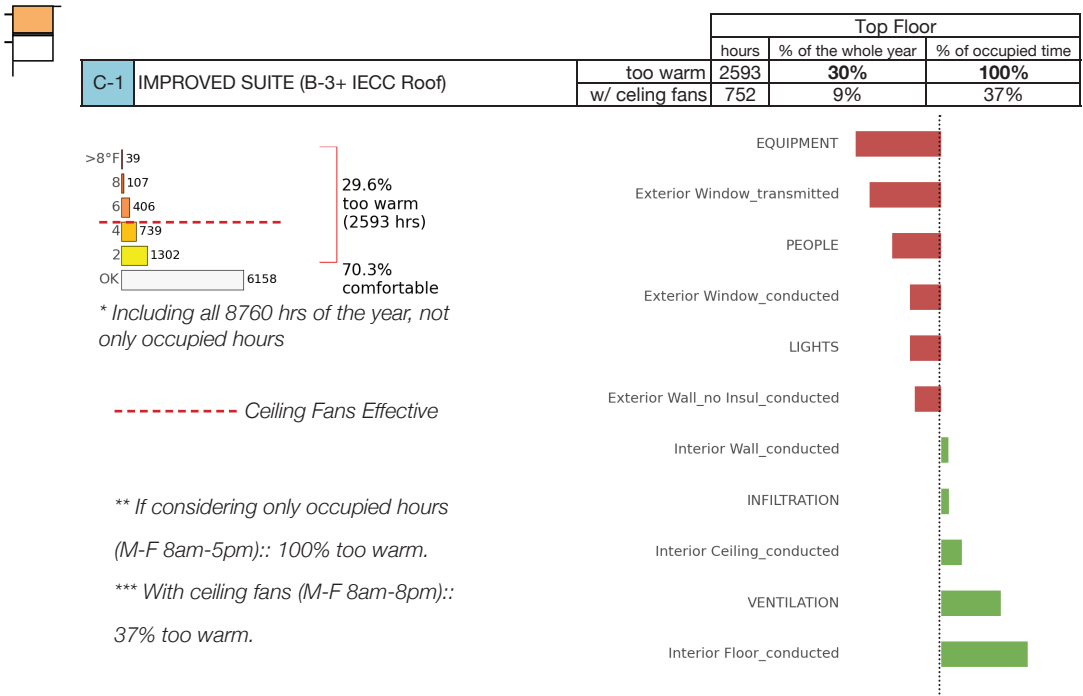
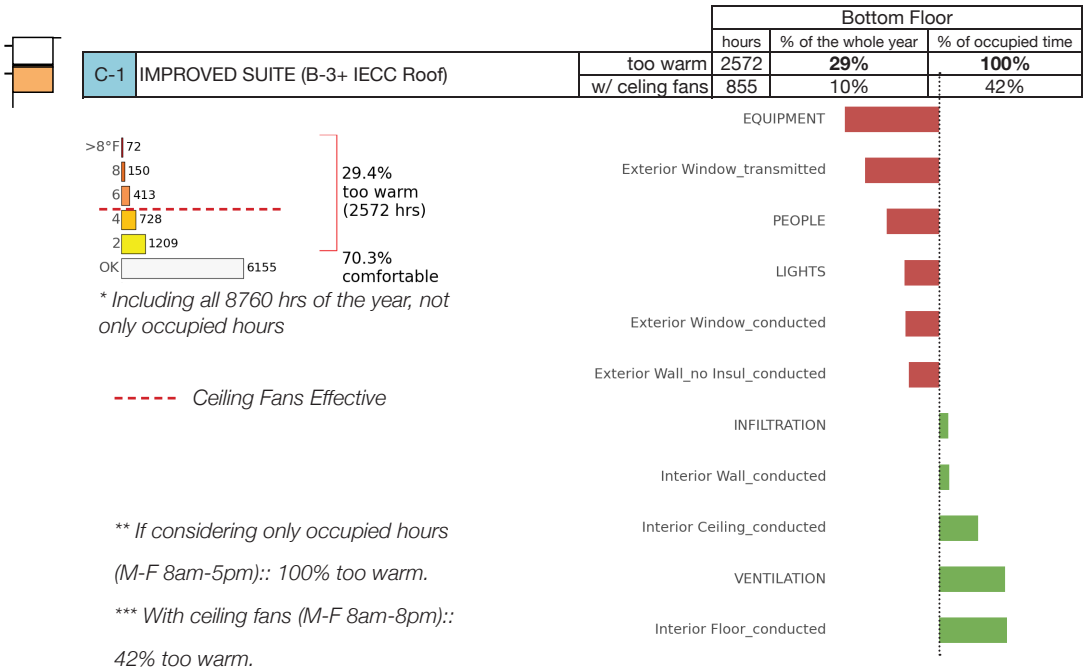
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.a.3 Office Analysis:: South Facing (Continued)



Add/C.4.a. OFFICE ANALYSIS:: SOUTH FACING

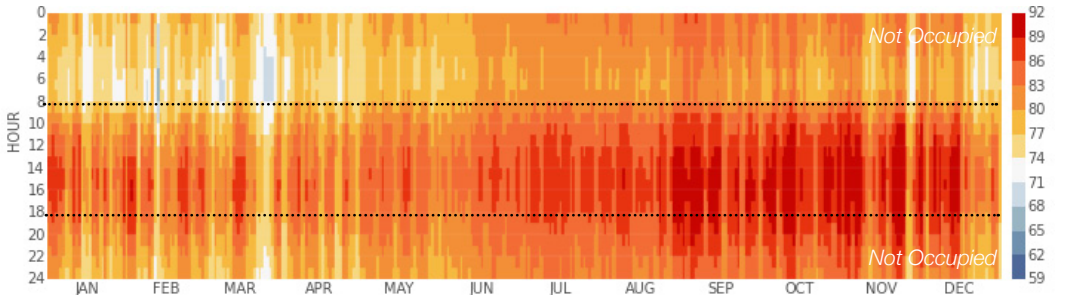
C.4.a.4. CODE SUITE



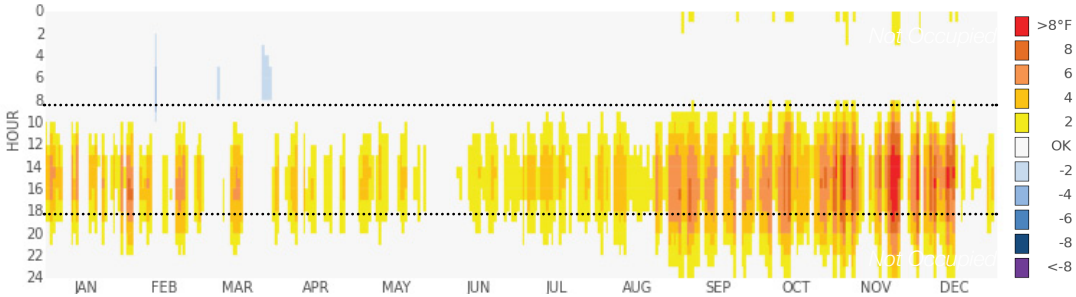
Equal to IMPROVED SUITE + IECC Walls



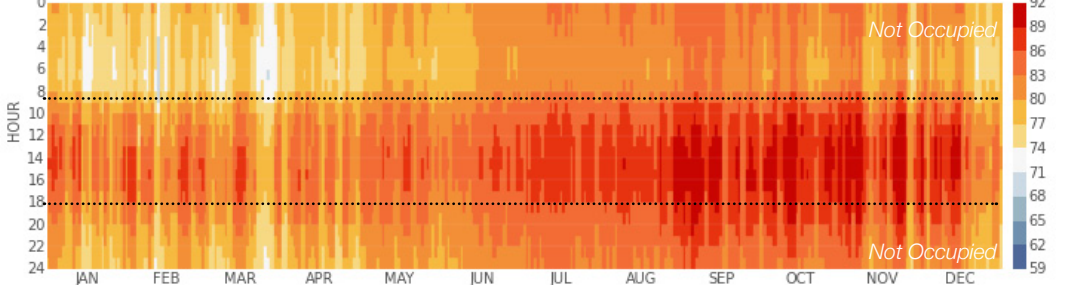
Operative temperature for bottom floor



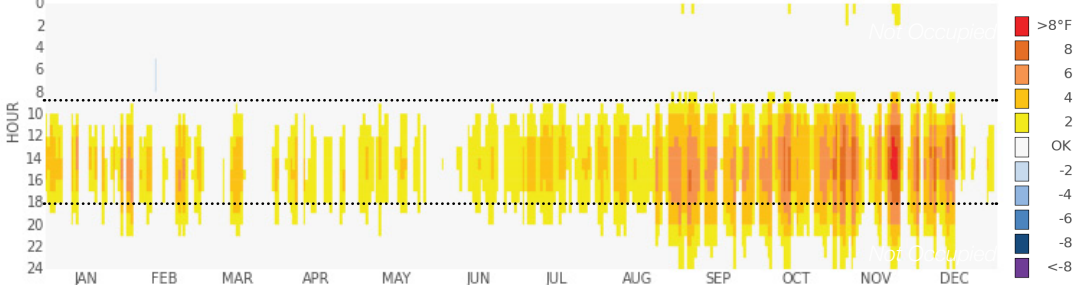
Degrees from comfort for bottom floor



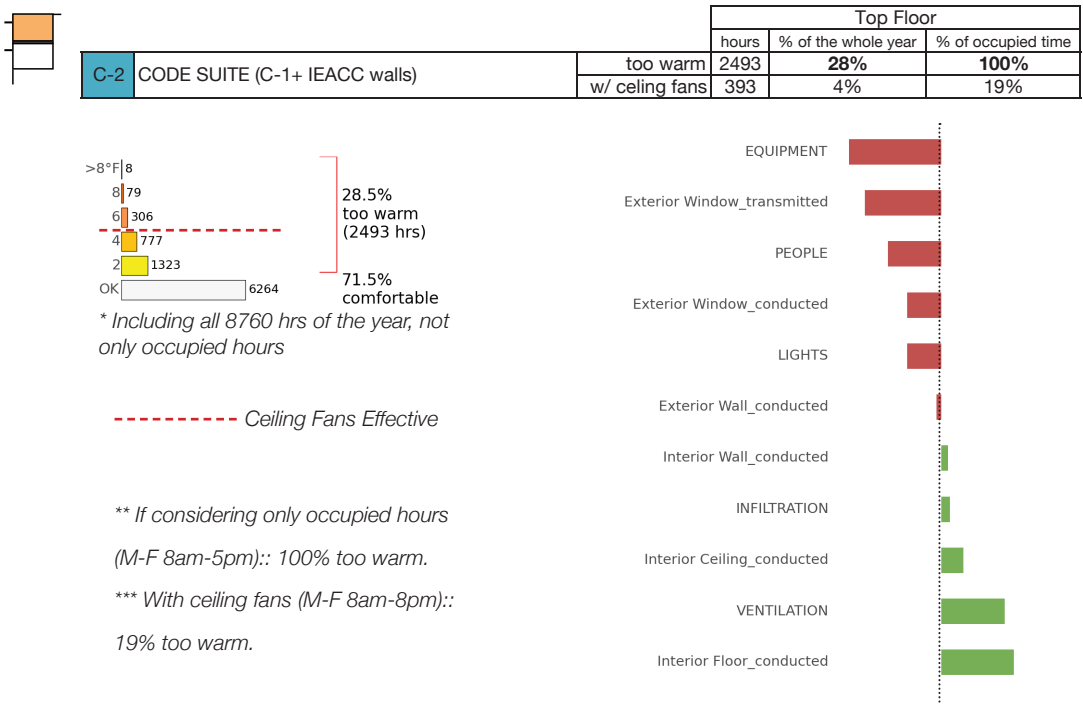
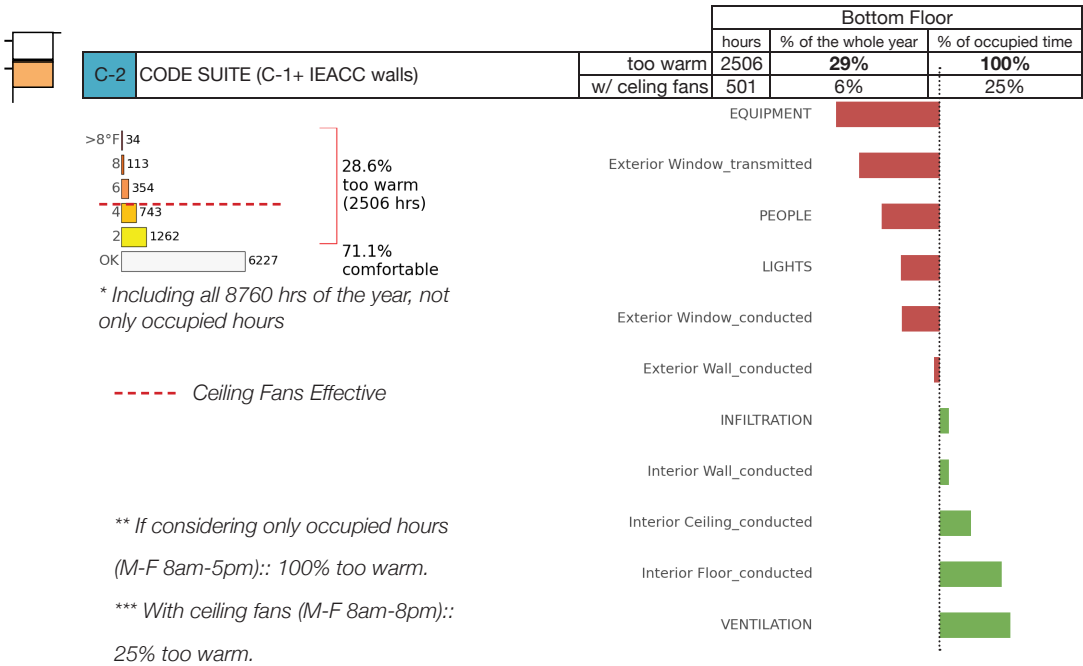
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.a.4 Office Analysis:: South Facing (Continued)



Add/C.4.a. OFFICE ANALYSIS:: SOUTH FACING

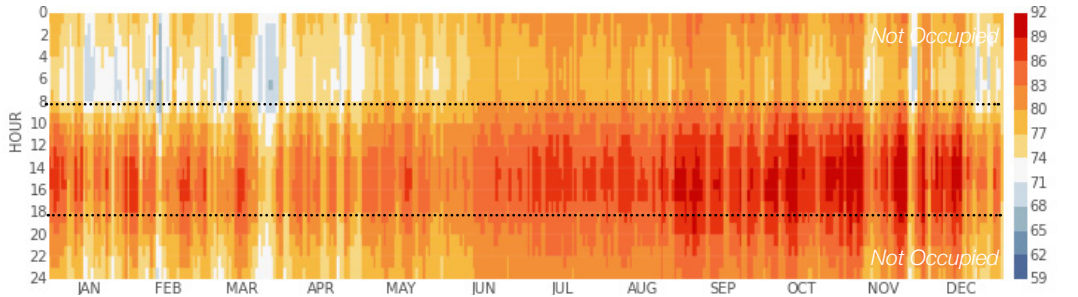
C.4.a.5. IMPROVED SUITE WITH VENTILATION



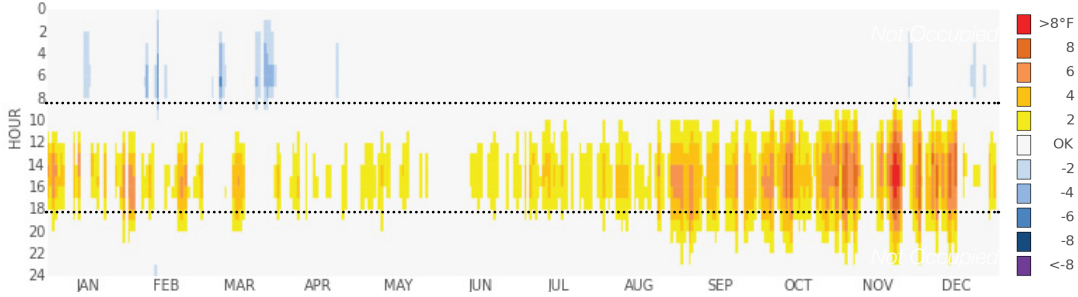
Equal to IMPROVED SUITE +2ACH



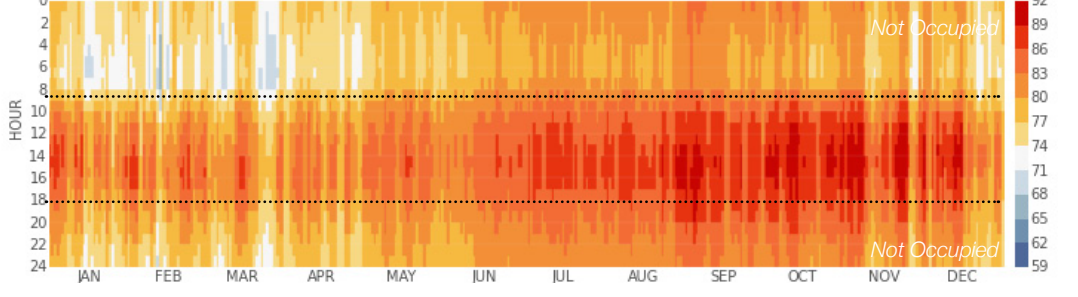
Operative temperature for bottom floor



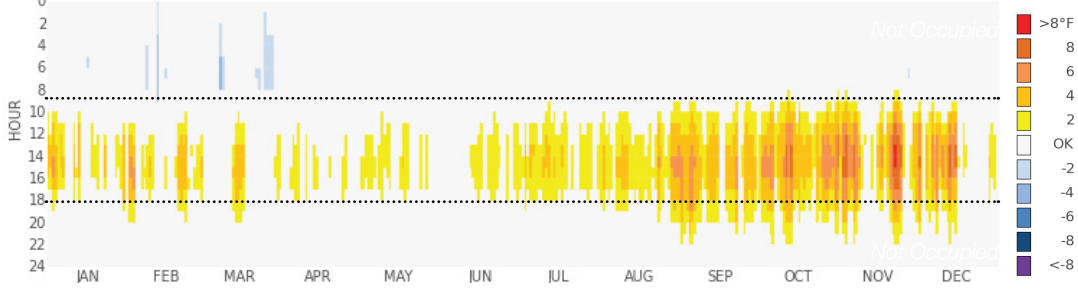
Degrees from comfort for bottom floor



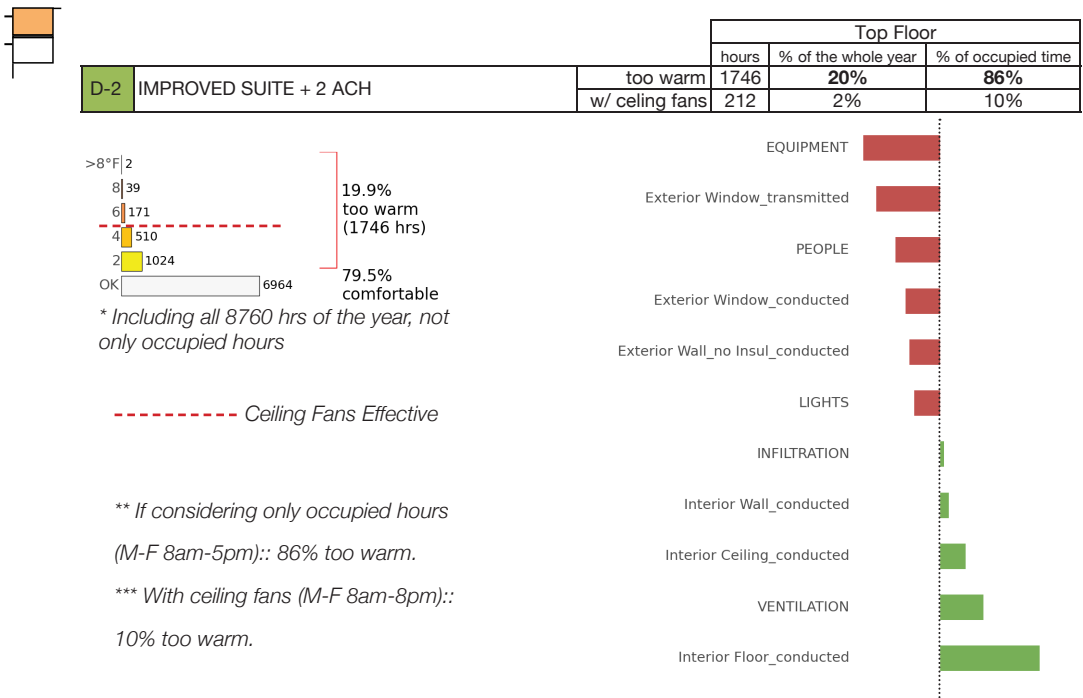
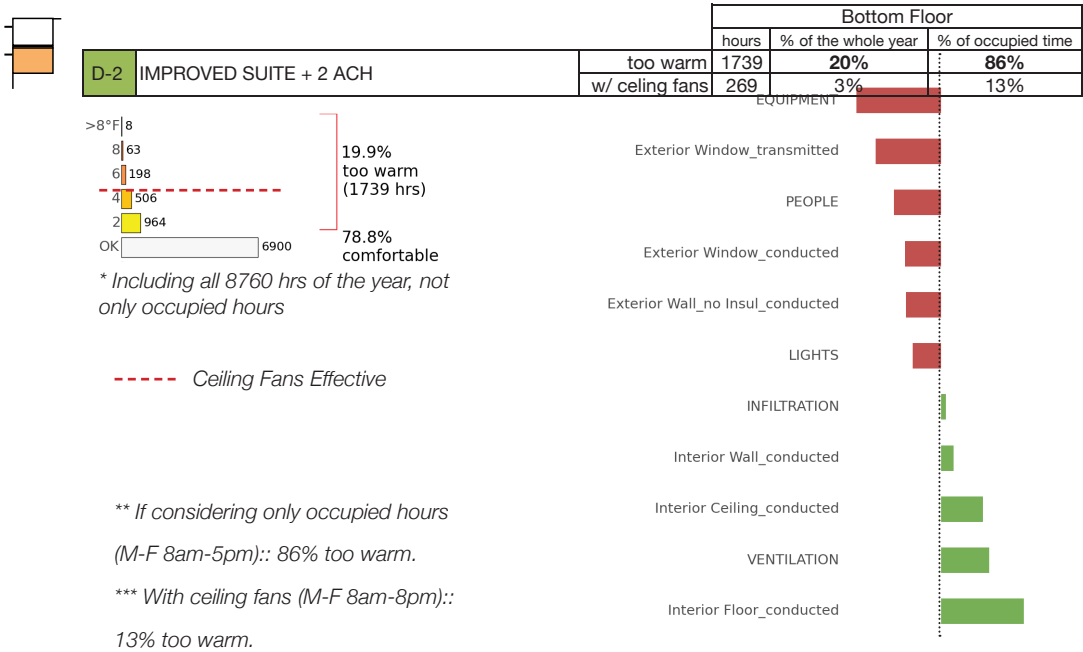
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.a.5 Office Analysis:: South Facing (Continued)



Add/C.4.a. OFFICE ANALYSIS:: SOUTH FACING

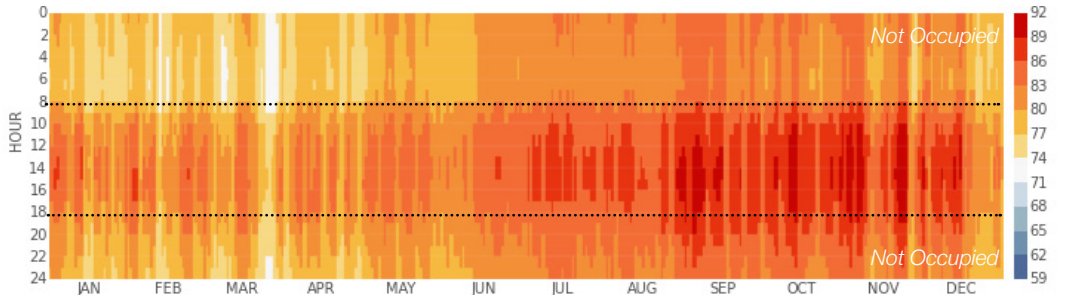
C.4.a.6. IDEAL SUITE



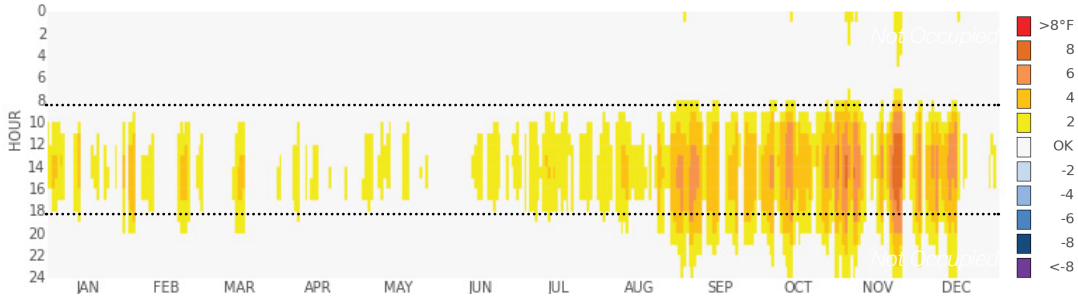
Equal to CODE SUITE + Thermal Mass



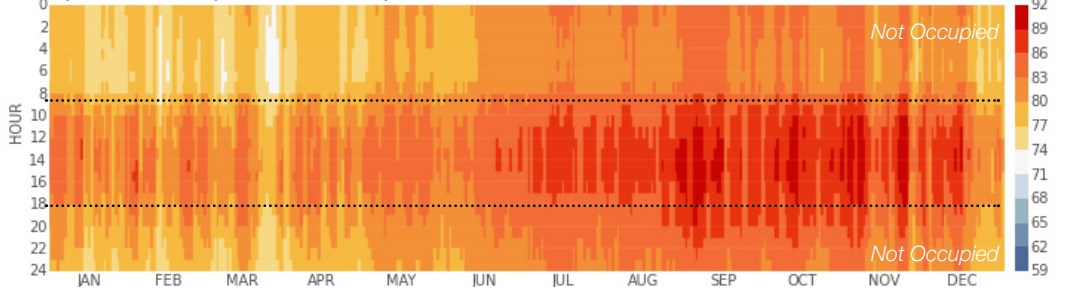
Operative temperature for bottom floor



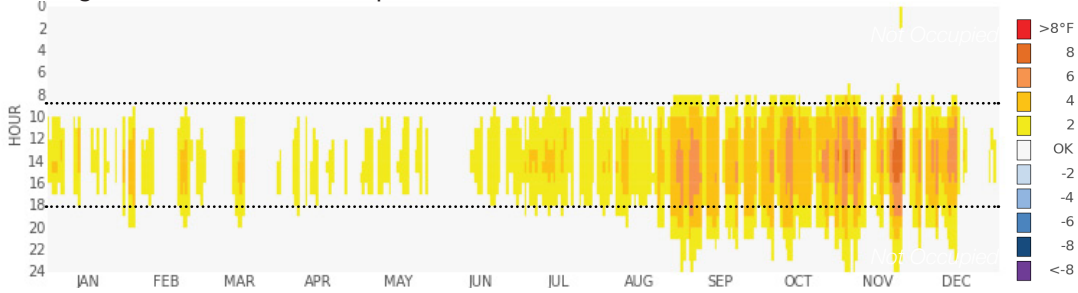
Degrees from comfort for bottom floor



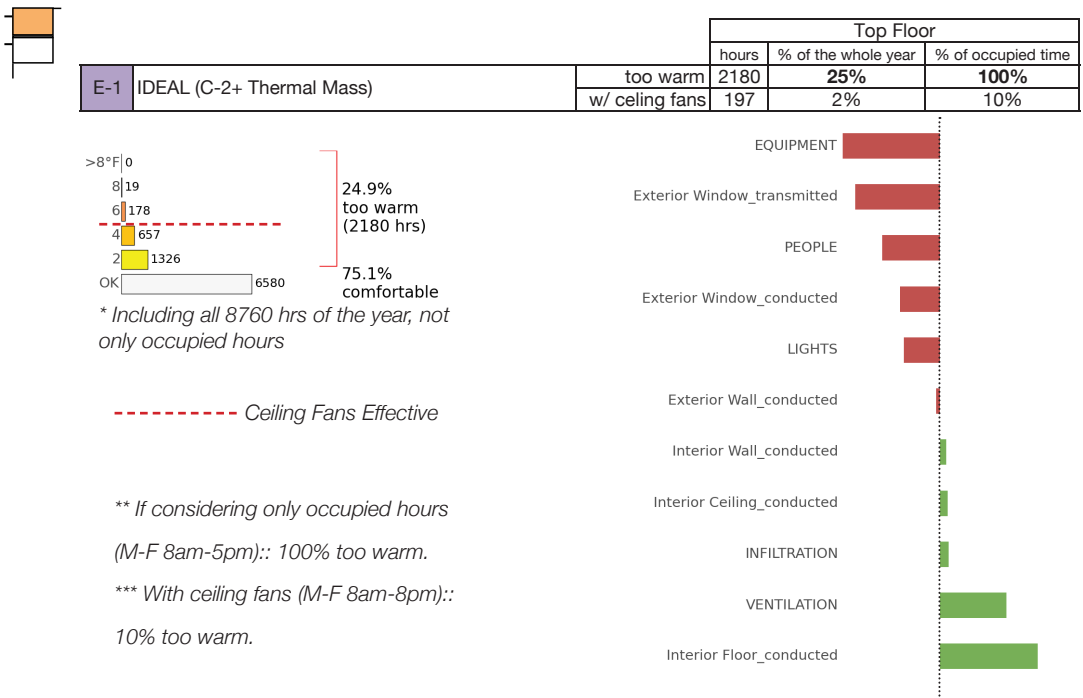
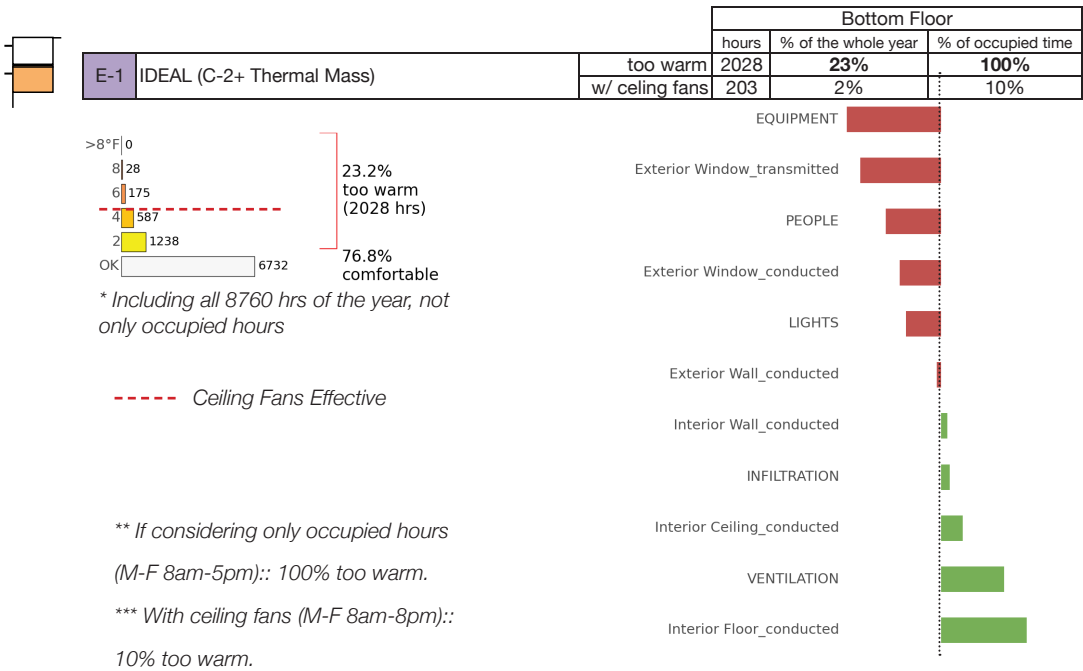
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.a.6 Office Analysis:: South Facing (Continued)



Add/C.4.a. OFFICE ANALYSIS:: SOUTH FACING

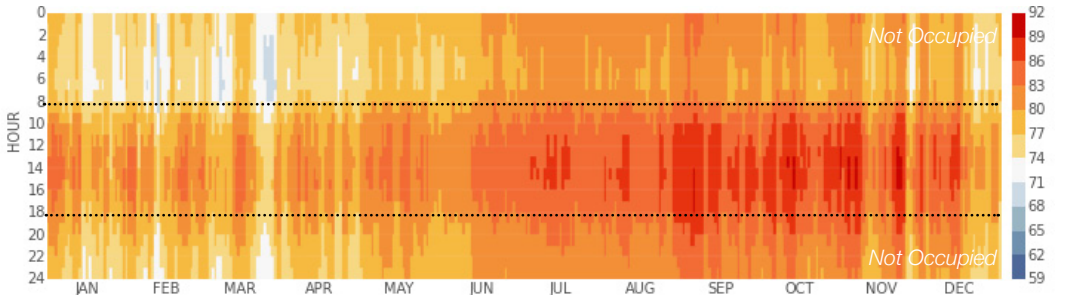
C.4.a.7. IDEAL SUITE WITH VENTILATION



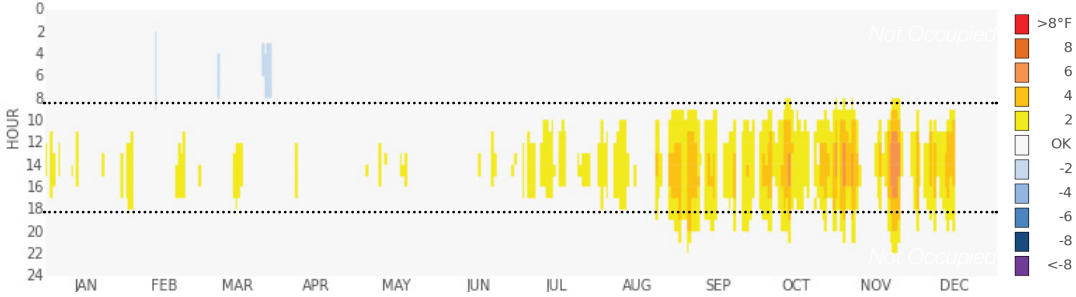
Equal to IDEAL SUITE + 2ACH



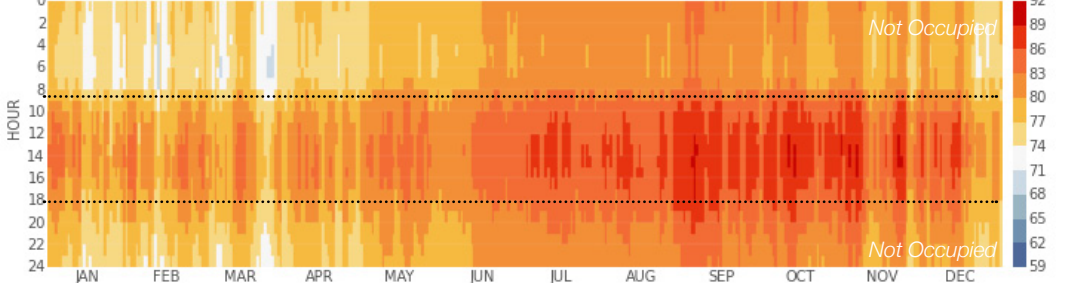
Operative temperature for bottom floor



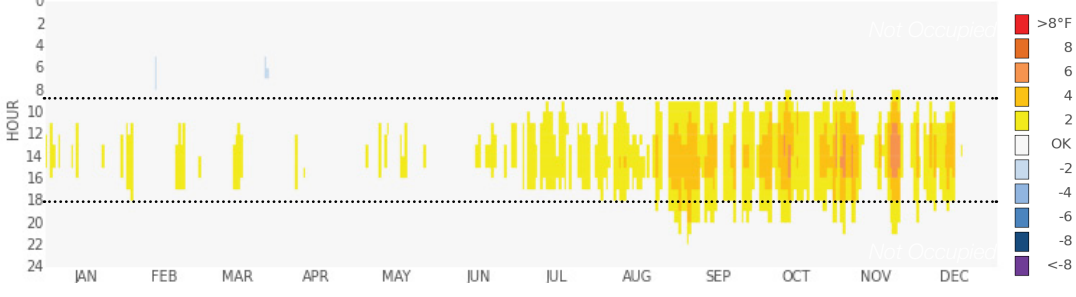
Degrees from comfort for bottom floor



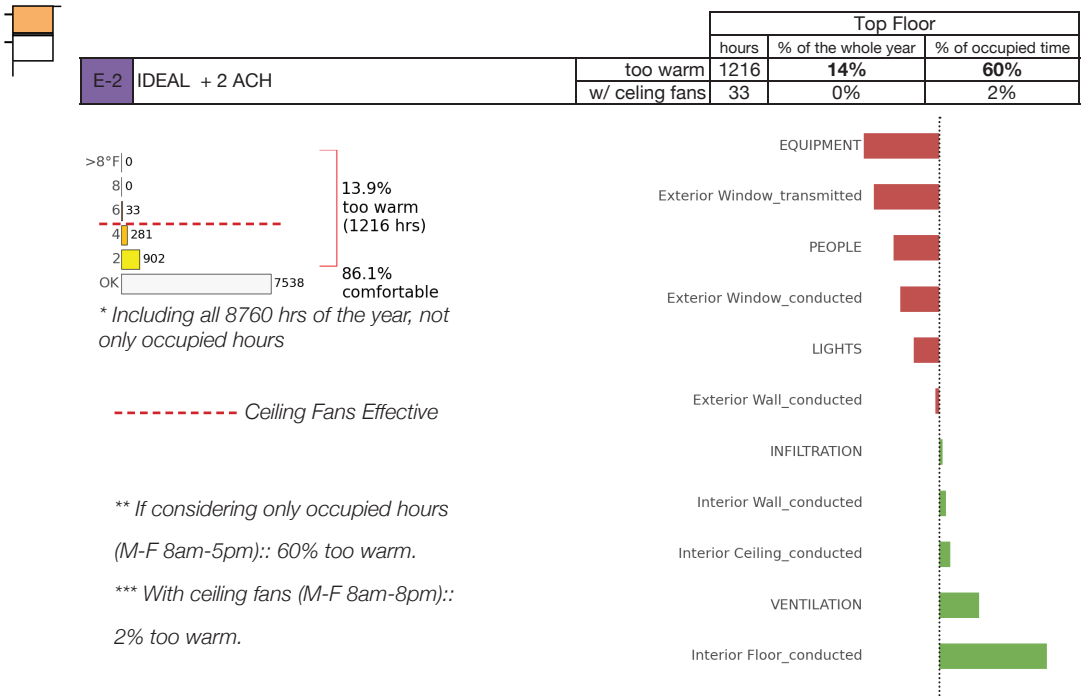
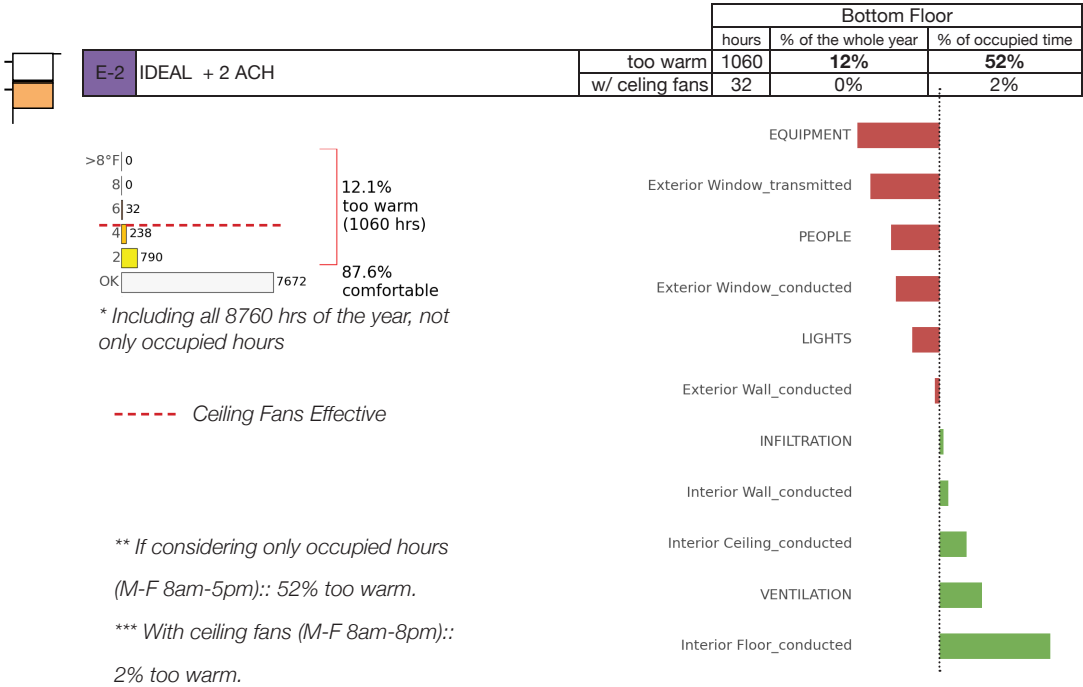
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.a.7 Office Analysis:: South Facing (Continued)



Add/C.4.b. OFFICE ANALYSIS:: NORTH FACING

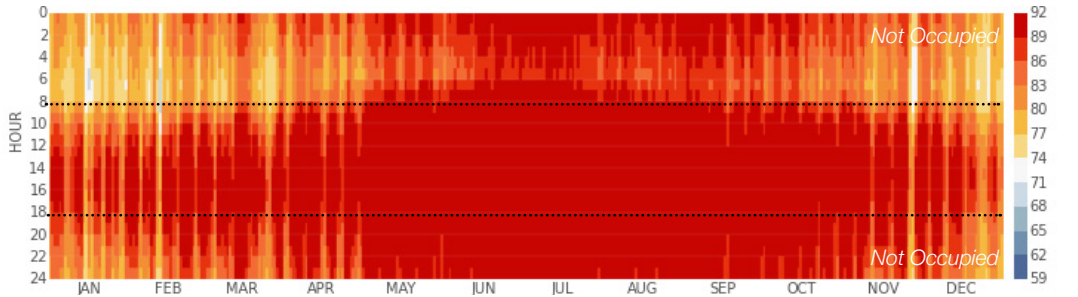


C.4.b.0. TYPICAL EXISTING

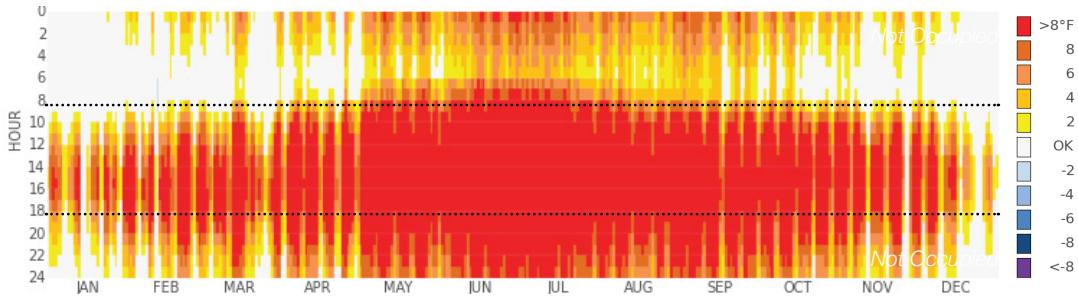
No Insulation in Opaque Surfaces and Single Pane Glass



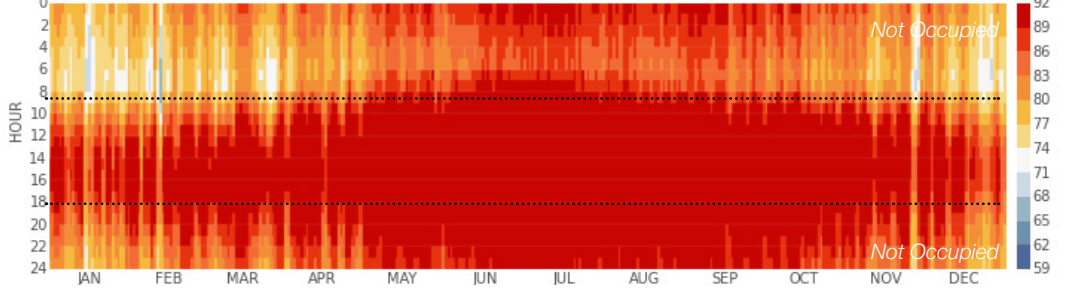
Operative temperature for bottom floor



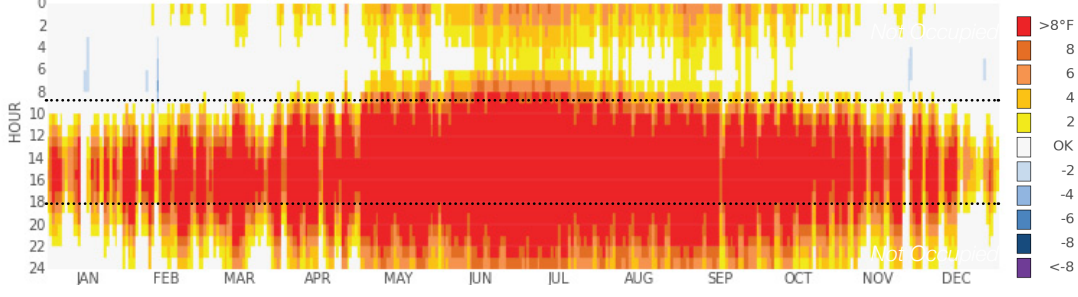
Degrees from comfort for bottom floor



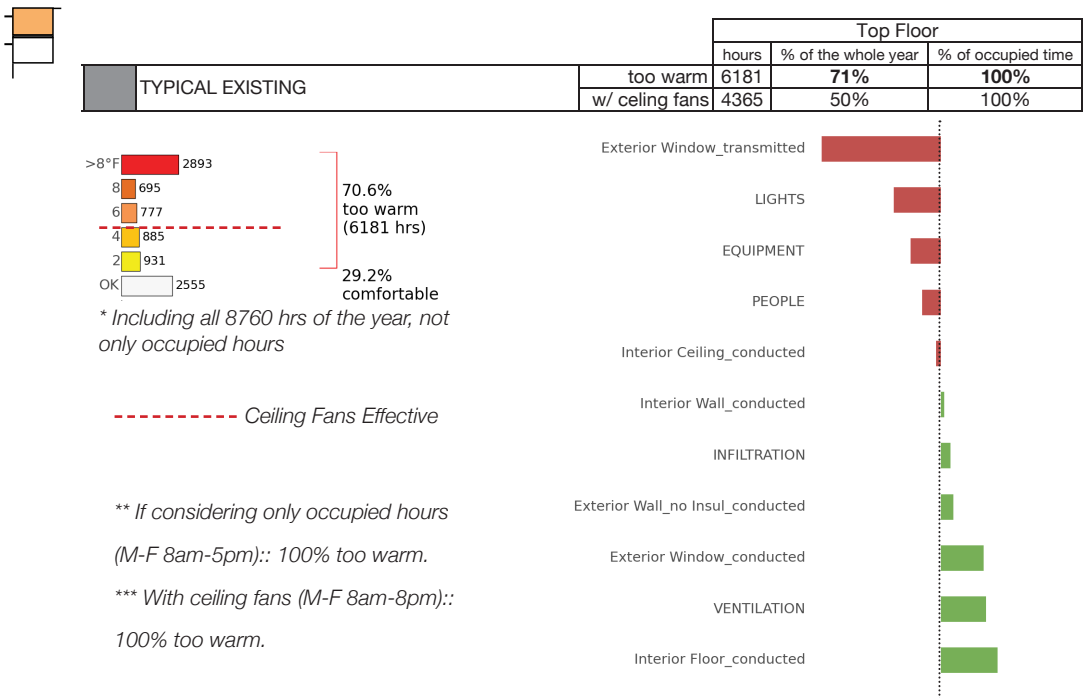
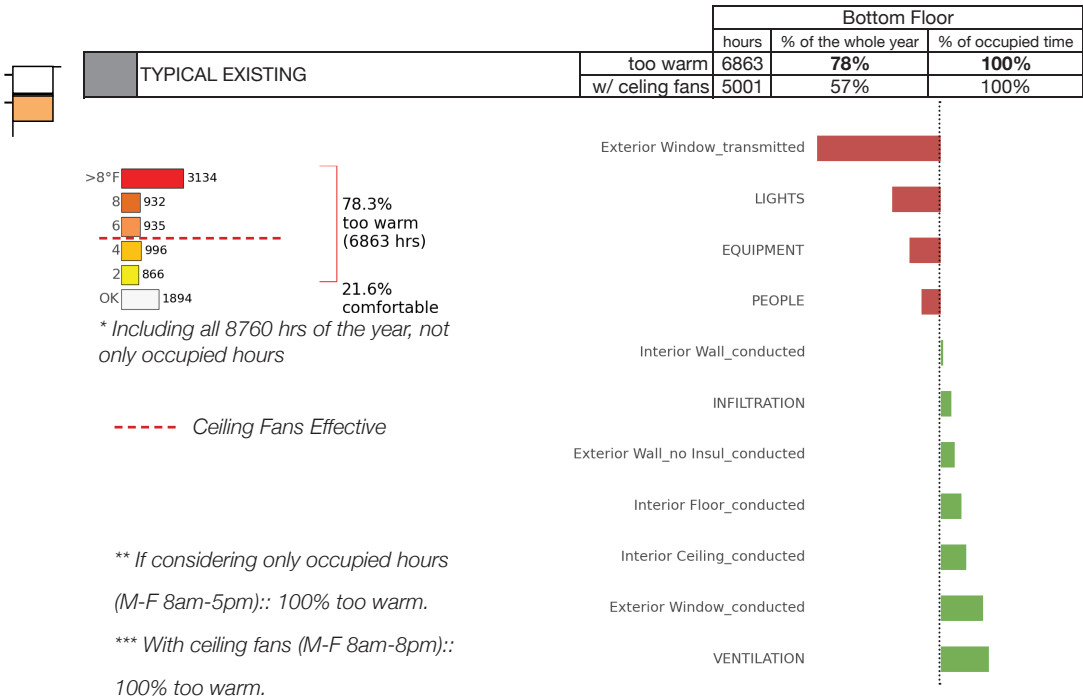
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.b.0 Office Analysis:: North Facing (Continued)



Add/C.4.b. OFFICE ANALYSIS:: NORTH FACING

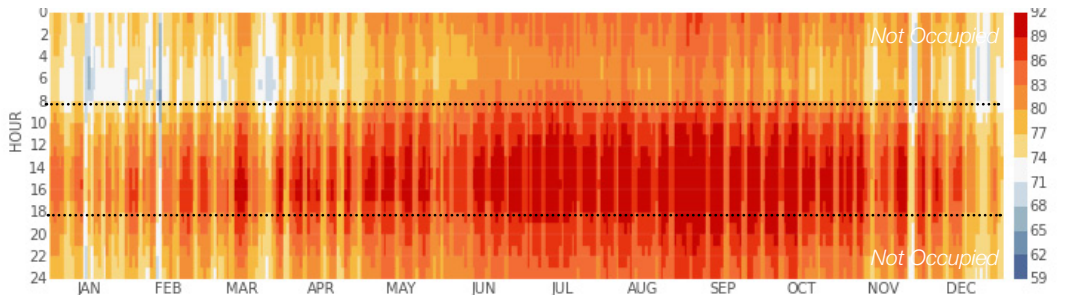


C.4.b.1. TYPICAL WITH WINDOW IMPROVEMENTS

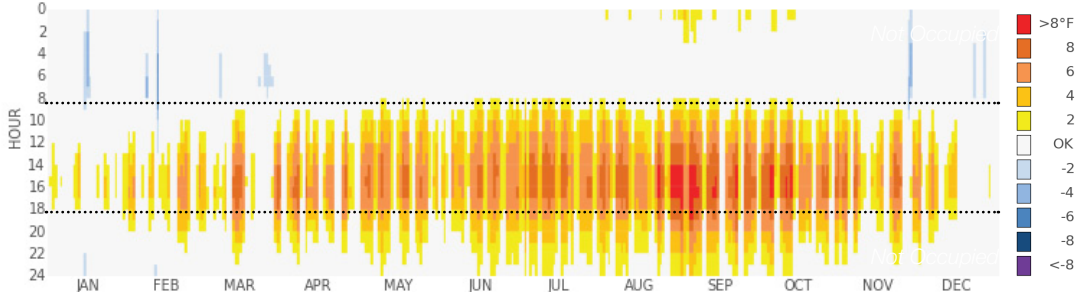
Equal to TYPICAL + 1ACH + Shading + IECC 2015 Windows



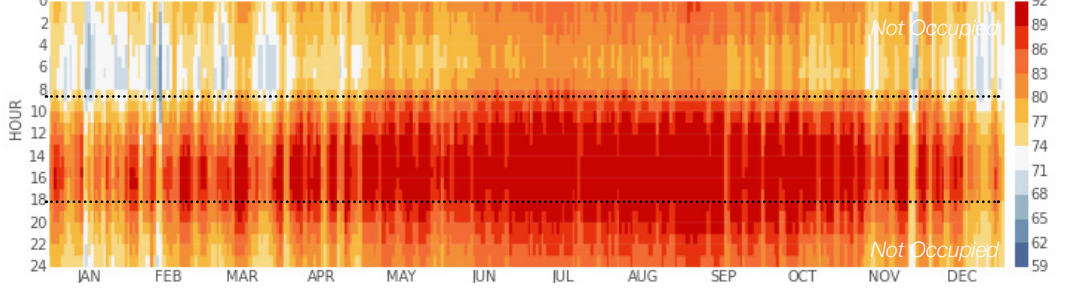
Operative temperature for bottom floor



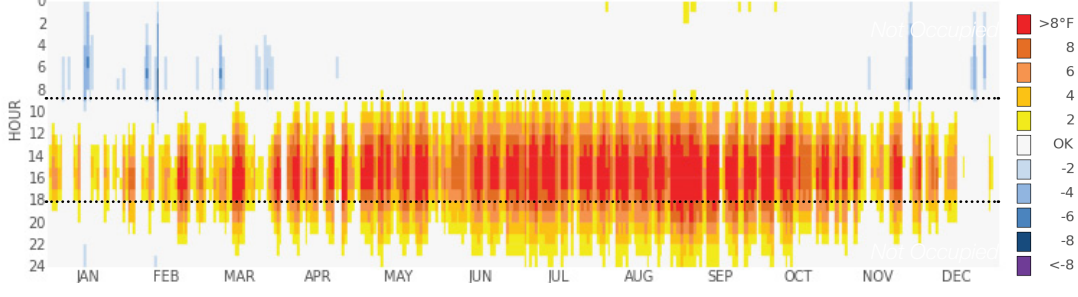
Degrees from comfort for bottom floor



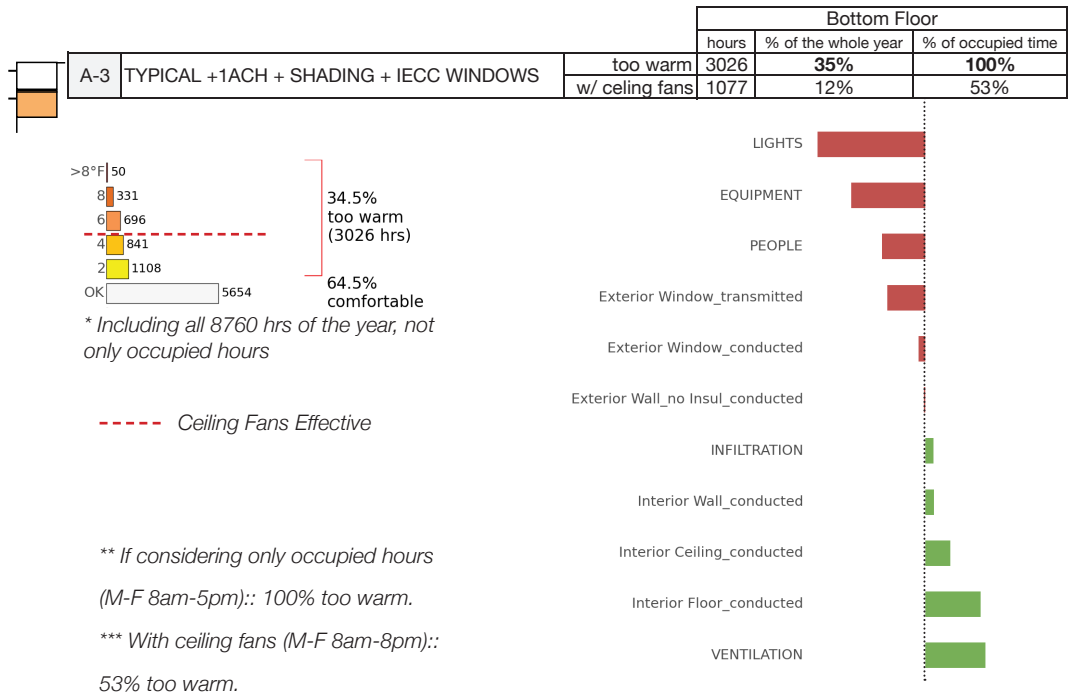
Operative temperature for top floor



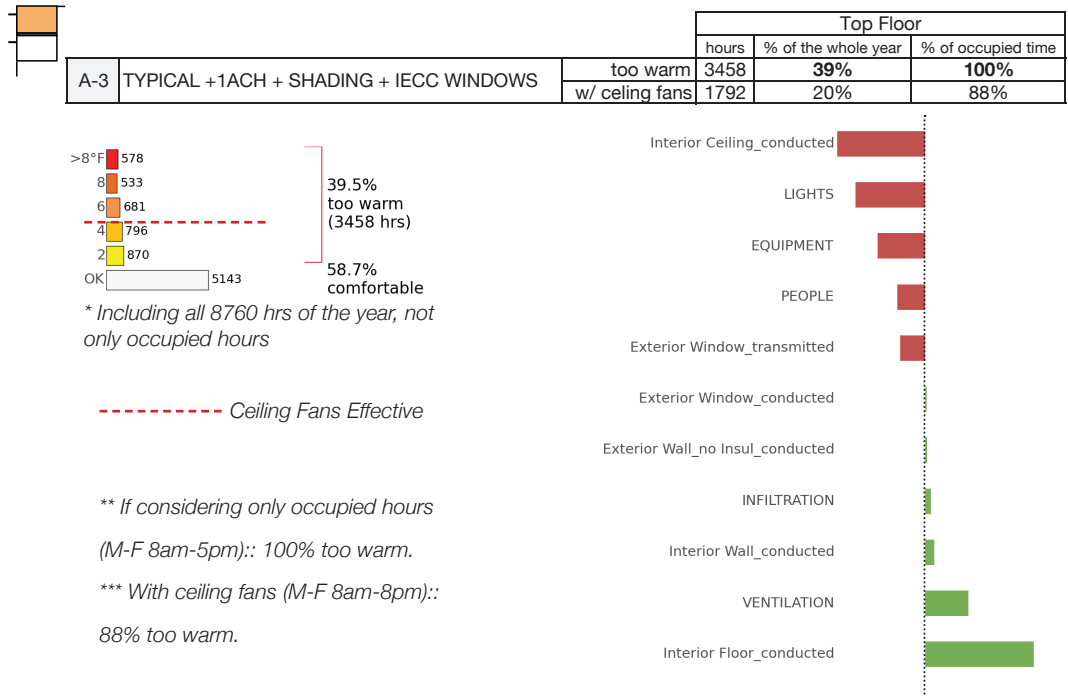
Degrees from comfort for top floor



Add/C.4.b.1 Office Analysis:: North Facing (Continued)



A-3 TYPICAL +1ACH +



Add/C.4.b. OFFICE ANALYSIS:: NORTH FACING

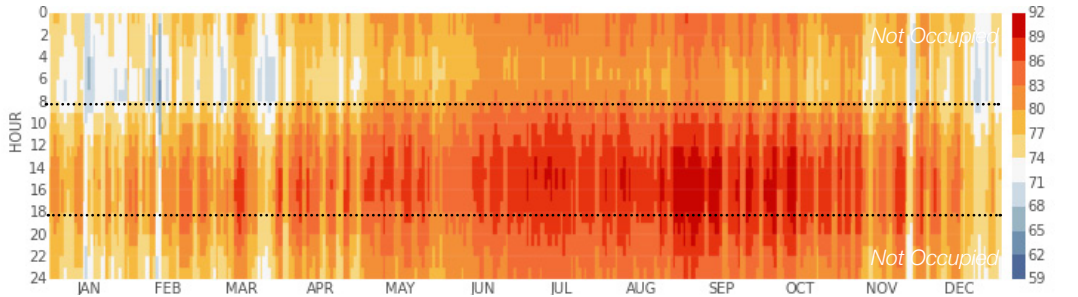


C.4.b.2. MINIMUM SUITE

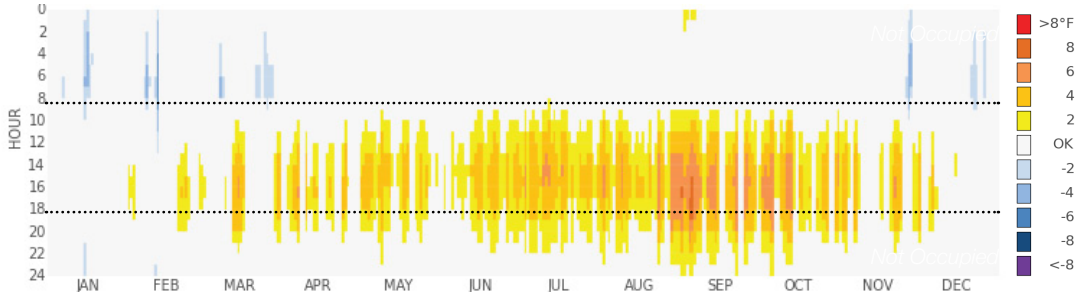
Equal to TYPICAL + IECC Windows + Shading +lower LPD + Daylight Controls +1ACH



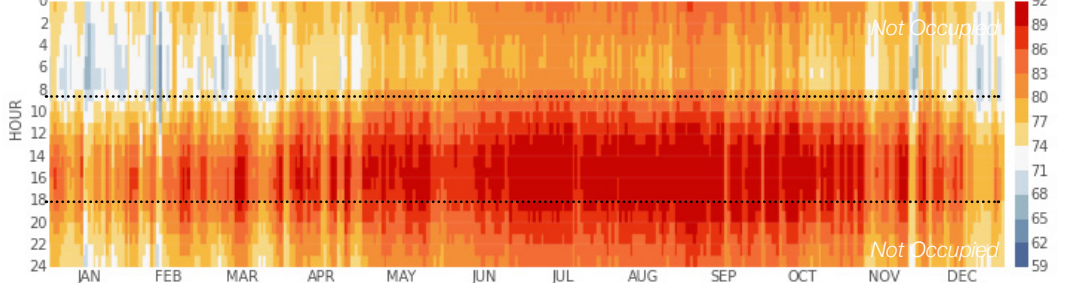
Operative temperature for bottom floor



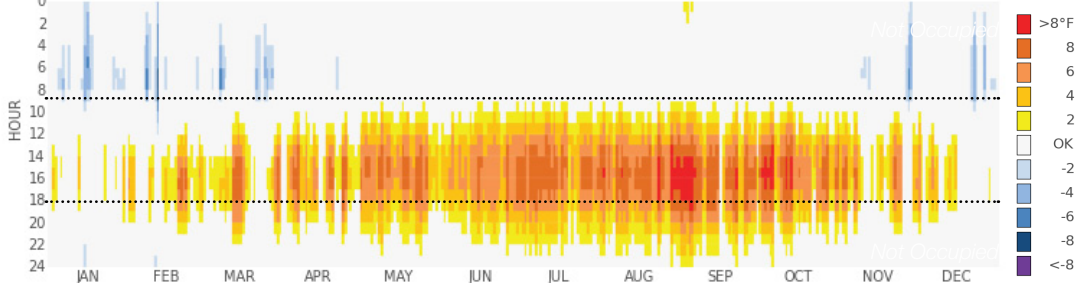
Degrees from comfort for bottom floor



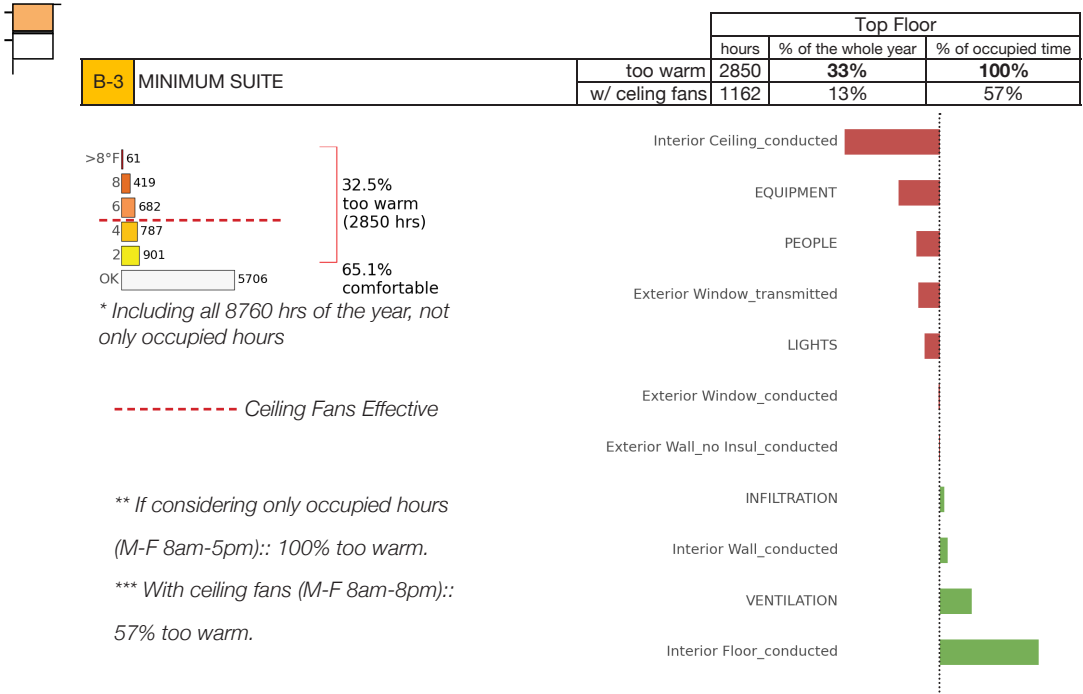
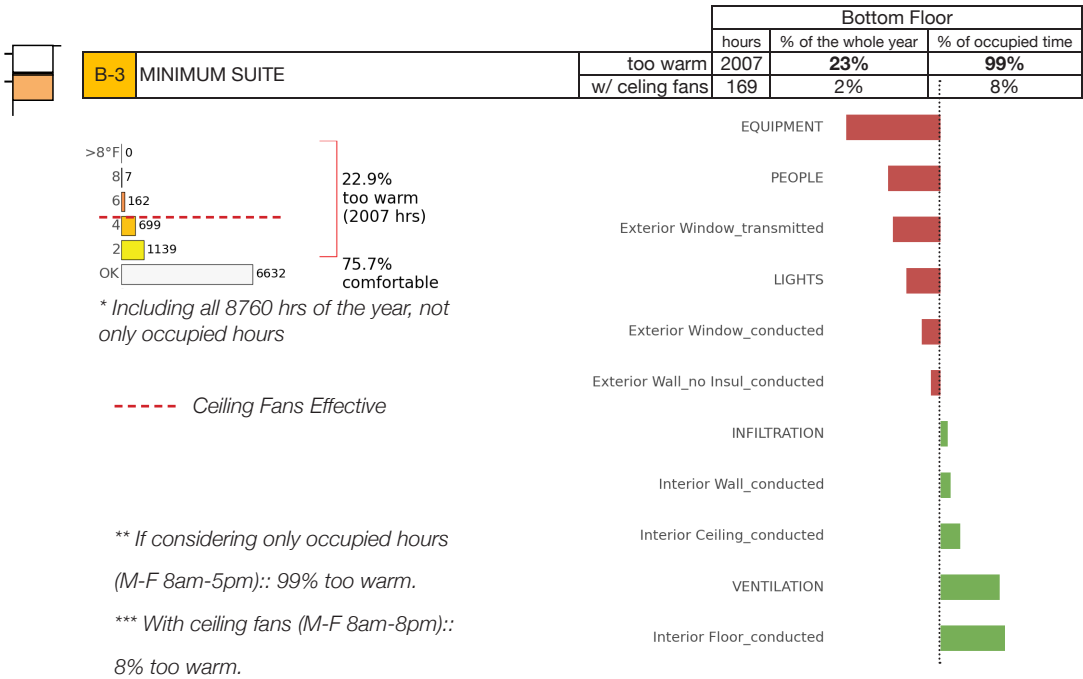
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.b.2 Office Analysis:: North Facing (Continued)



Add/C.4.b. OFFICE ANALYSIS:: NORTH FACING

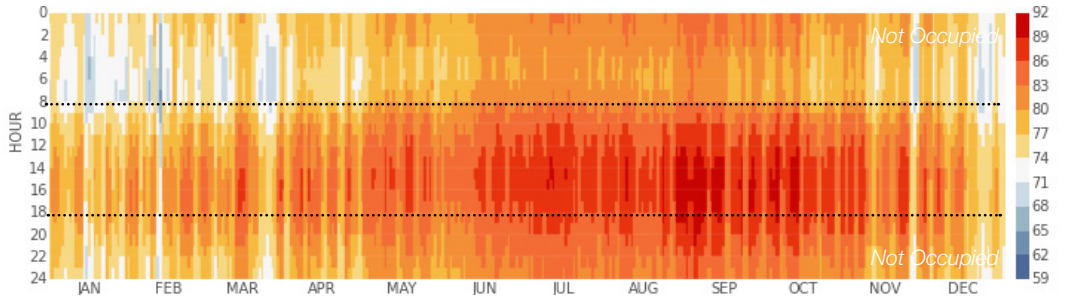


C.4.b.3. IMPROVED SUITE

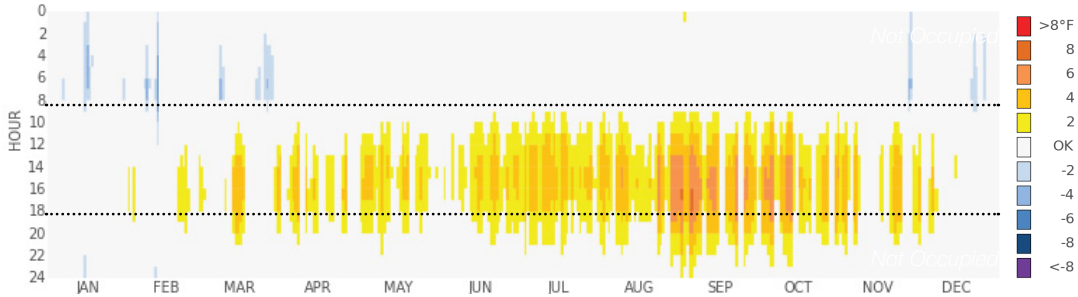
Equal to MINIMUM SUITE + IECC Roof



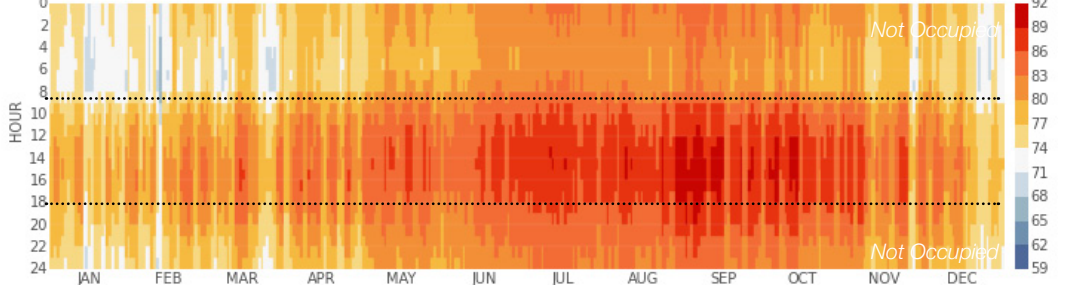
Operative temperature for bottom floor



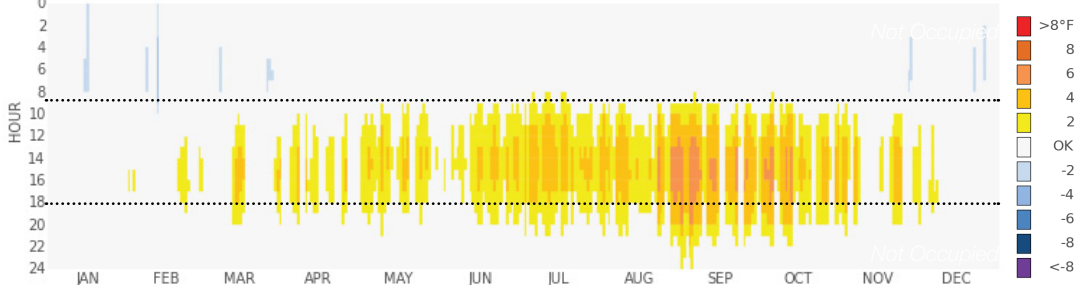
Degrees from comfort for bottom floor



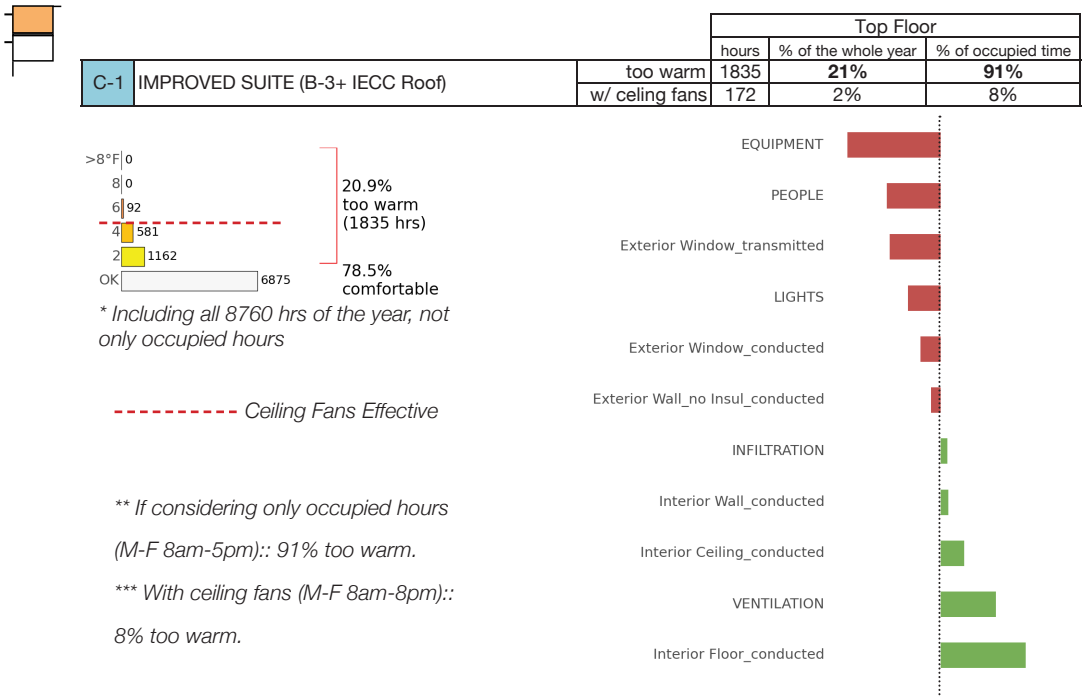
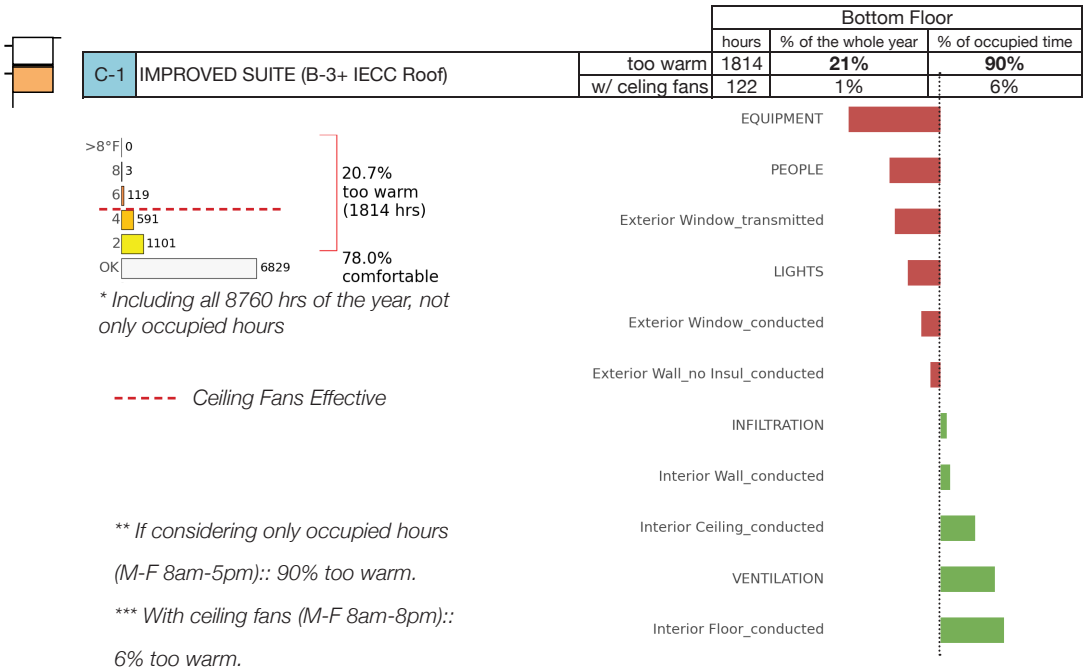
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.b.3 Office Analysis:: North Facing (Continued)



Add/C.4.b. OFFICE ANALYSIS:: NORTH FACING

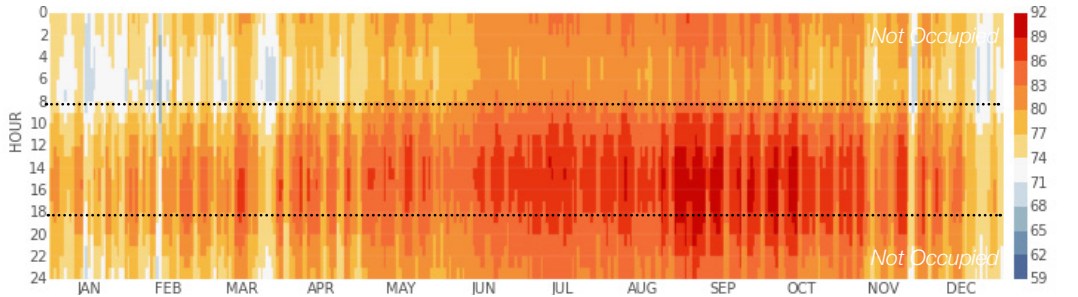


C.4.b.4. CODE SUITE

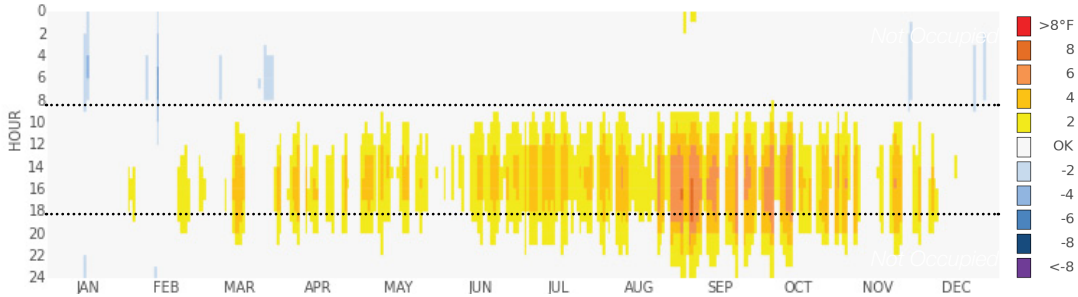
Equal to IMPROVED SUITE + IECC Walls



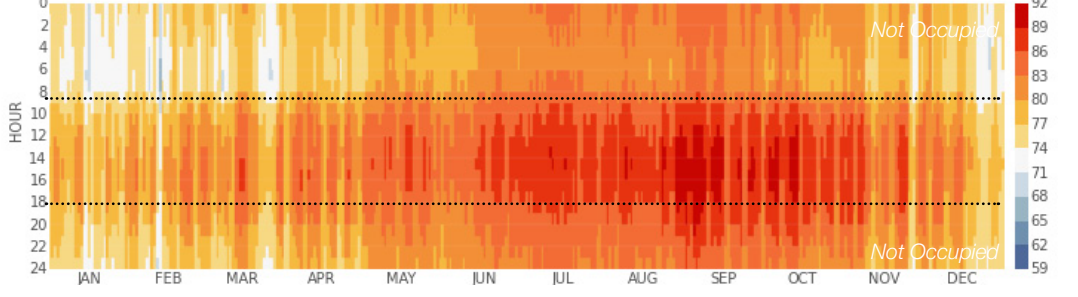
Operative temperature for bottom floor



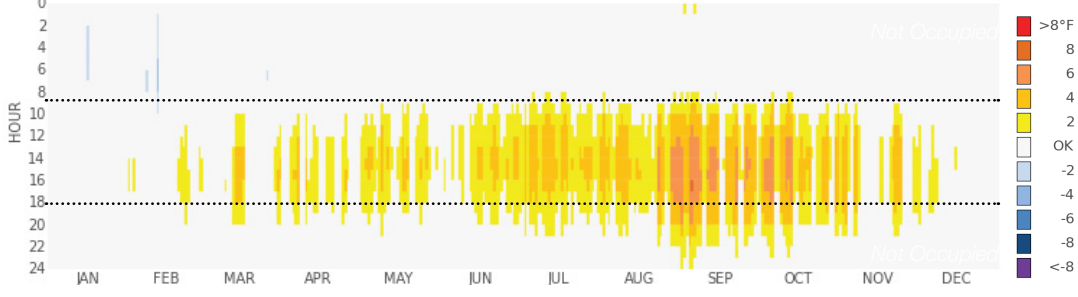
Degrees from comfort for bottom floor



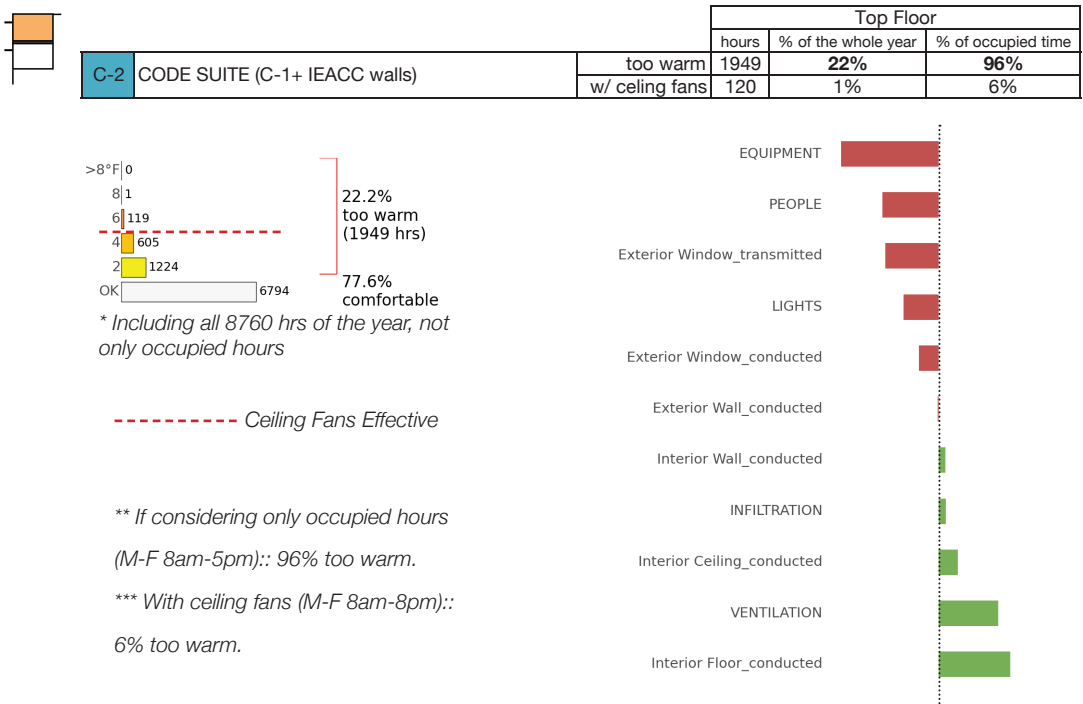
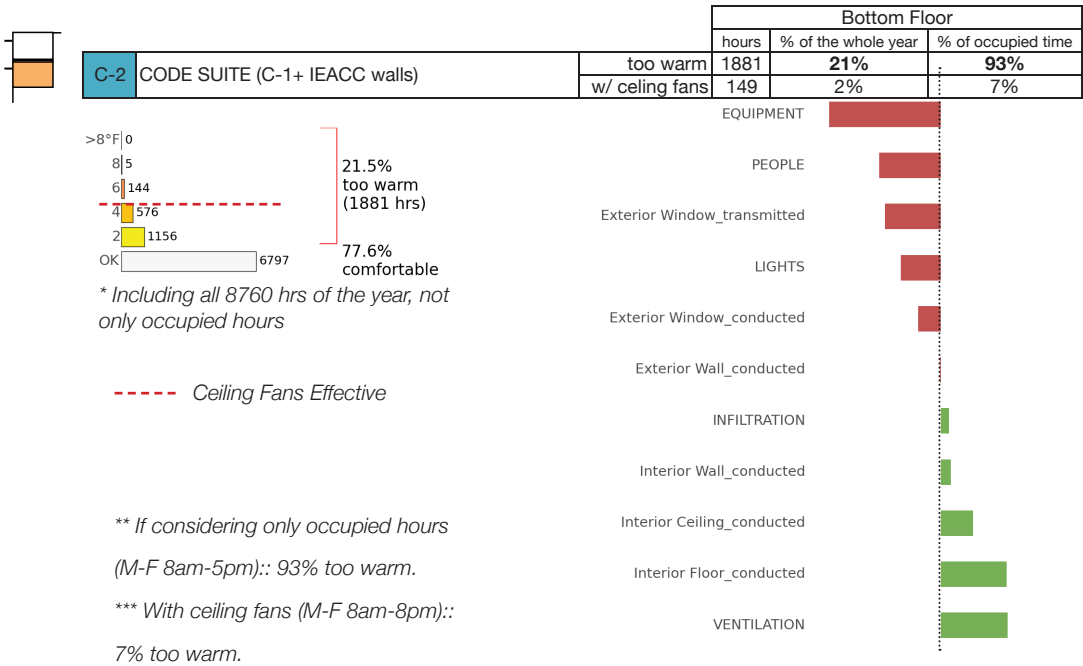
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.b.4 Office Analysis:: North Facing (Continued)



Add/C.4.b. OFFICE ANALYSIS:: NORTH FACING

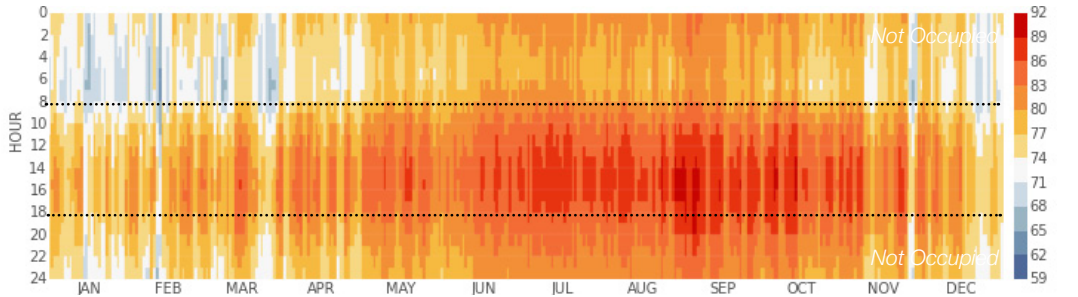


C.4.b.5. IMPROVED SUITE WITH VENTILATION

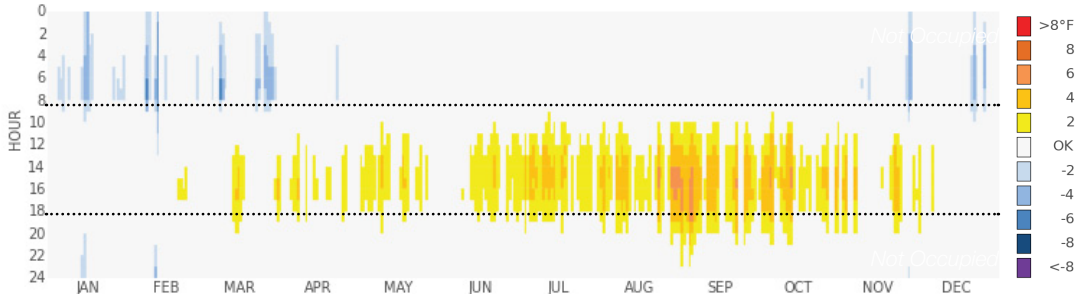
Equal to IMPROVED SUITE +2ACH



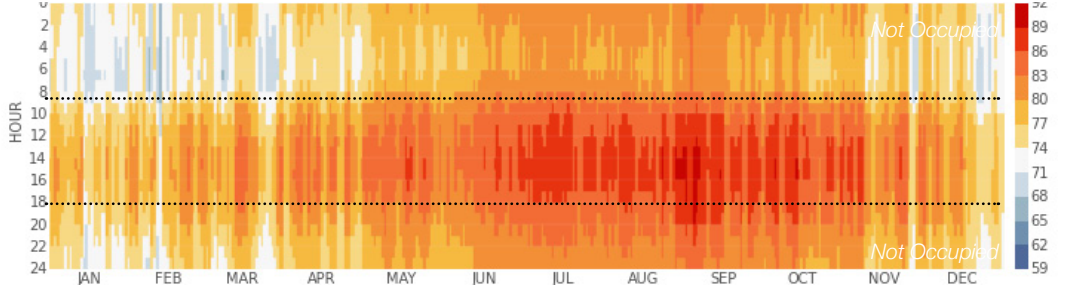
Operative temperature for bottom floor



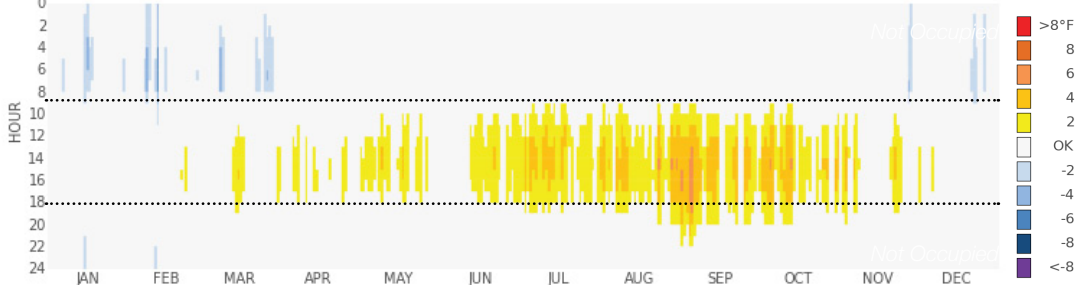
Degrees from comfort for bottom floor



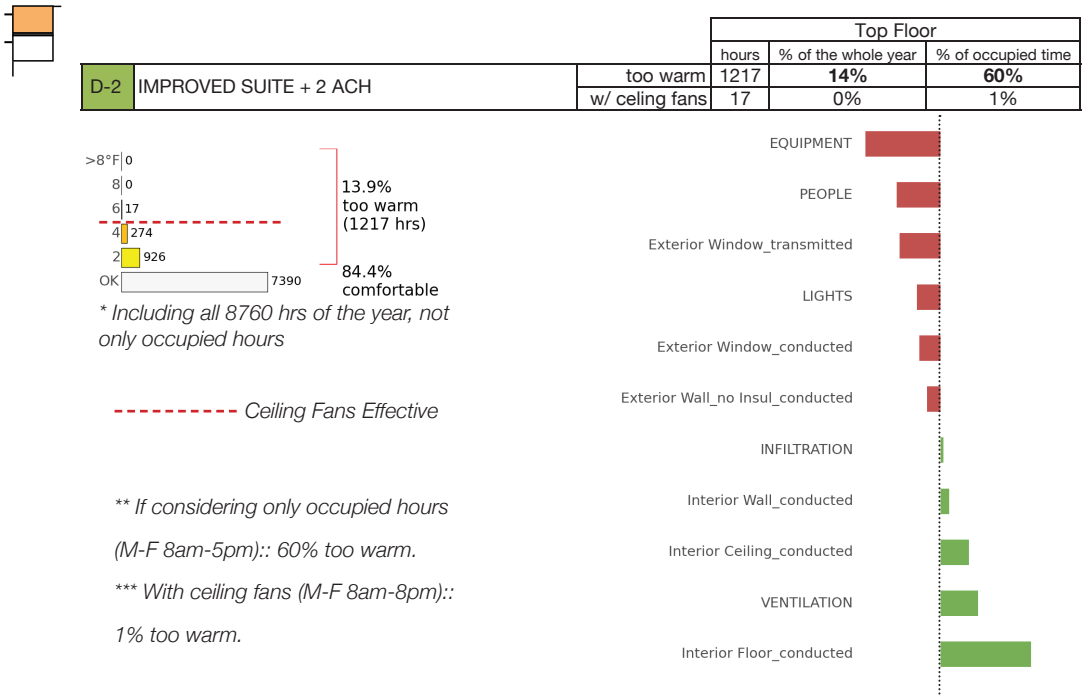
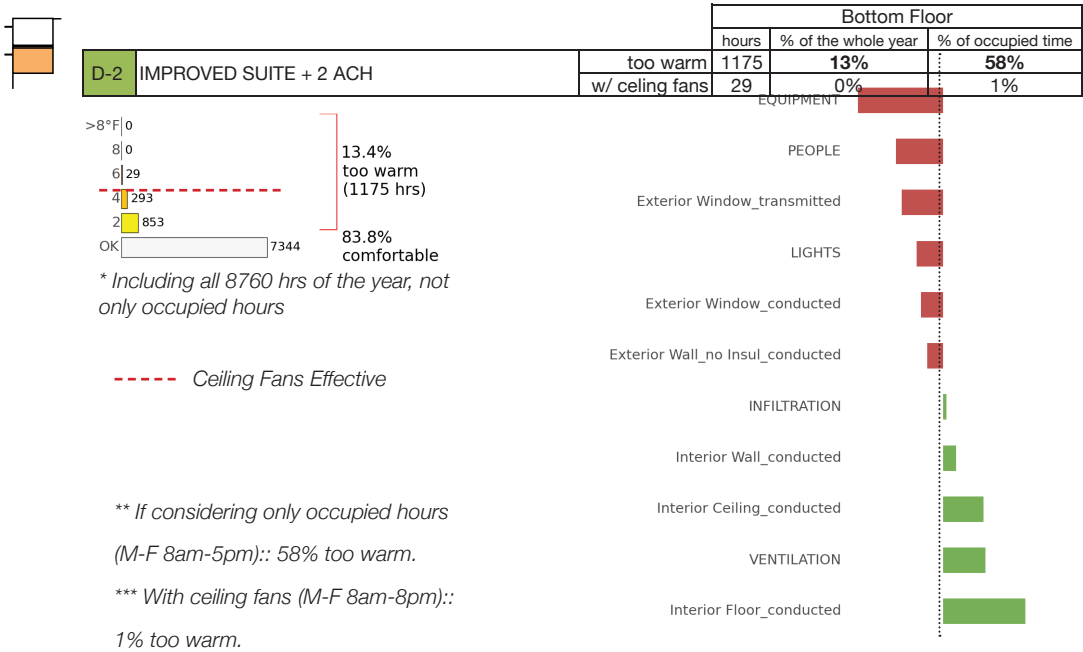
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.b.5 Office Analysis:: North Facing (Continued)



Add/C.4.b. OFFICE ANALYSIS:: NORTH FACING

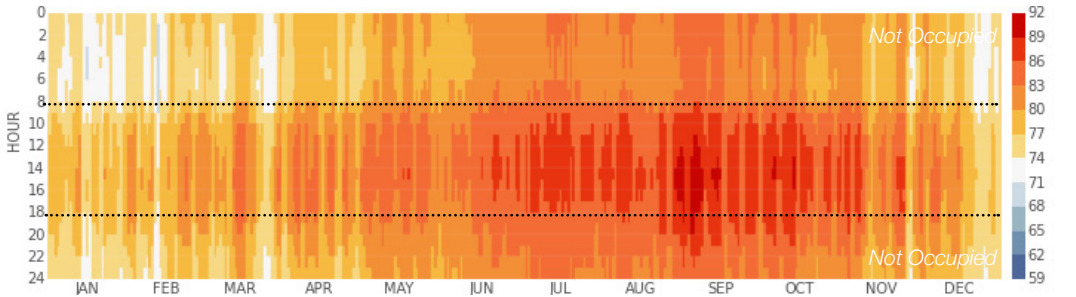


C.4.b.6. IDEAL SUITE

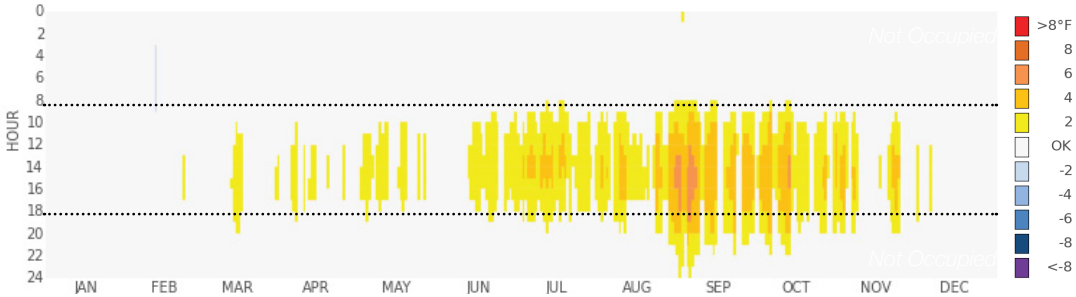
Equal to CODE SUITE + Thermal Mass



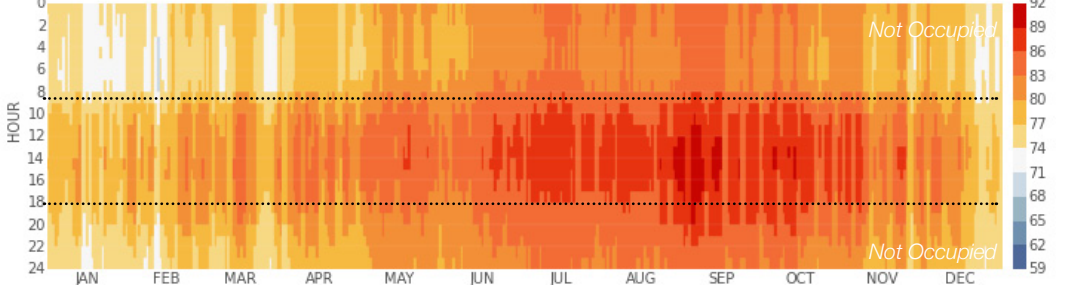
Operative temperature for bottom floor



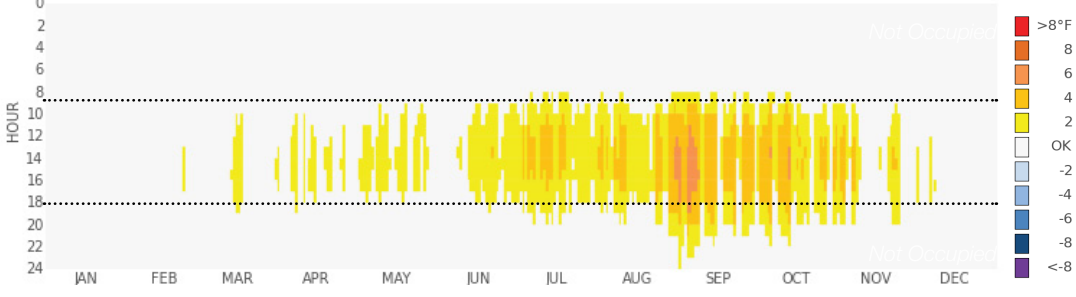
Degrees from comfort for bottom floor



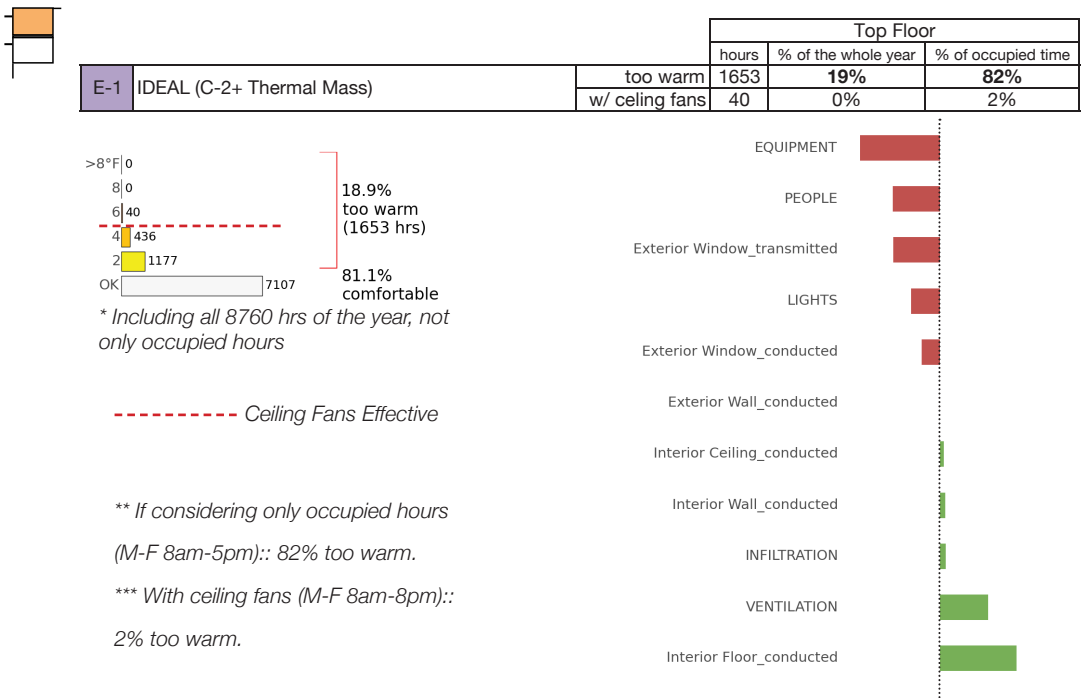
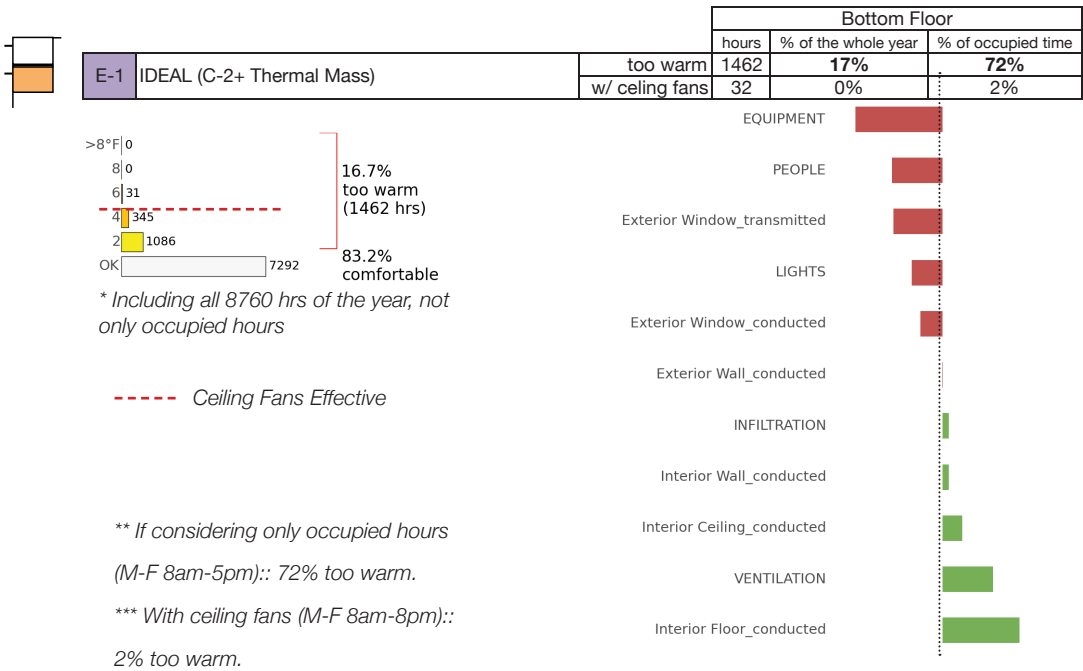
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.b.6 Office Analysis:: North Facing (Continued)



Add/C.4.b. OFFICE ANALYSIS:: NORTH FACING

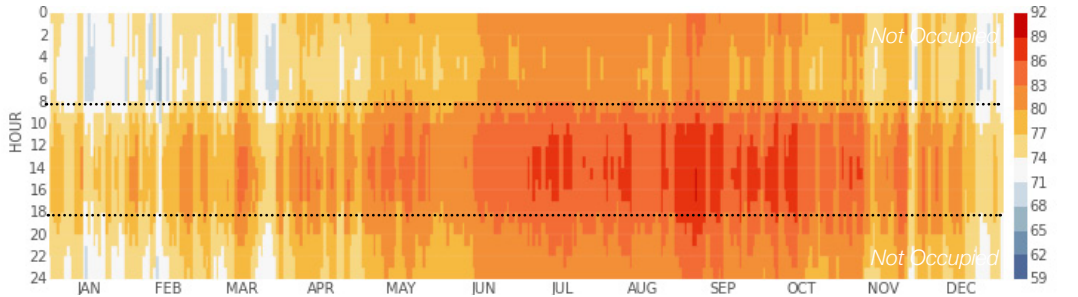


C.4.b.7. IDEAL SUITE WITH VENTILATION

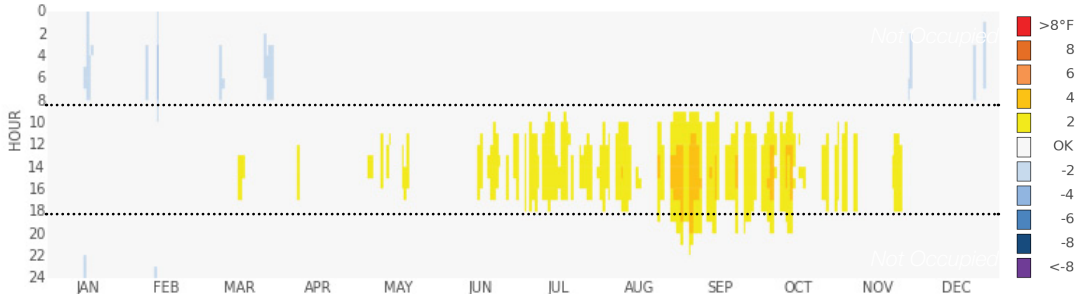
Equal to IDEAL SUITE + 2ACH



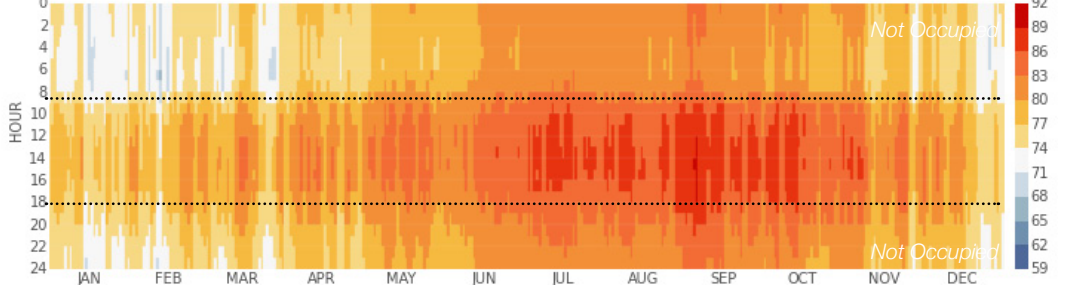
Operative temperature for bottom floor



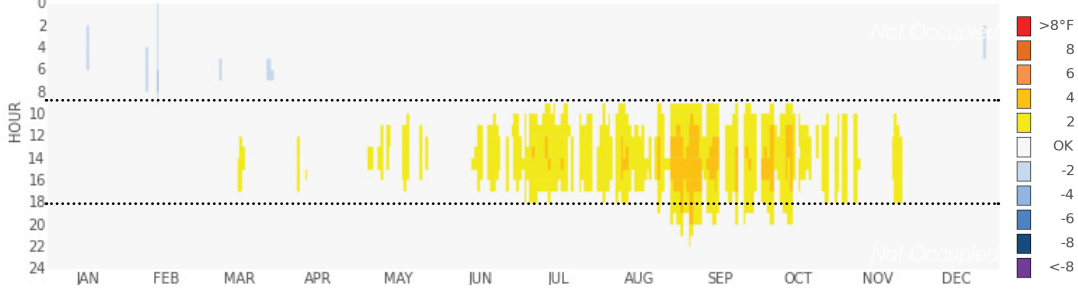
Degrees from comfort for bottom floor



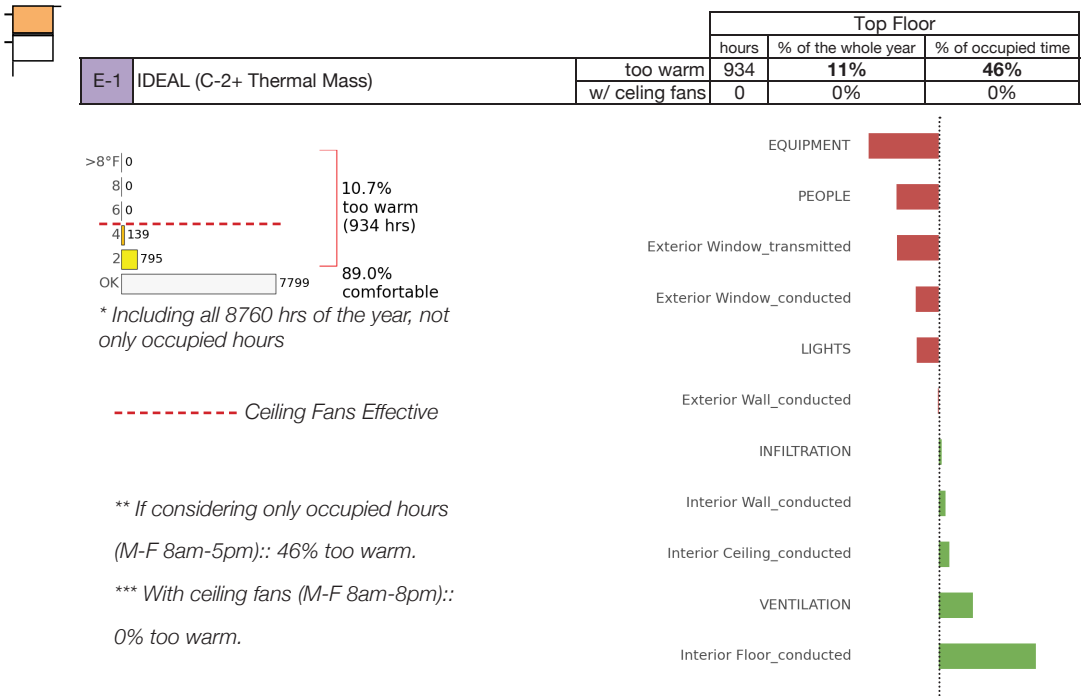
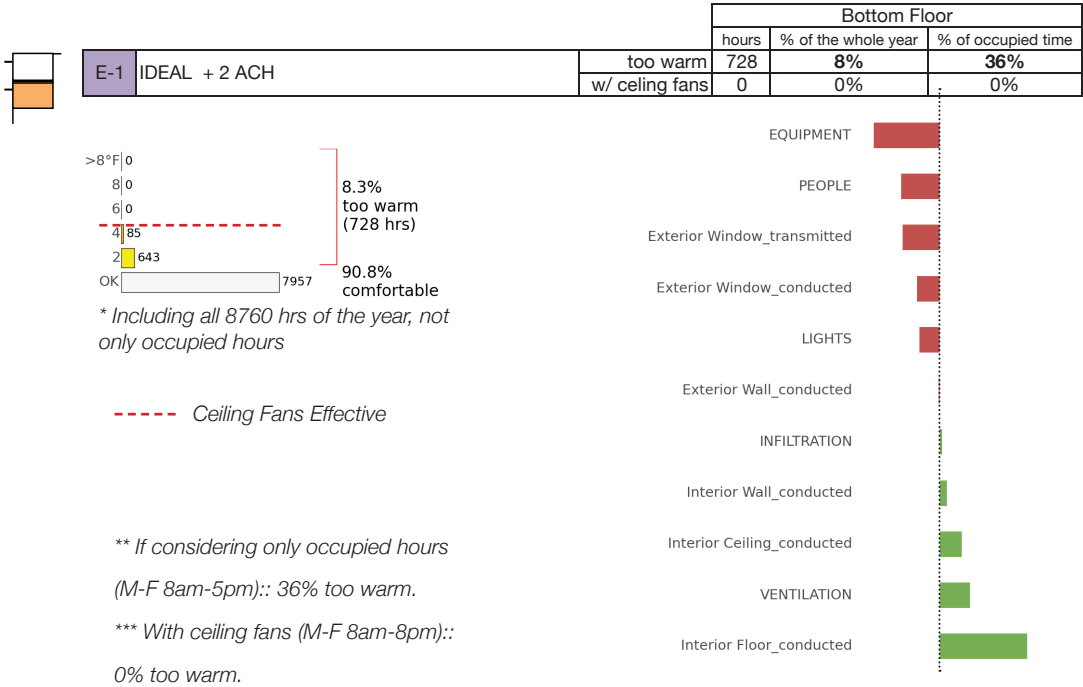
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.b.7 Office Analysis:: North Facing (Continued)



Add/C.4.c. OFFICE ANALYSIS:: EAST FACING



C.4.c.0. TYPICAL EXISTING

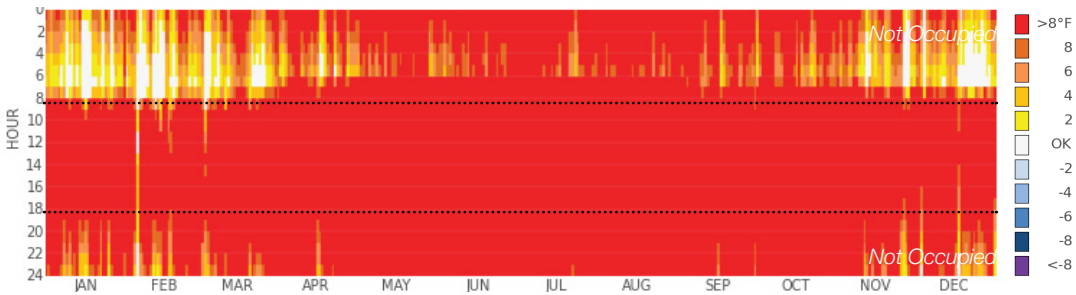
No Insulation in Opaque Surfaces and Single Pane Glass



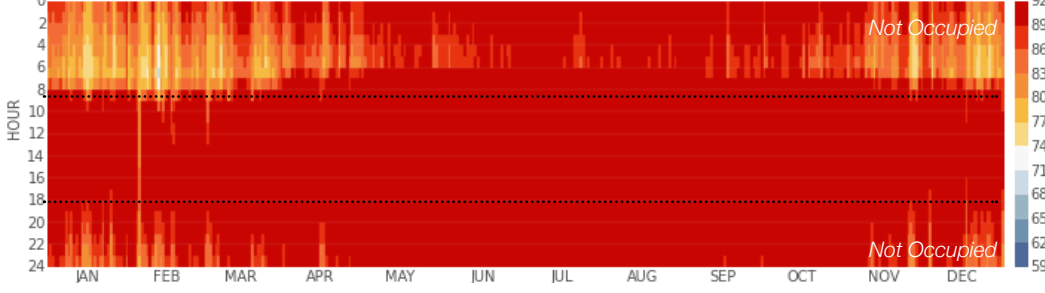
Operative temperature for bottom floor



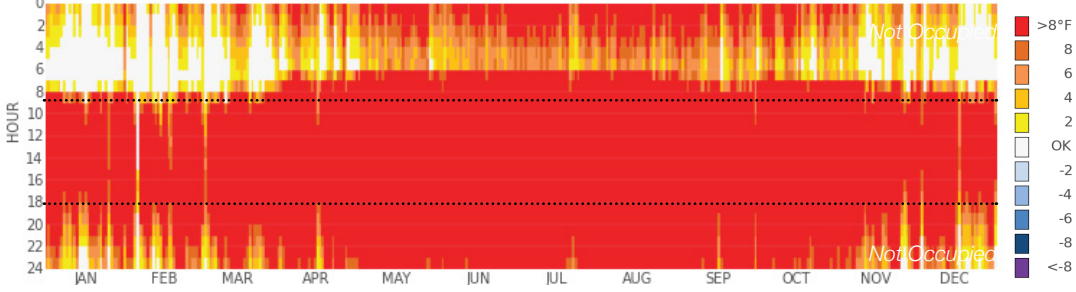
Degrees from comfort for bottom floor



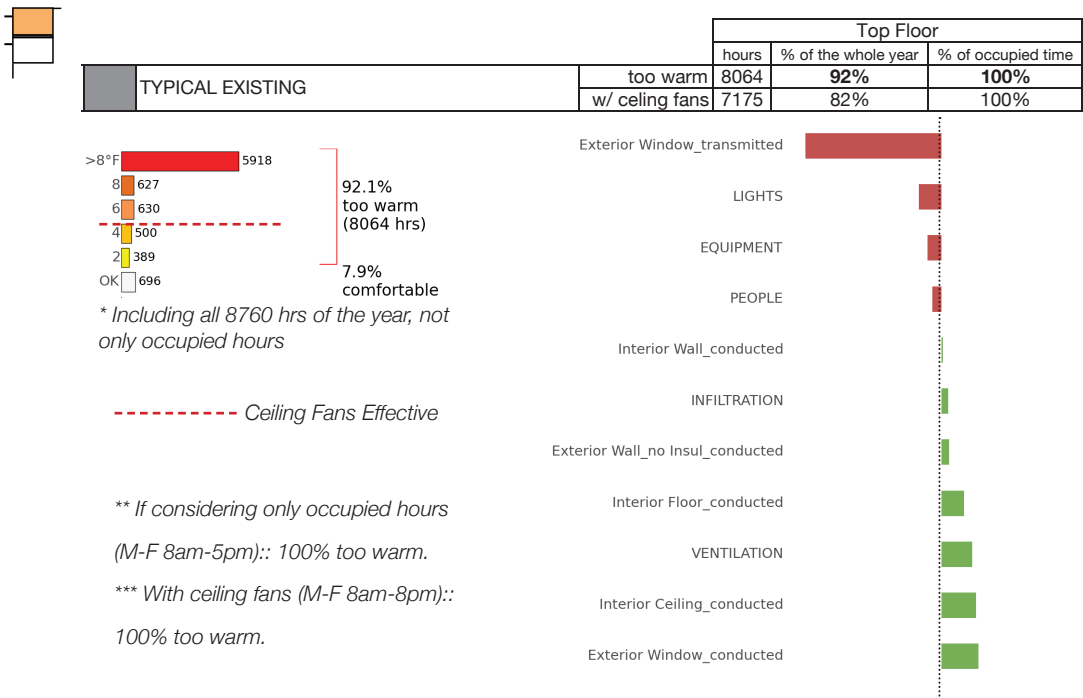
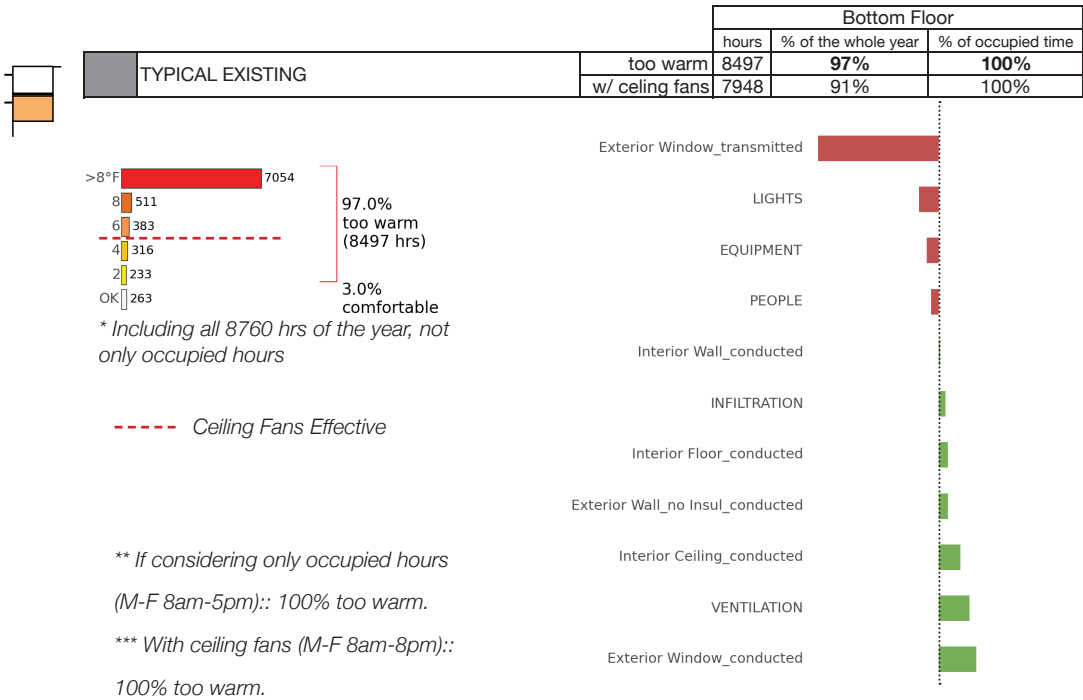
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.c.0 Office Analysis:: East Facing (Continued)



Add/C.4.c. OFFICE ANALYSIS:: EAST FACING

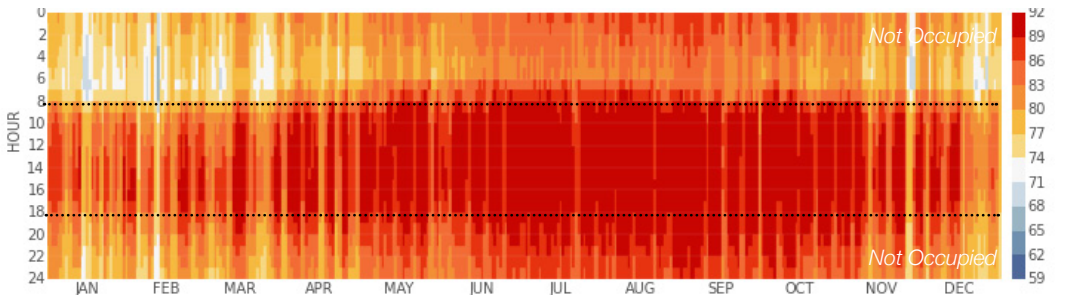


C.4.c.1. TYPICAL WITH WINDOW IMPROVEMENTS

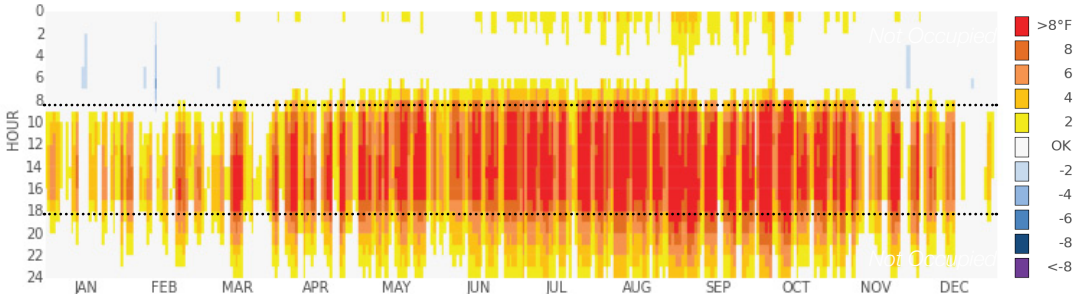
Equal to TYPICAL + 1ACH + Shading + IECC 2015 Windows



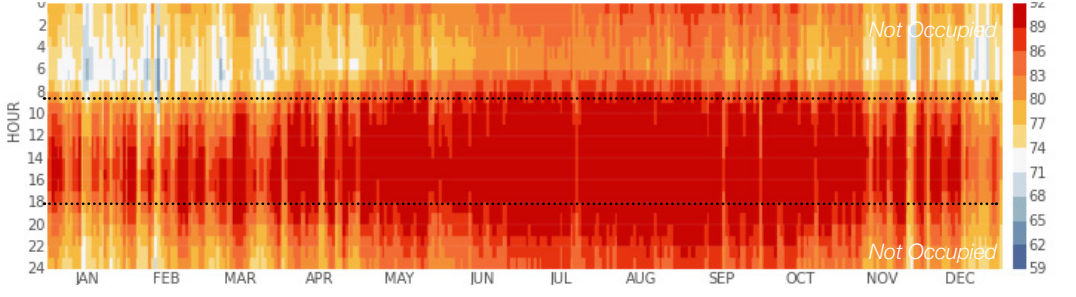
Operative temperature for bottom floor



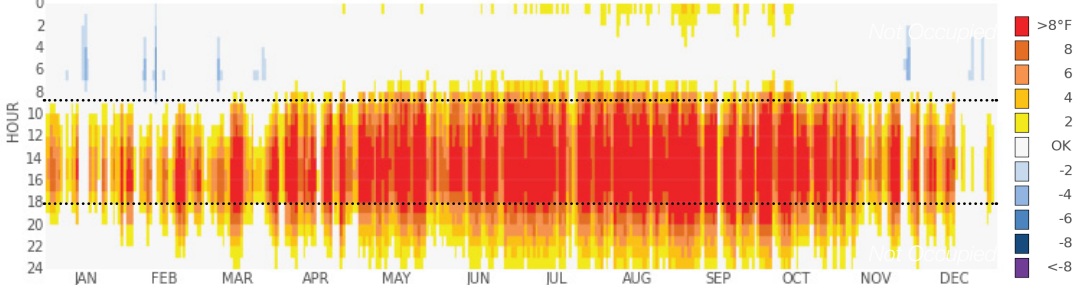
Degrees from comfort for bottom floor



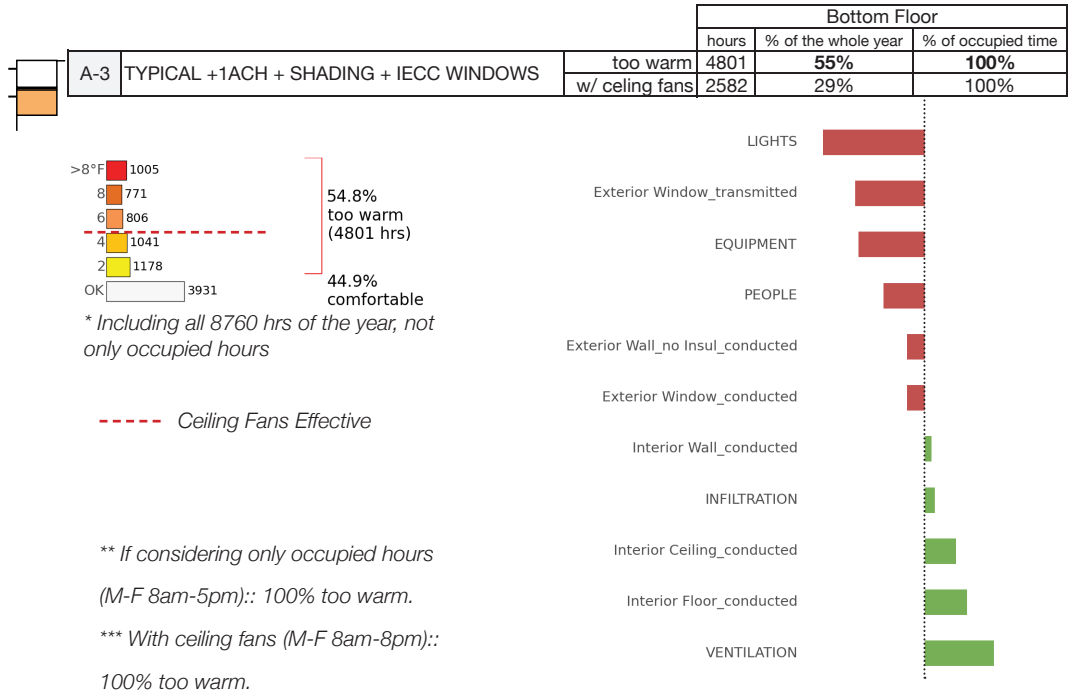
Operative temperature for top floor



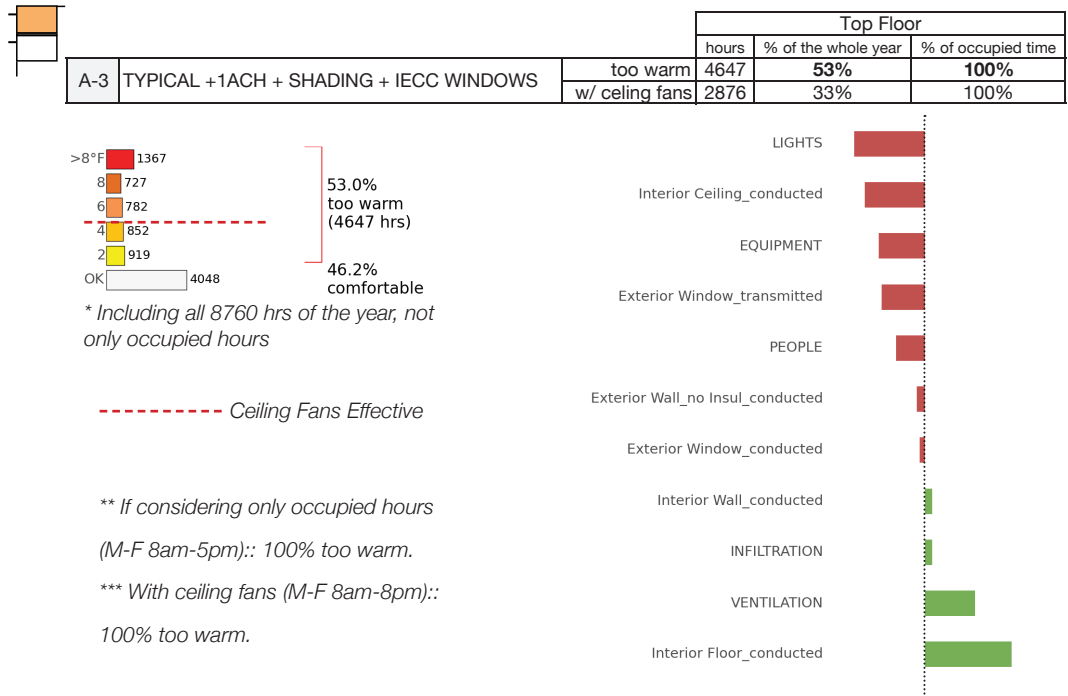
Degrees from comfort for top floor



Add/C.4.c.1 Office Analysis:: East Facing (Continued)



A-3 TYPICAL +1ACH +



Add/C.4.c. OFFICE ANALYSIS:: EAST FACING

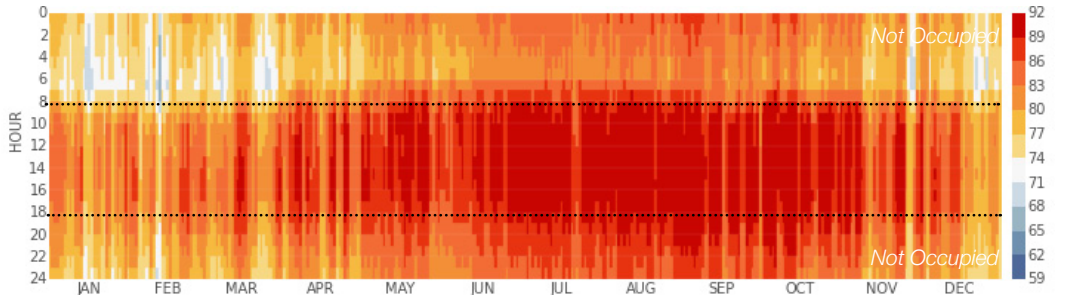


C.4.c.2. MINIMUM SUITE

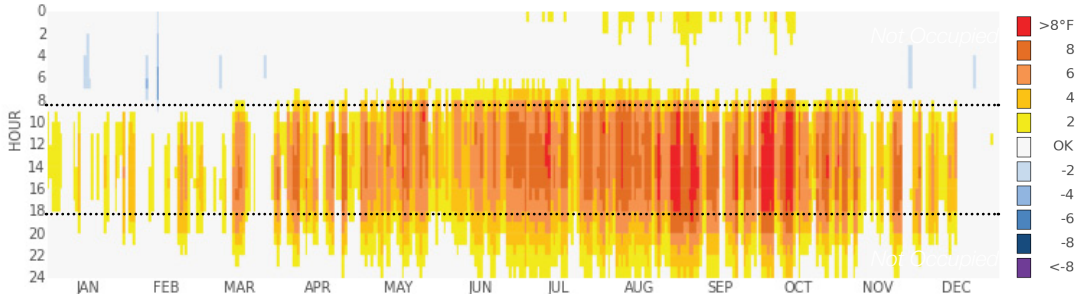
Equal to TYPICAL + IECC Windows + Shading +lower LPD + Daylight Controls +1ACH



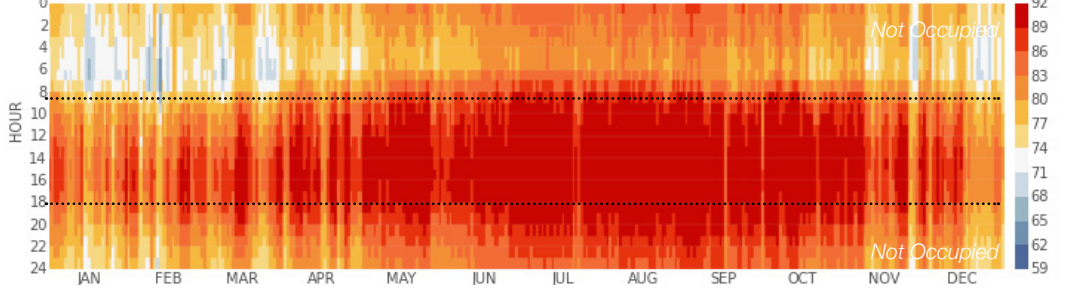
Operative temperature for bottom floor



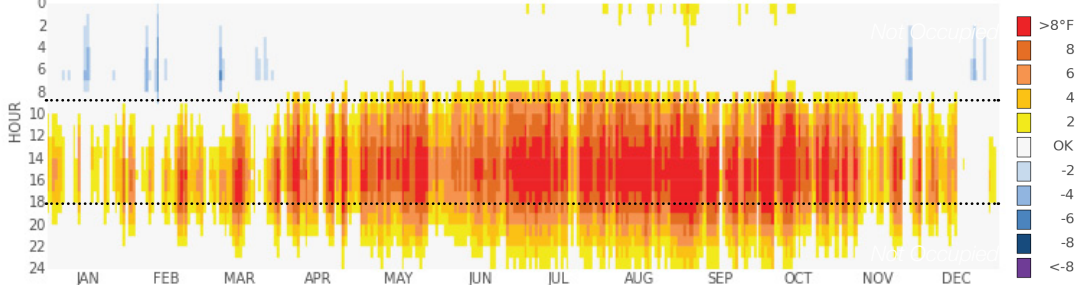
Degrees from comfort for bottom floor



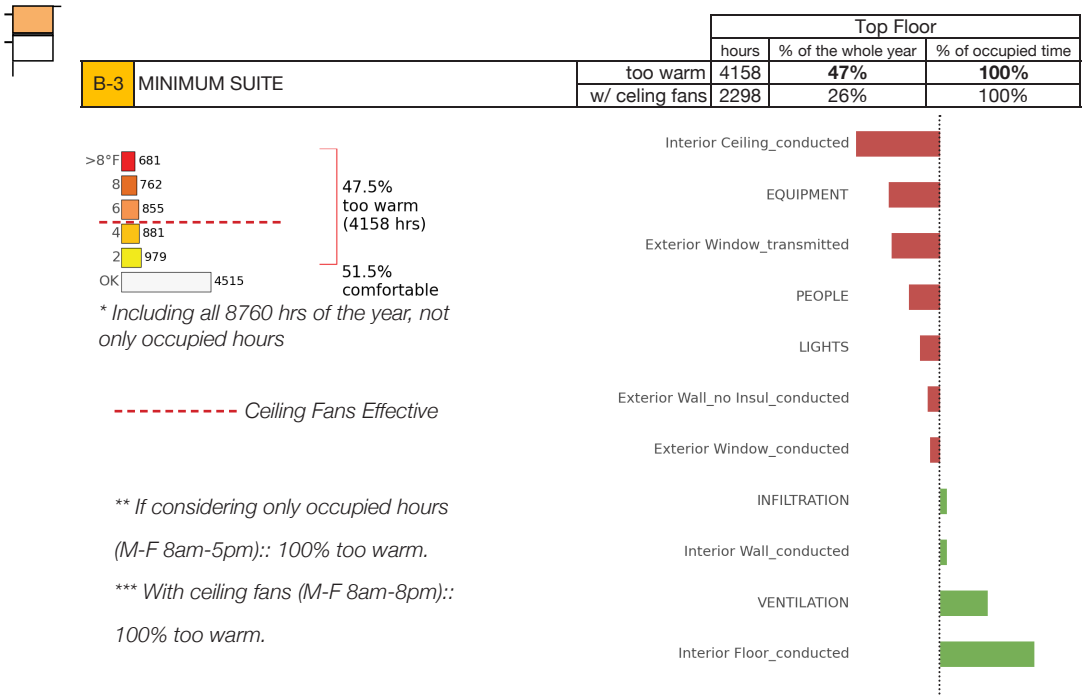
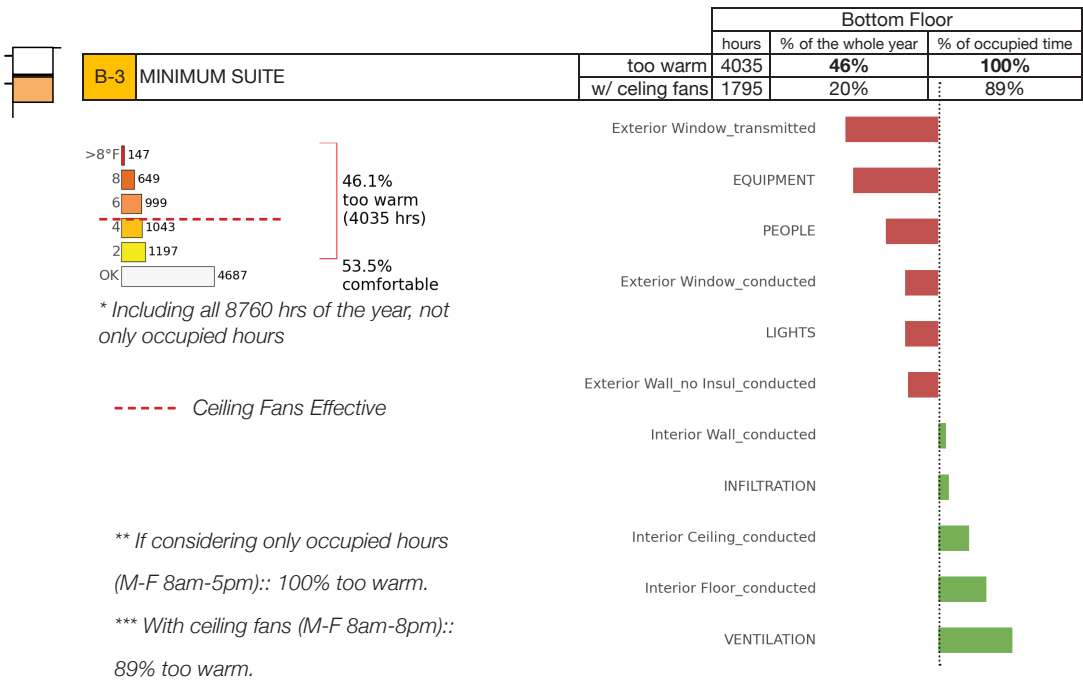
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.c.2 Office Analysis:: East Facing (Continued)



Add/C.4.c. OFFICE ANALYSIS:: EAST FACING

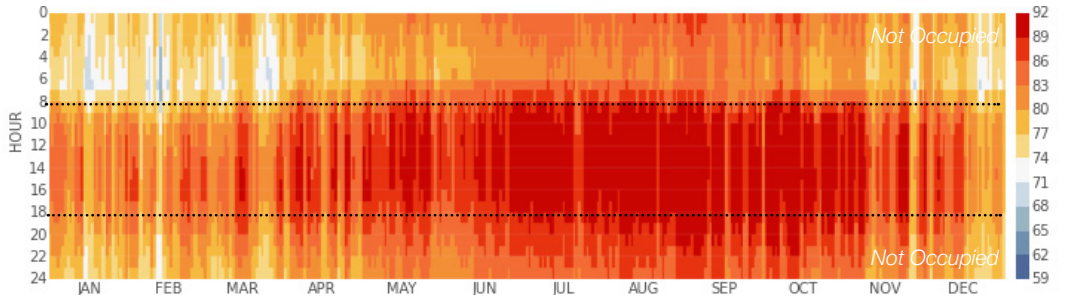


C.4.c.3. IMPROVED SUITE

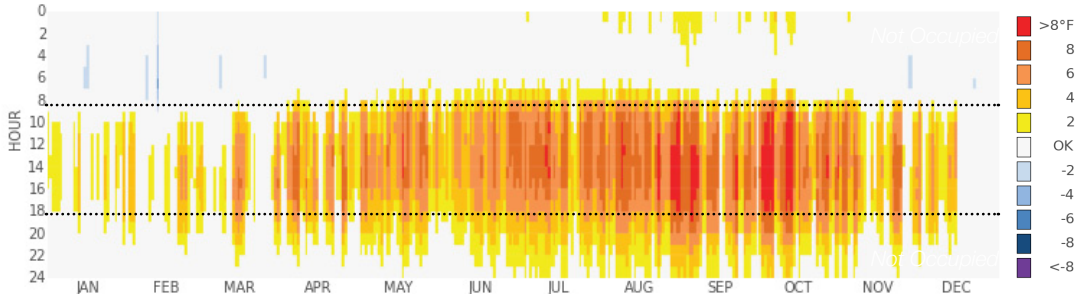
Equal to MINIMUM SUITE + IECC Roof



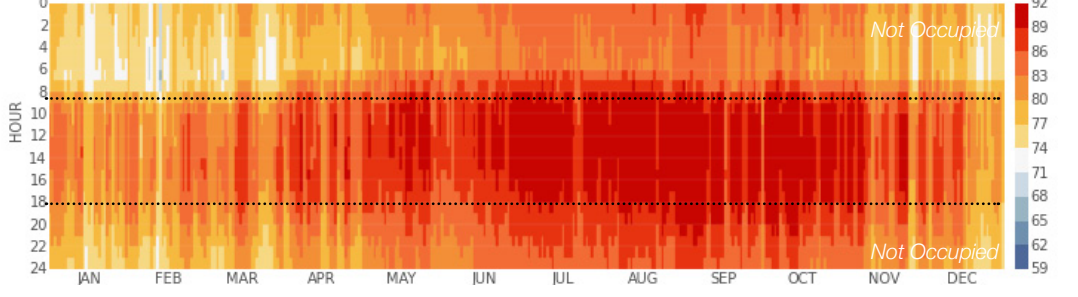
Operative temperature for bottom floor



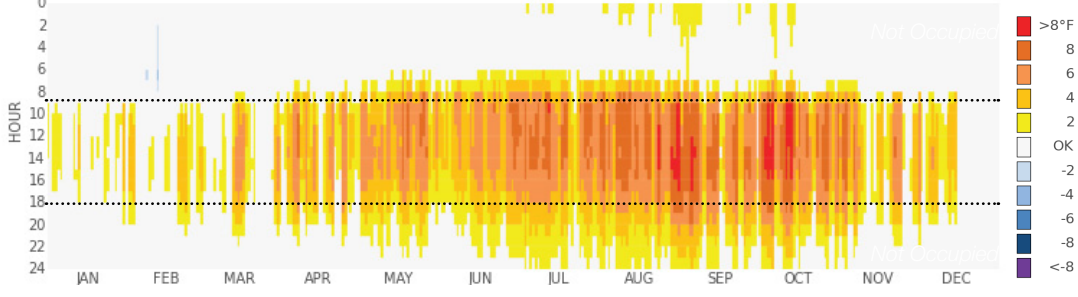
Degrees from comfort for bottom floor



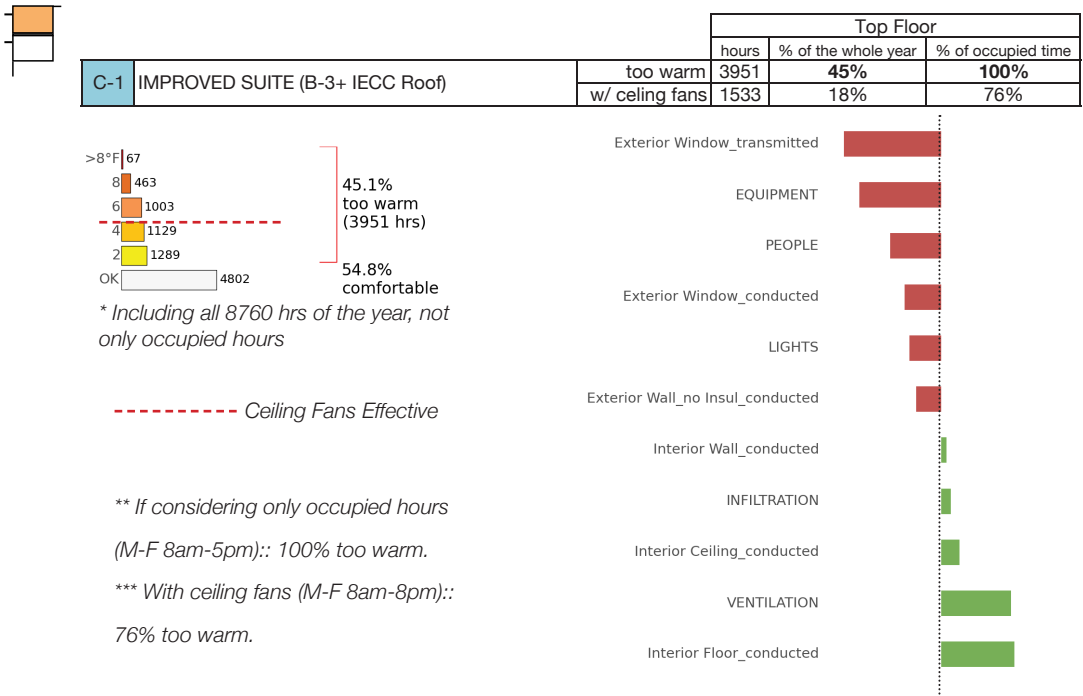
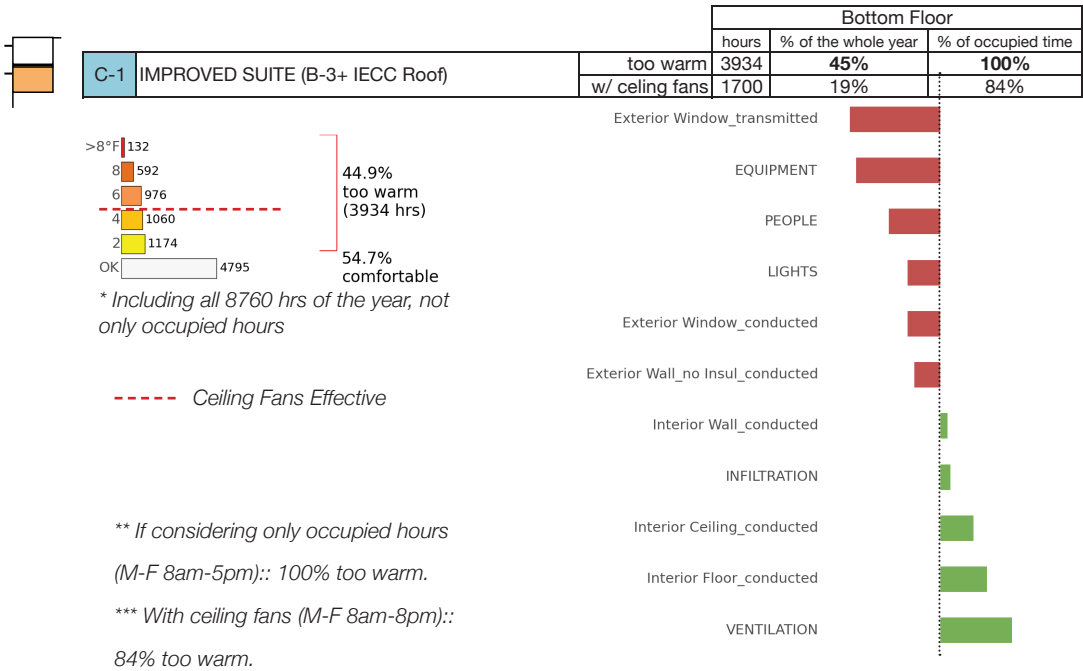
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.c.3 Office Analysis:: East Facing (Continued)



Add/C.4.c. OFFICE ANALYSIS:: EAST FACING

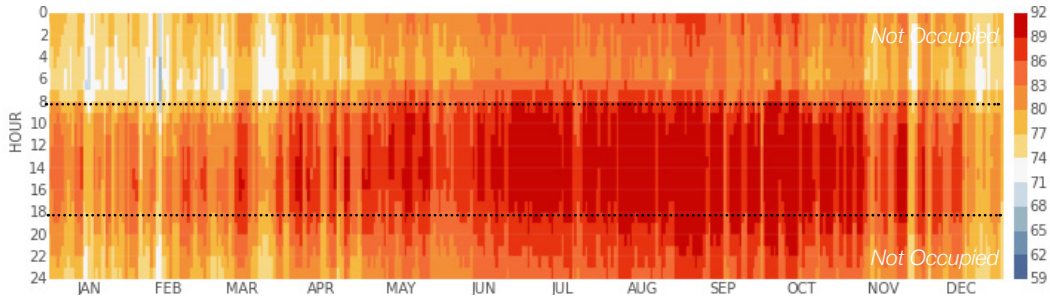


C.4.c.4. CODE SUITE

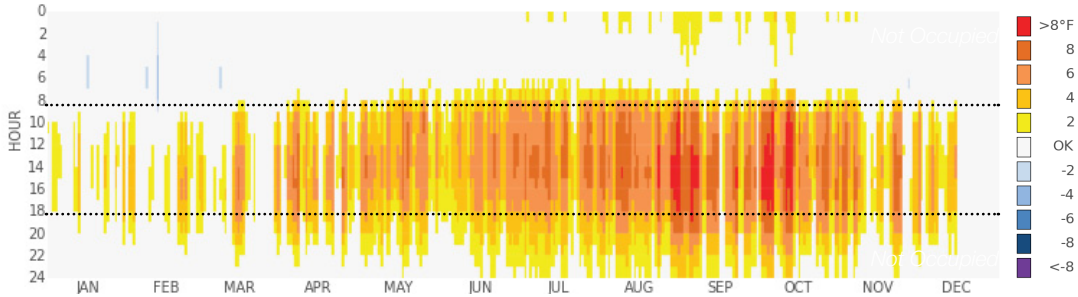
Equal to IMPROVED SUITE + IECC Walls



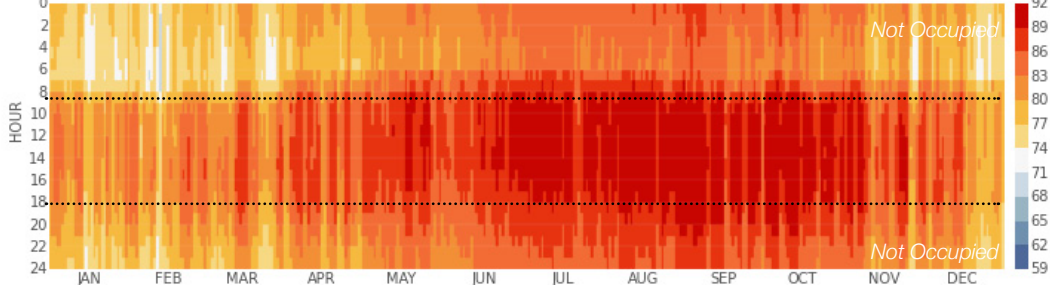
Operative temperature for bottom floor



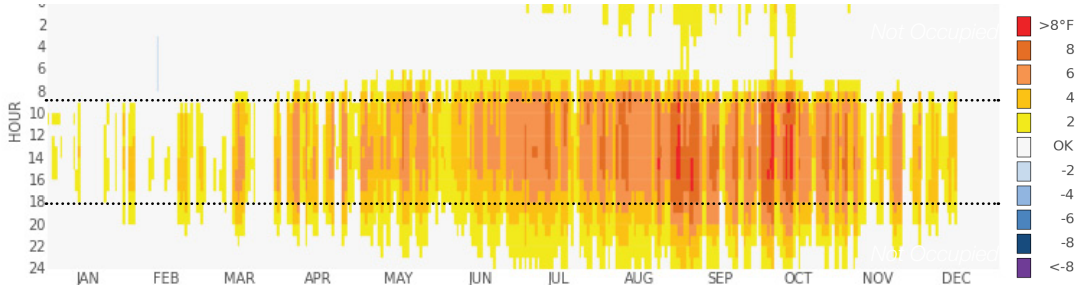
Degrees from comfort for bottom floor



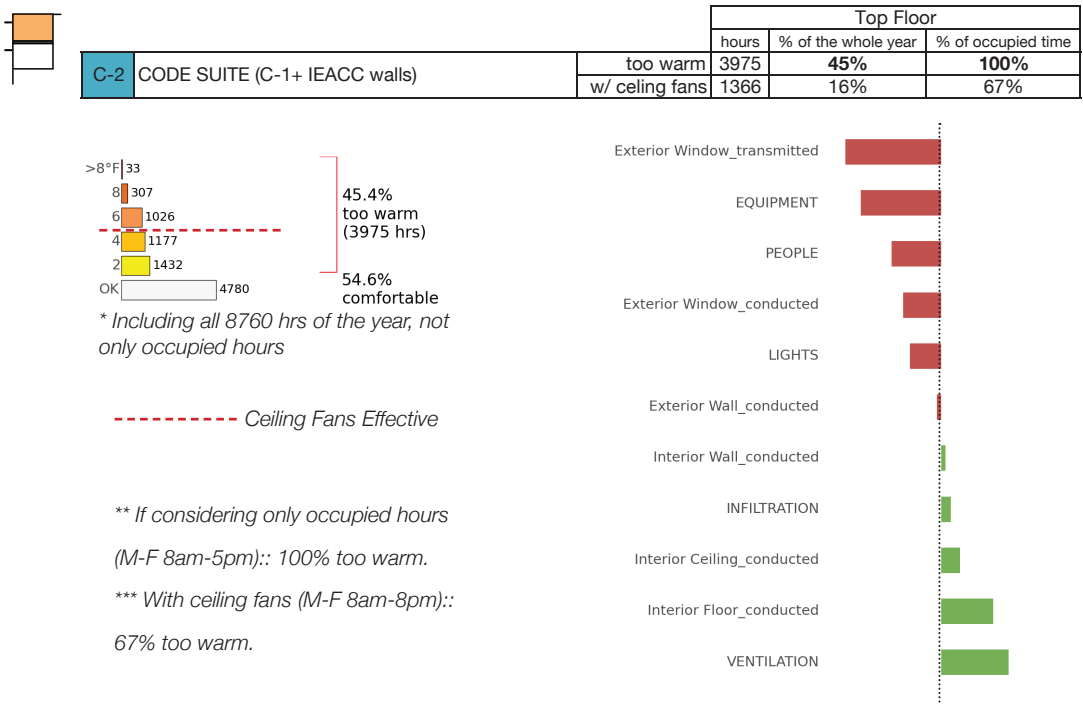
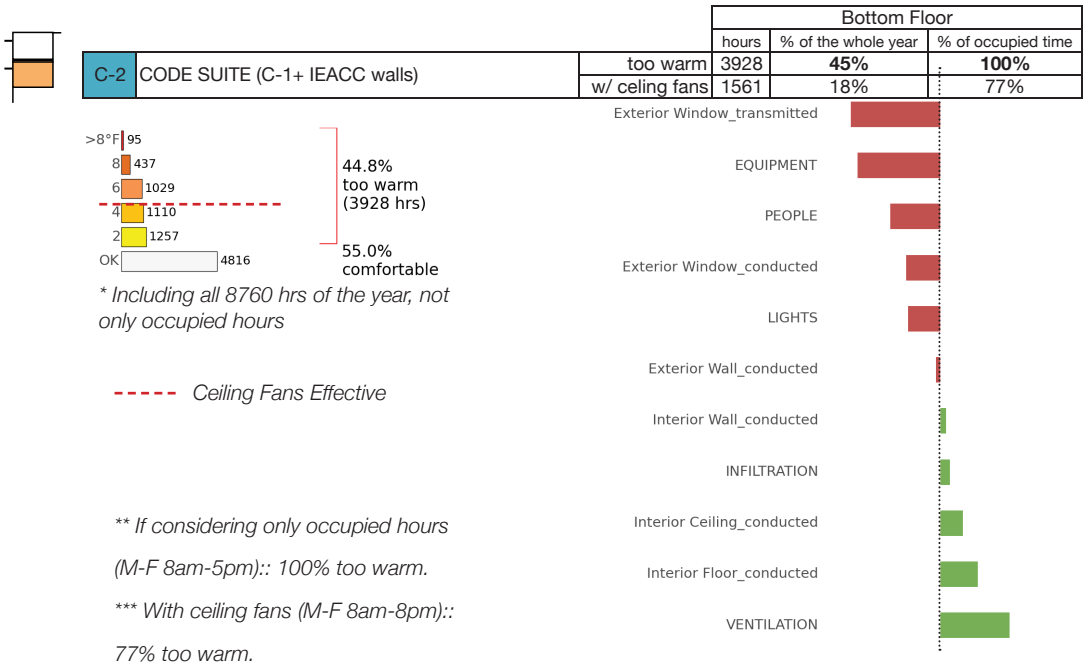
Operative temperature for top floor



Degrees from comfort for top floor



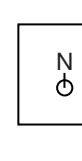
Add/C.4.c.4 Office Analysis:: East Facing (Continued)



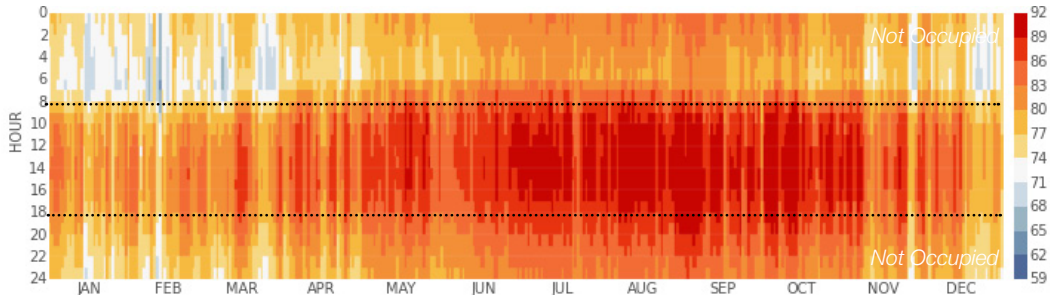
Add/C.4.c. OFFICE ANALYSIS:: EAST FACING

C.4.c.5. IMPROVED SUITE WITH VENTILATION

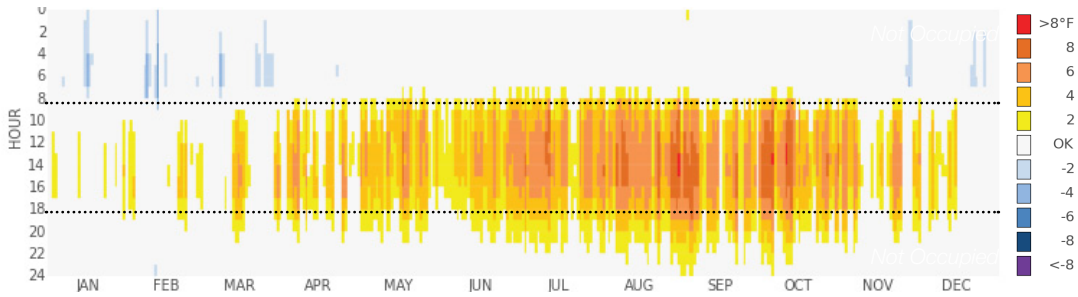
Equal to IMPROVED SUITE +2ACH



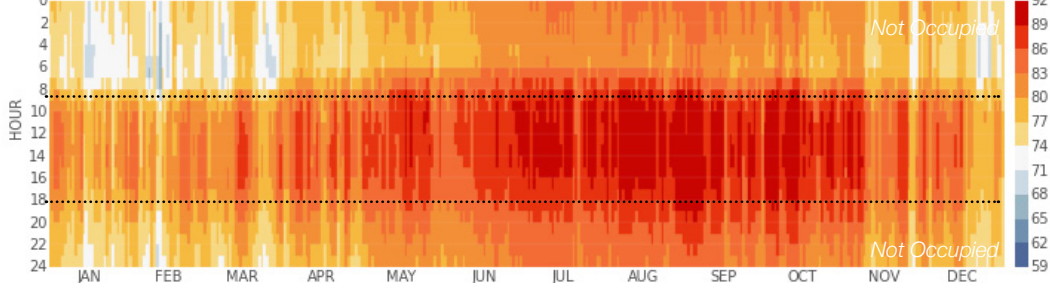
Operative temperature for bottom floor



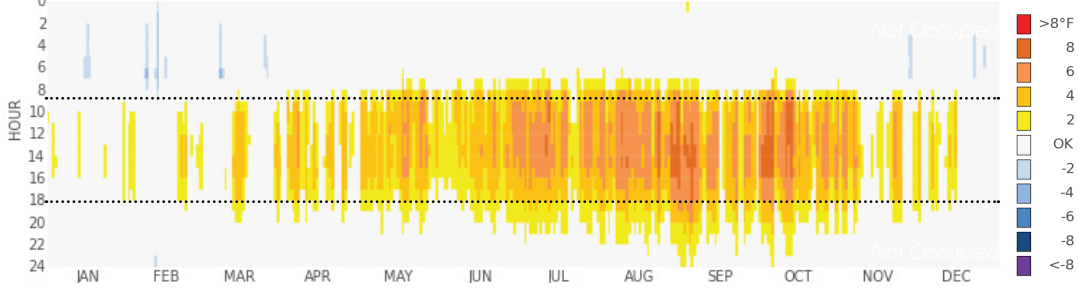
Degrees from comfort for bottom floor



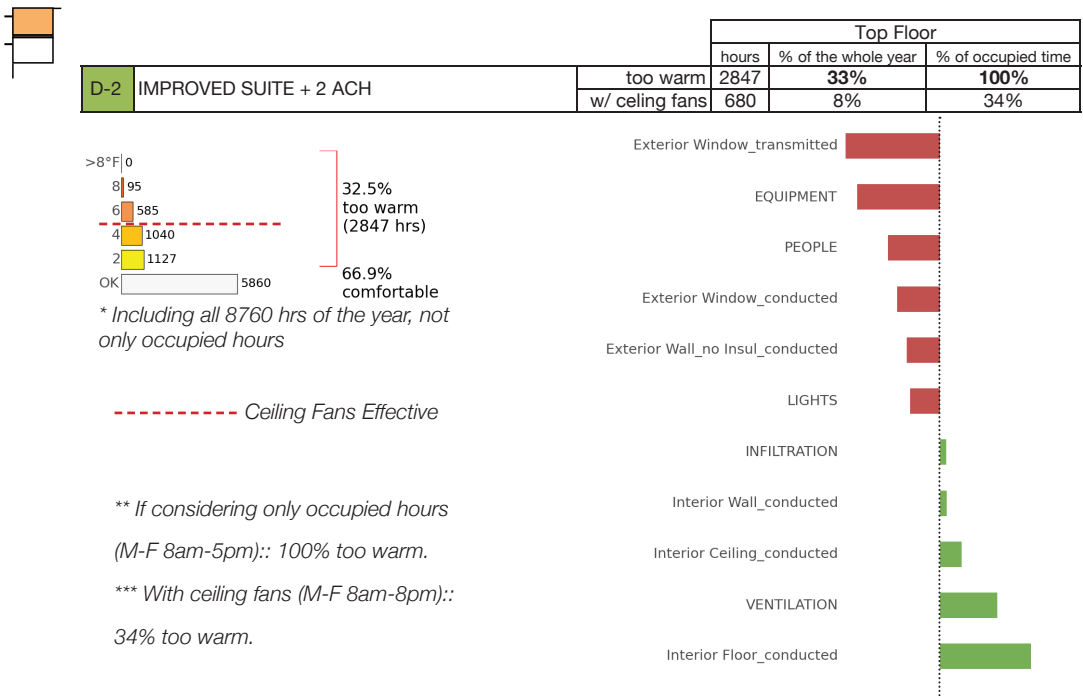
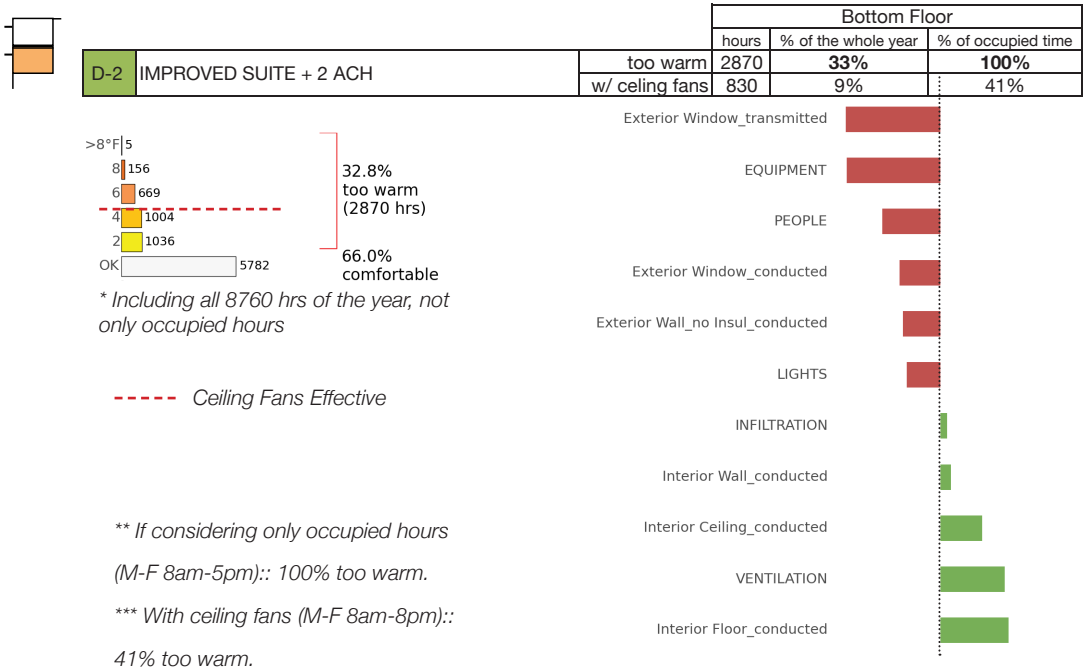
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.c.5 Office Analysis:: East Facing (Continued)



Add/C.4.c. OFFICE ANALYSIS:: EAST FACING

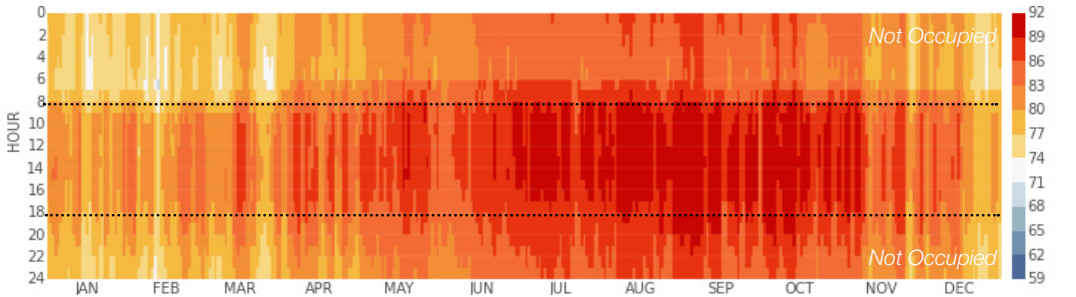
C.4.c.6. IDEAL SUITE



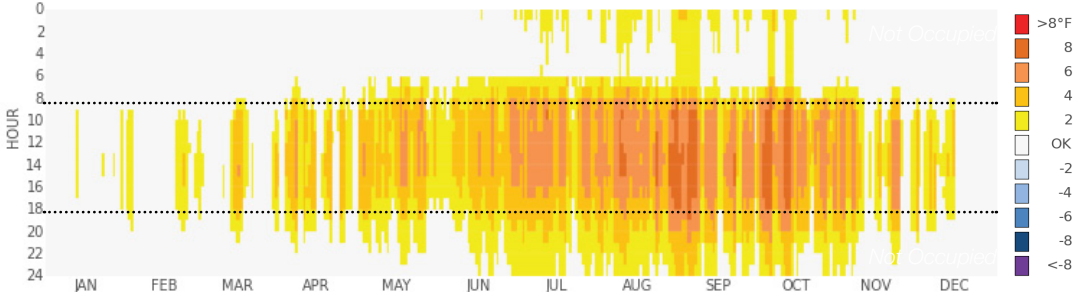
Equal to CODE SUITE + Thermal Mass



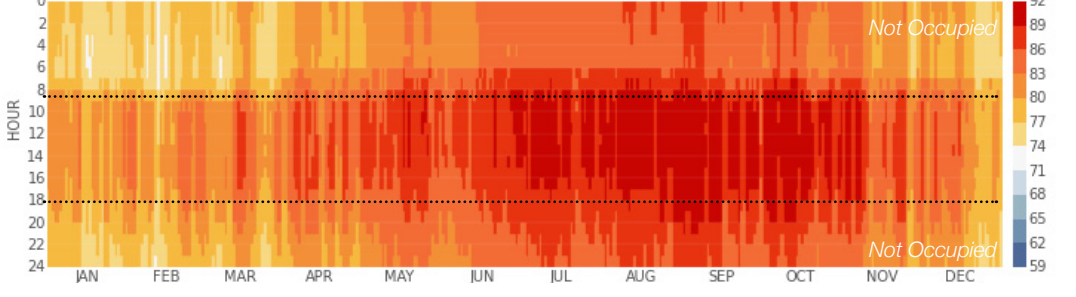
Operative temperature for bottom floor



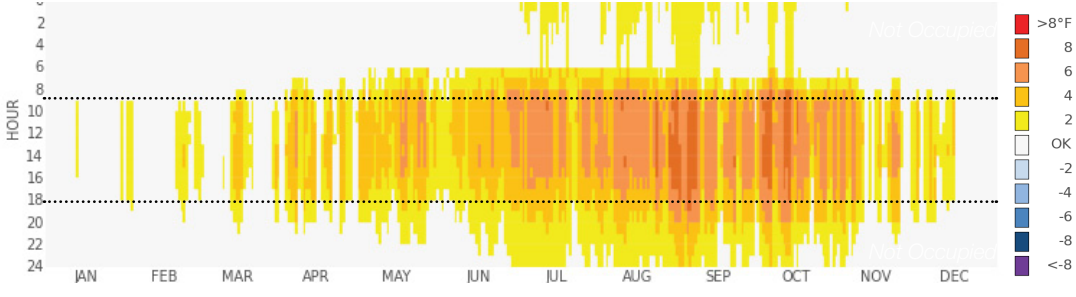
Degrees from comfort for bottom floor



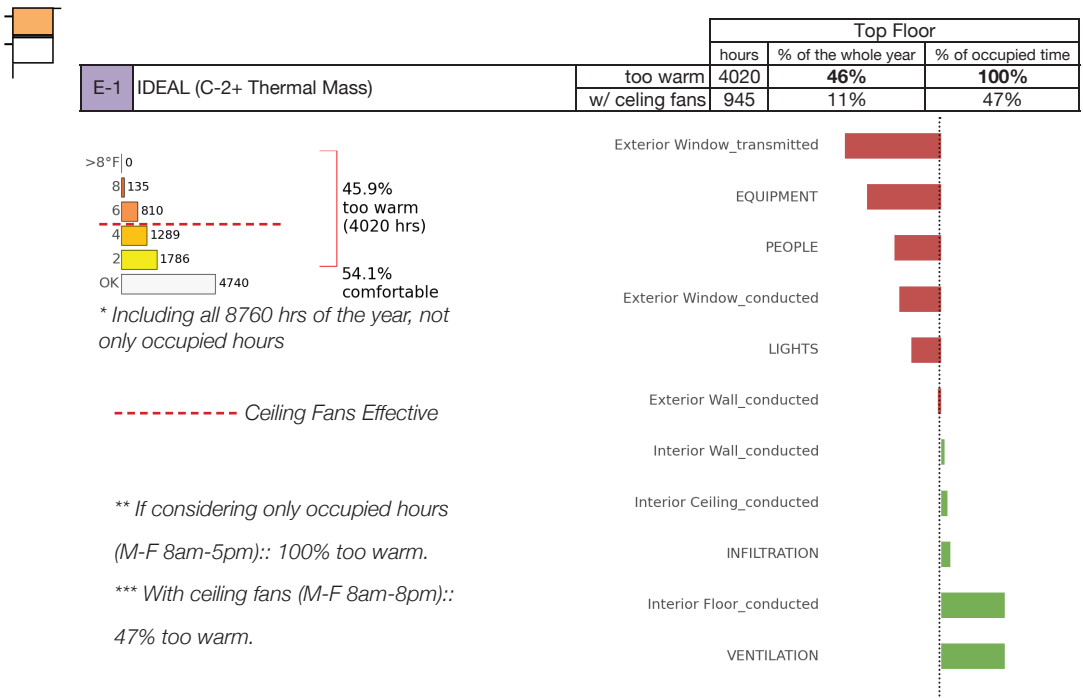
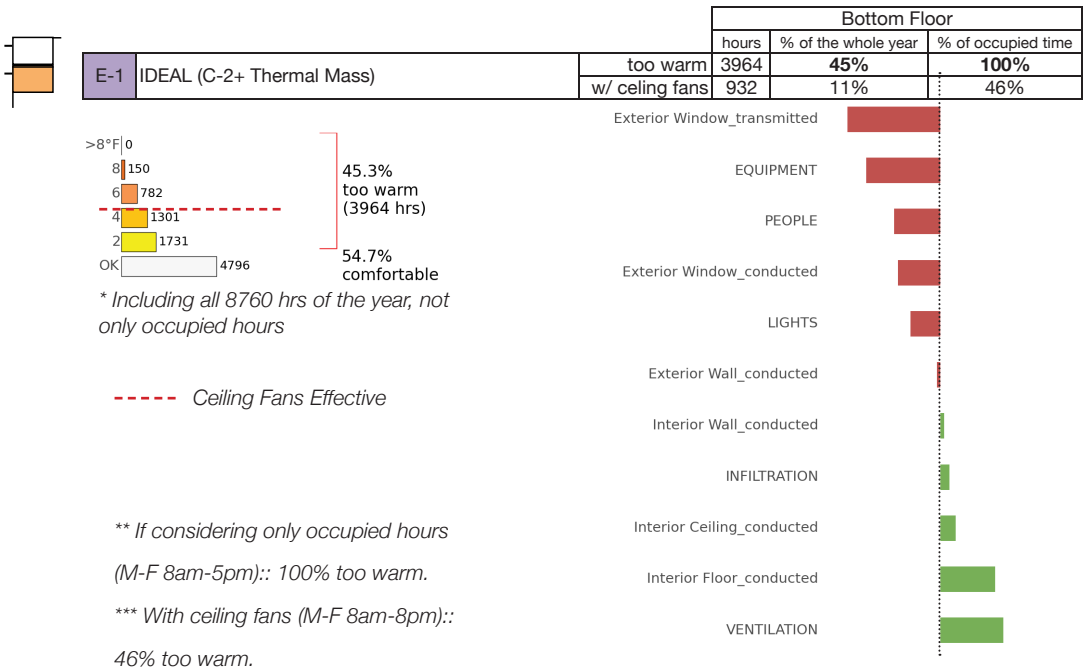
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.c.6 Office Analysis:: East Facing (Continued)



Add/C.4.c. OFFICE ANALYSIS:: EAST FACING

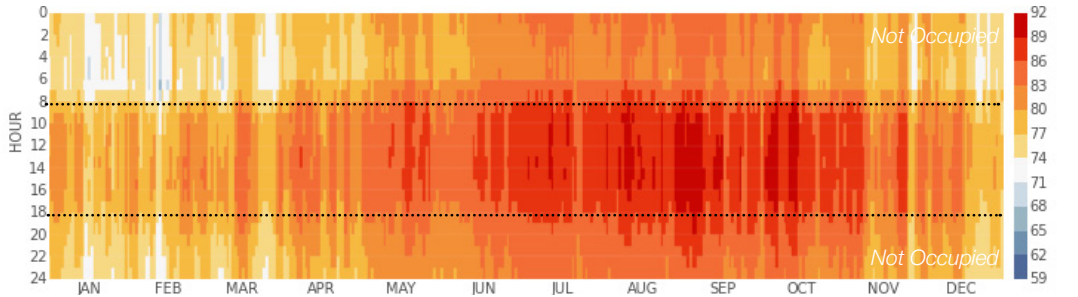
C.4.c.7. IDEAL SUITE WITH VENTILATION



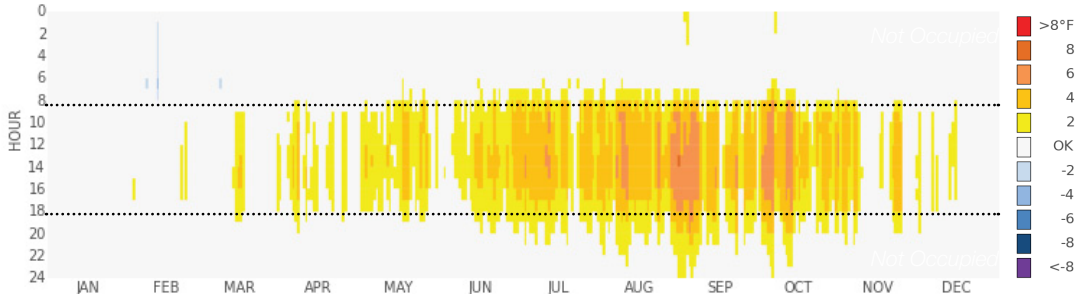
Equal to IDEAL SUITE + 2ACH



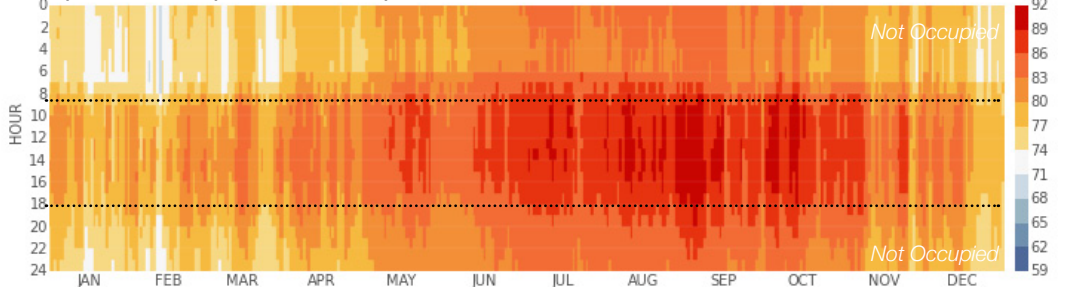
Operative temperature for bottom floor



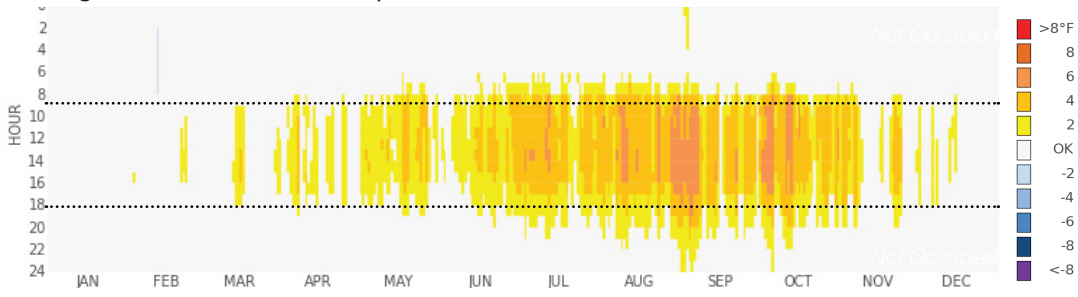
Degrees from comfort for bottom floor



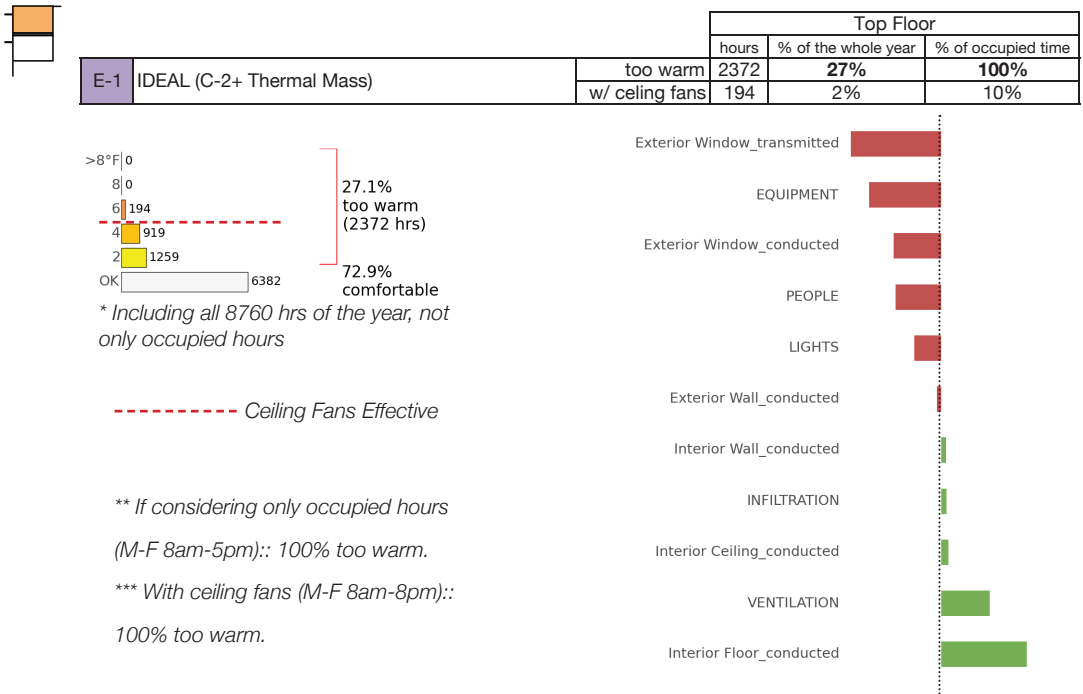
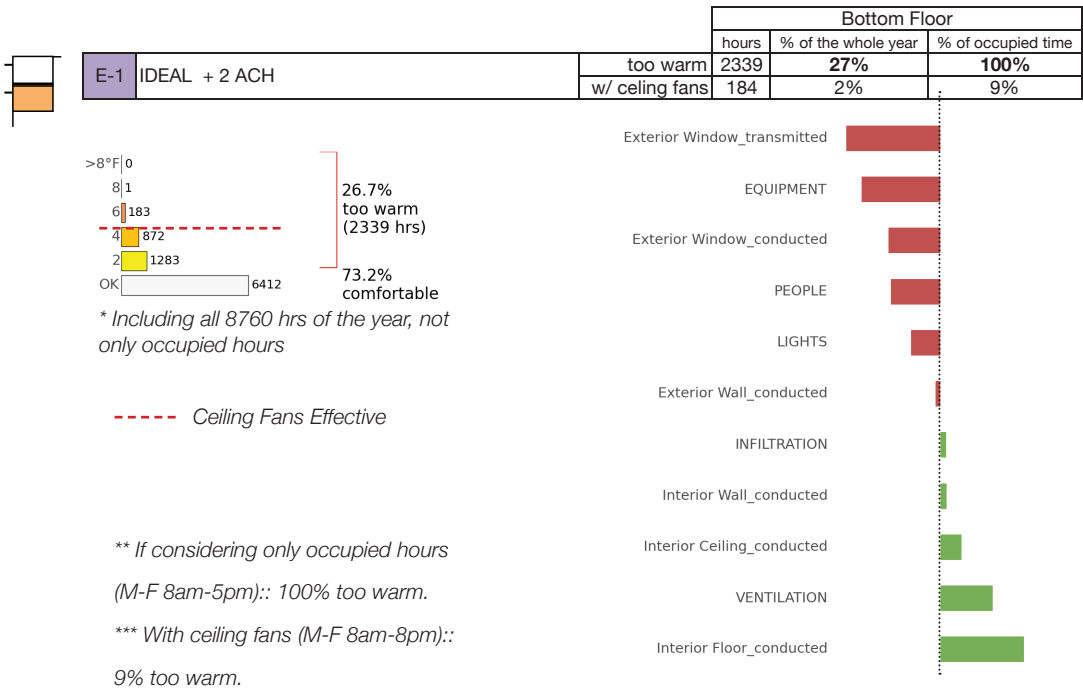
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.c.7 Office Analysis:: East Facing (Continued)



Add/C.4.d OFFICE ANALYSIS:: WEST FACING

C.4.d.0. TYPICAL EXISTING CONDITIONS

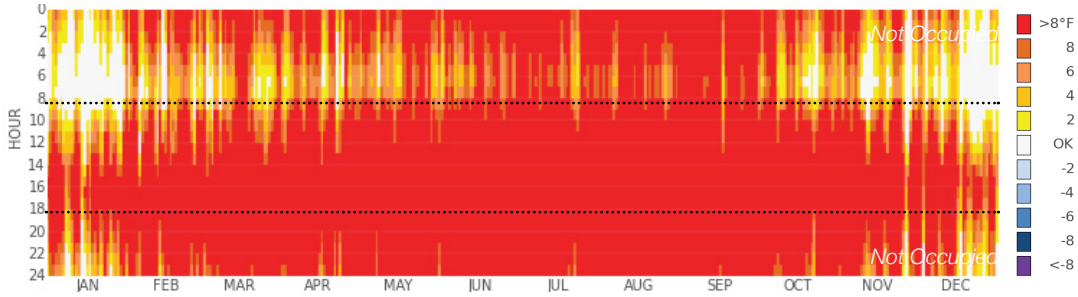
No Insulation in Opaque Surfaces and Single Pane Glass



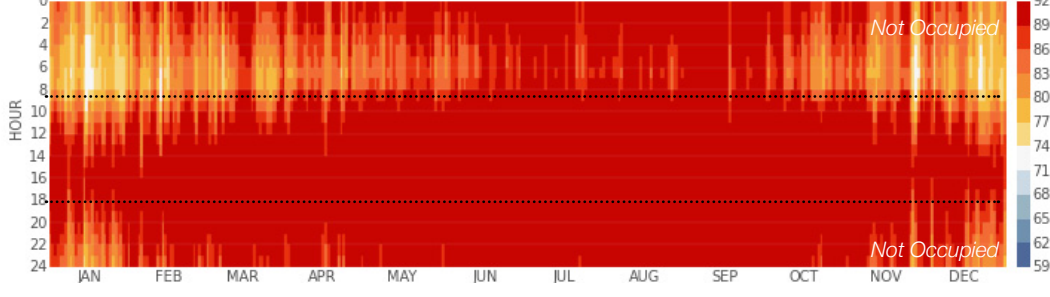
Operative temperature for bottom floor



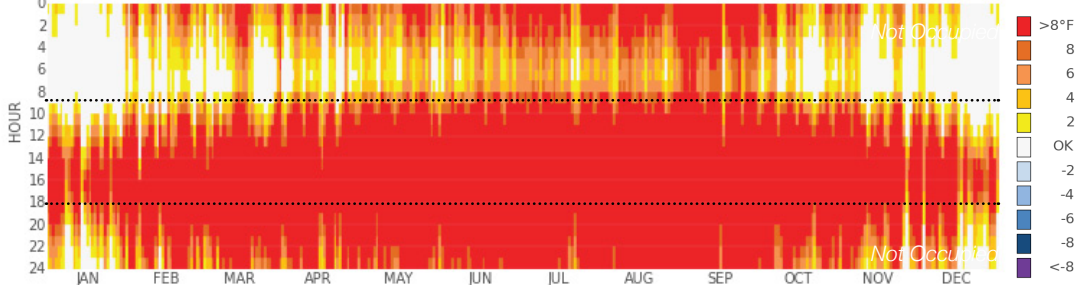
Degrees from comfort for bottom floor



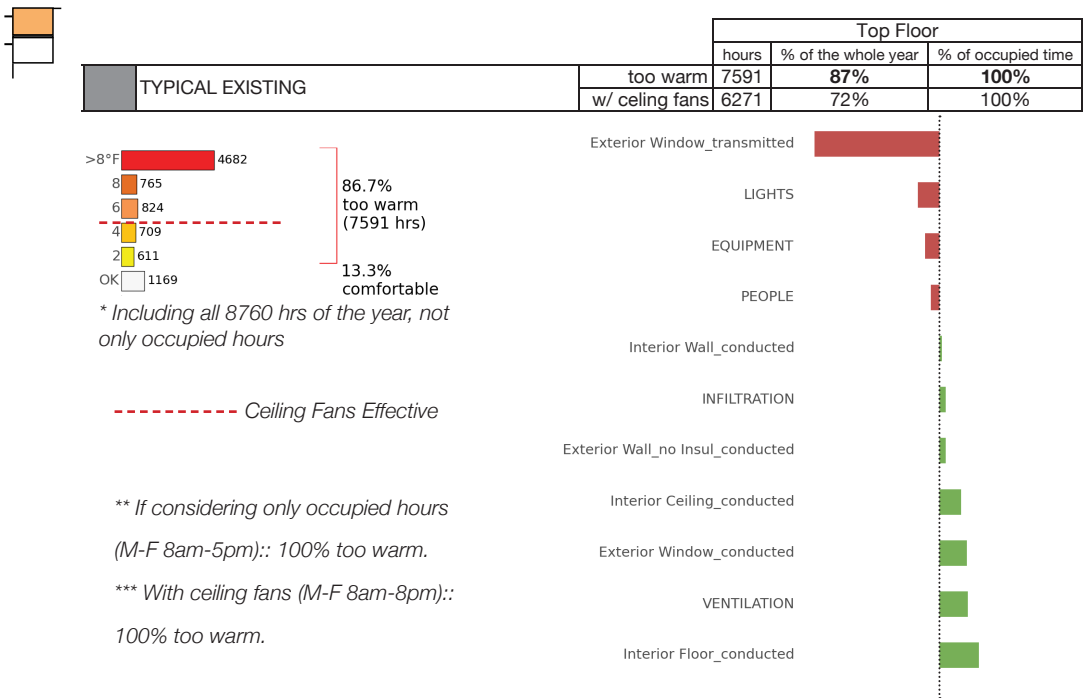
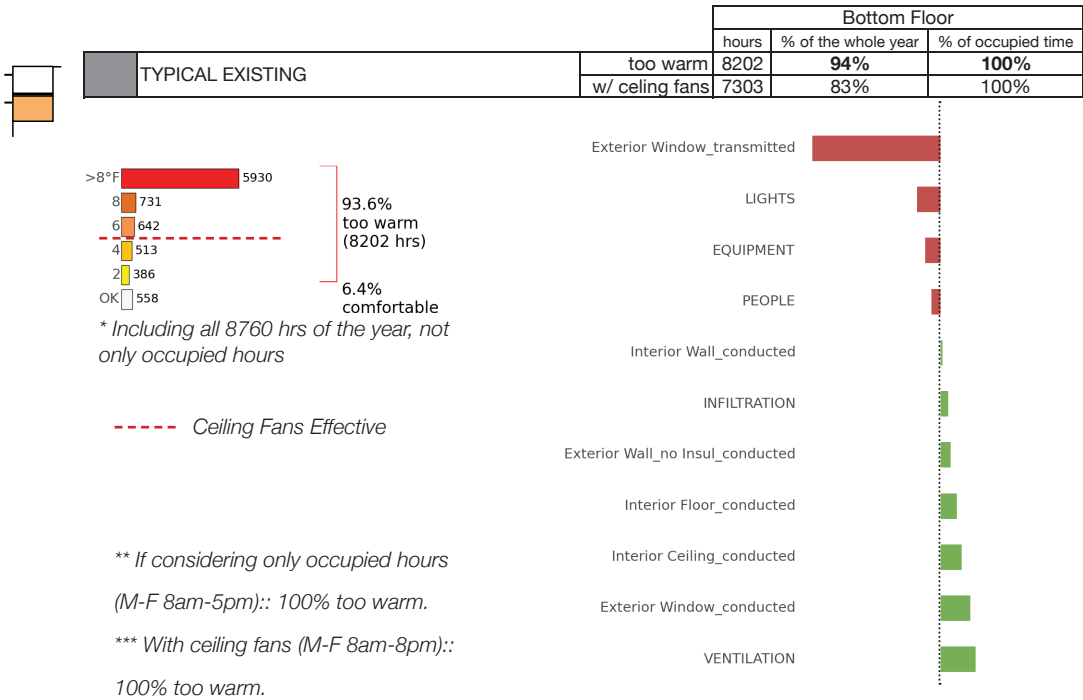
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.d.0 Office Analysis:: West Facing (Continued)



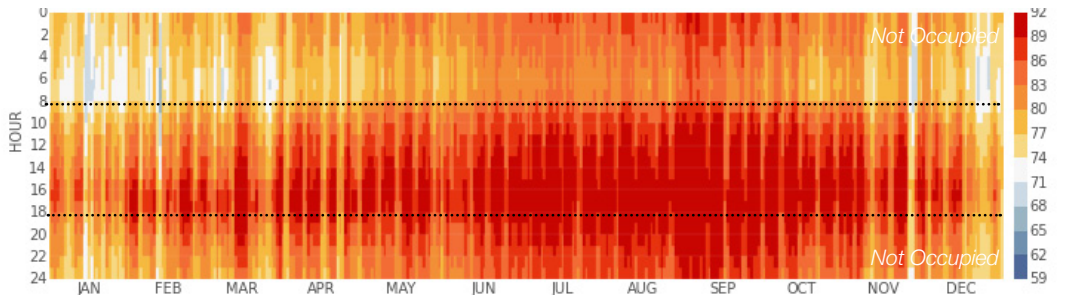
Add/C.4.d OFFICE ANALYSIS:: WEST FACING

C.4.d.1. TYPICAL WITH WINDOW IMPROVEMENTS

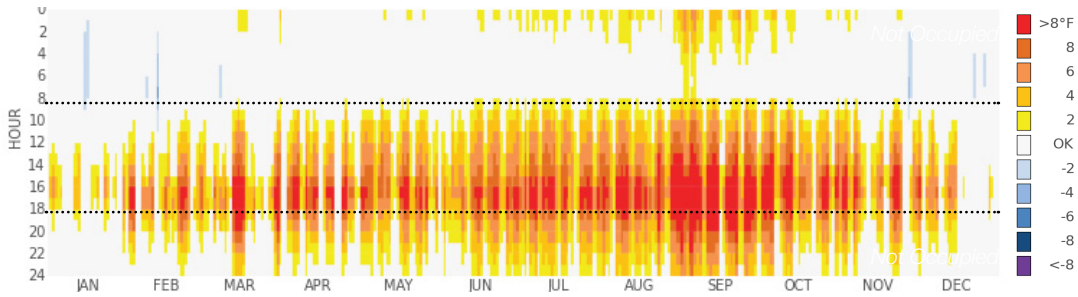
Equal to TYPICAL + 1ACH + Shading + IECC 2015 Windows



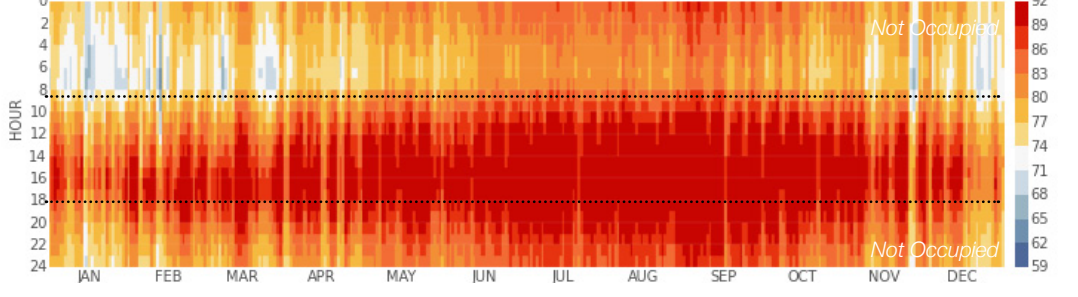
Operative temperature for bottom floor



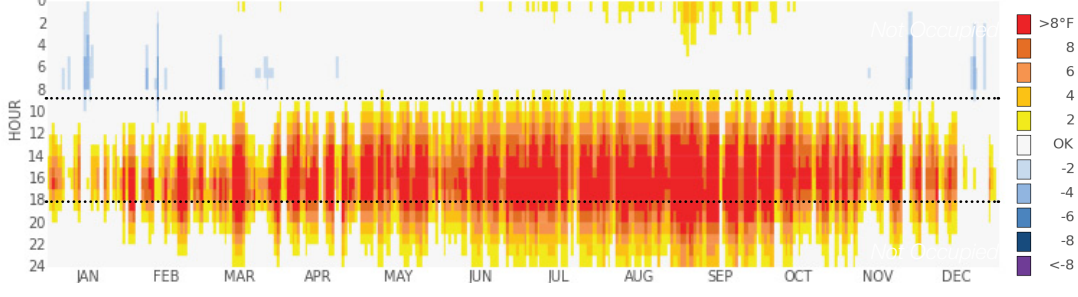
Degrees from comfort for bottom floor



Operative temperature for top floor



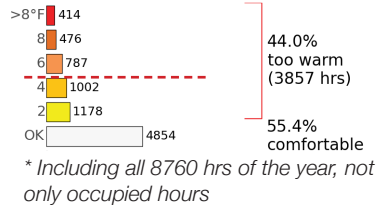
Degrees from comfort for top floor



Add/C.4.d.1 Office Analysis:: West Facing (Continued)

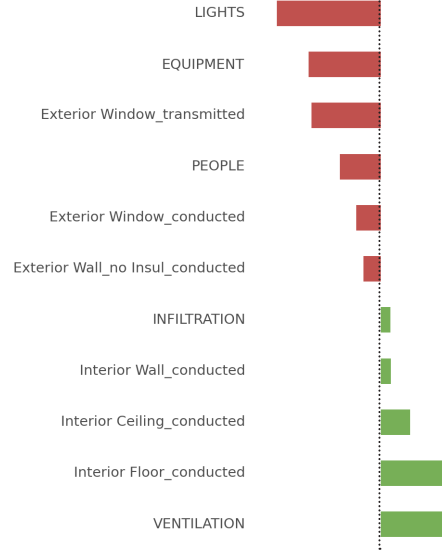
		Bottom Floor			
		hours	% of the whole year	% of occupied time	
A-3	TYPICAL +1ACH + SHADING + IECC WINDOWS	too warm	3857	44%	100%
		w/ ceiling fans	1677	19%	83%

A-3 TYPICAL +1ACH +

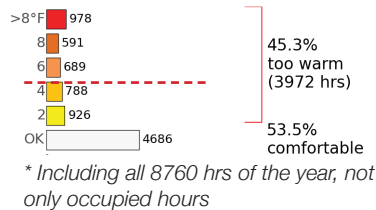


----- Ceiling Fans Effective

** If considering only occupied hours (M-F 8am-5pm):: 100% too warm.
*** With ceiling fans (M-F 8am-8pm):: 83% too warm.

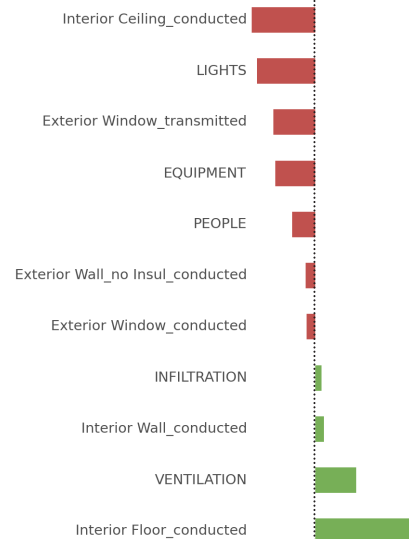


		Top Floor			
		hours	% of the whole year	% of occupied time	
A-3	TYPICAL +1ACH + SHADING + IECC WINDOWS	too warm	3972	45%	100%
		w/ ceiling fans	2258	26%	100%



----- Ceiling Fans Effective

** If considering only occupied hours (M-F 8am-5pm):: 100% too warm.
*** With ceiling fans (M-F 8am-8pm):: 100% too warm.



Add/C.4.d OFFICE ANALYSIS:: WEST FACING

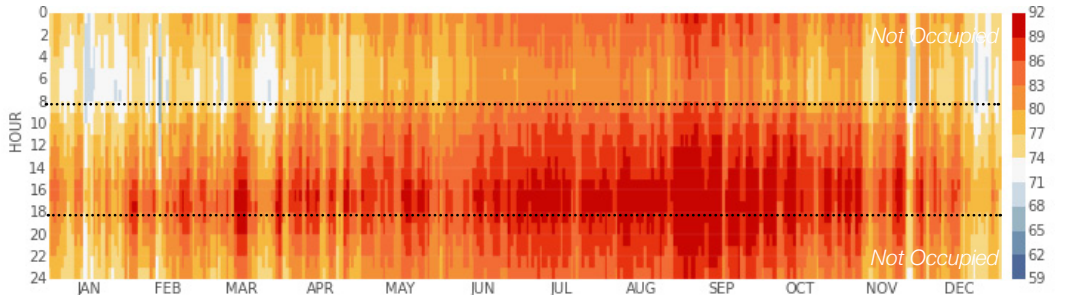
C.4.d.2. MINIMUM SUITE



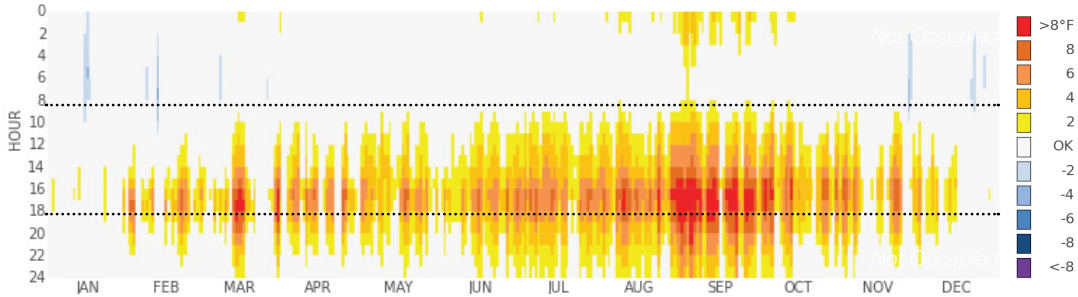
Equal to TYPICAL + IECC Windows + Shading +lower LPD + Daylight Controls +1ACH



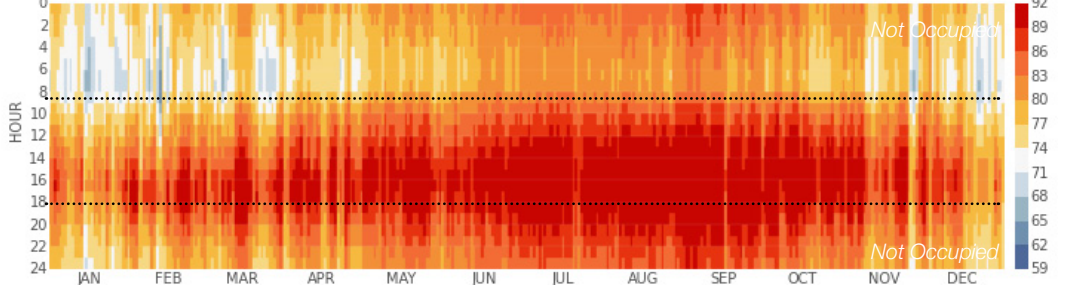
Operative temperature for bottom floor



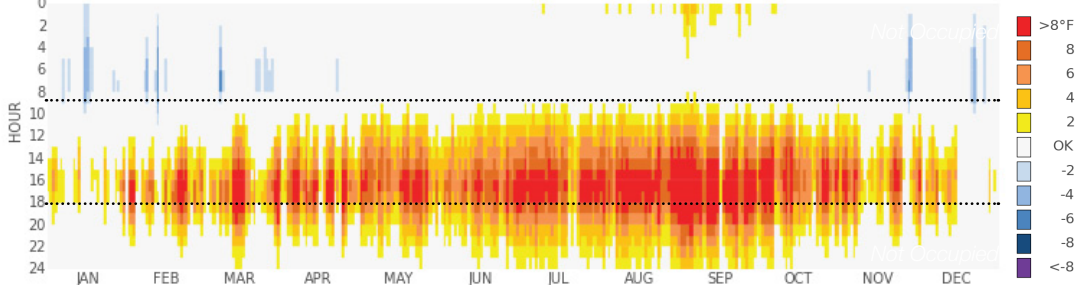
Degrees from comfort for bottom floor



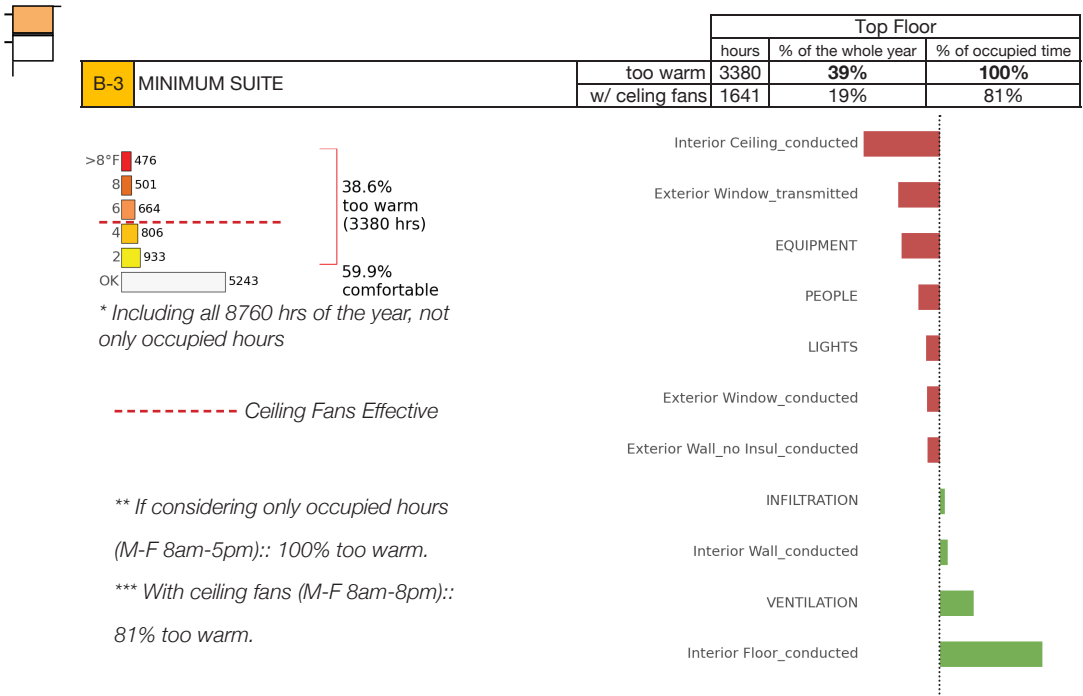
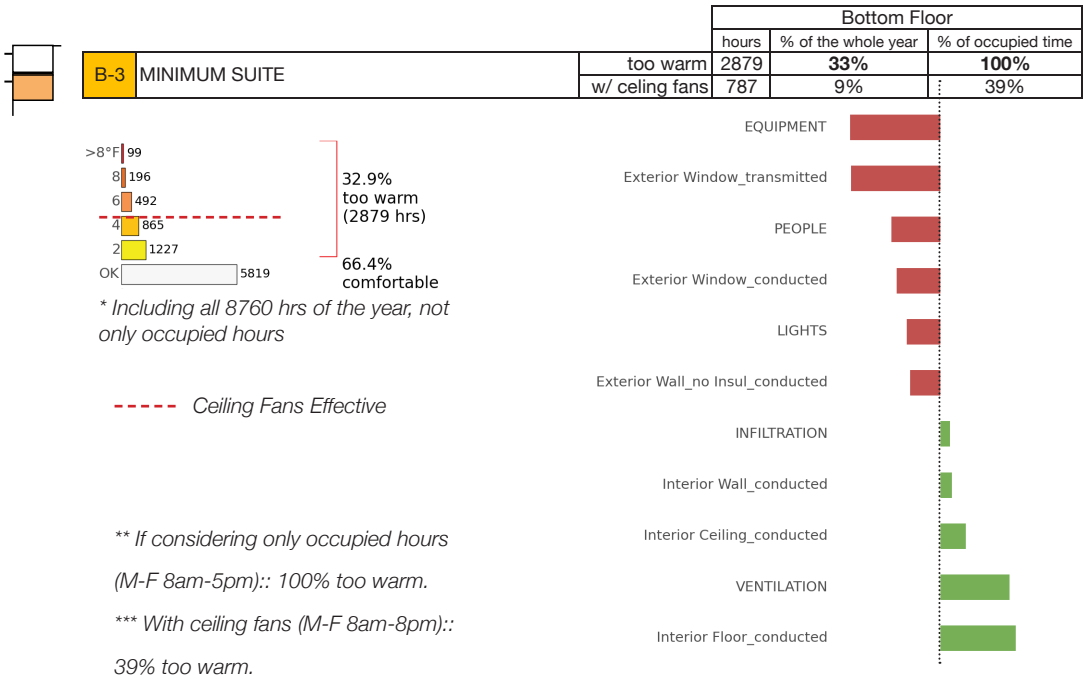
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.d.2 Office Analysis:: West Facing (Continued)



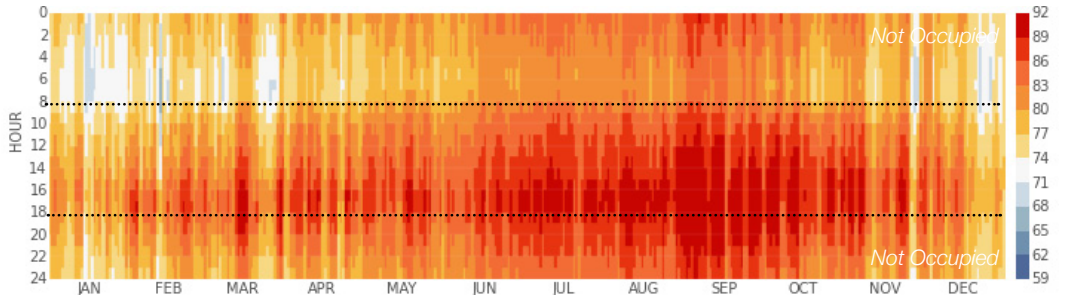
Add/C.4.d OFFICE ANALYSIS:: WEST FACING

C.4.d.3. IMPROVED SUITE

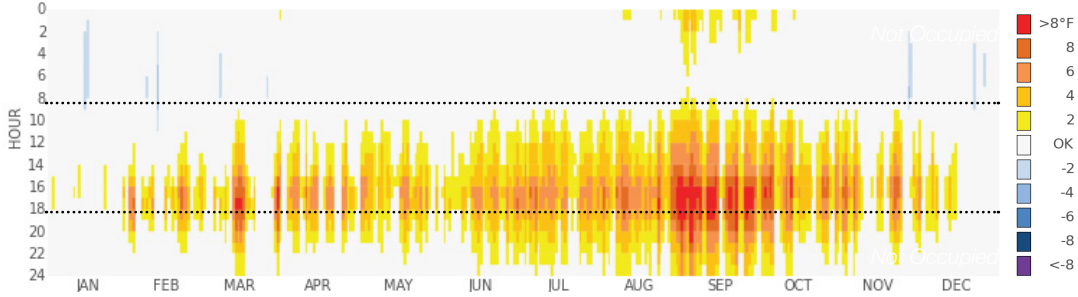
Equal to MINIMUM SUITE + IECC Roof



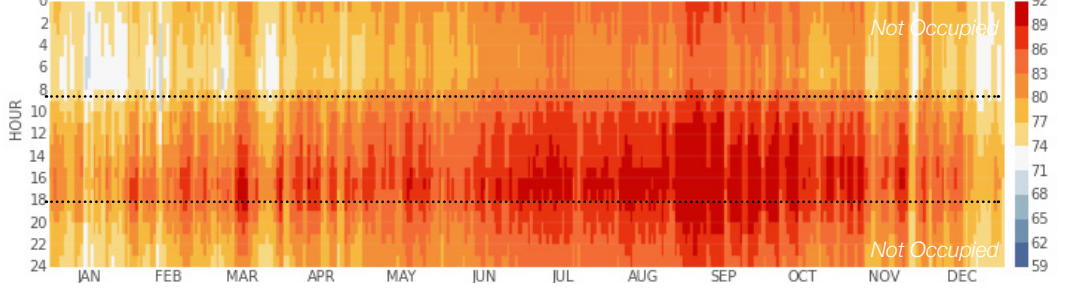
Operative temperature for bottom floor



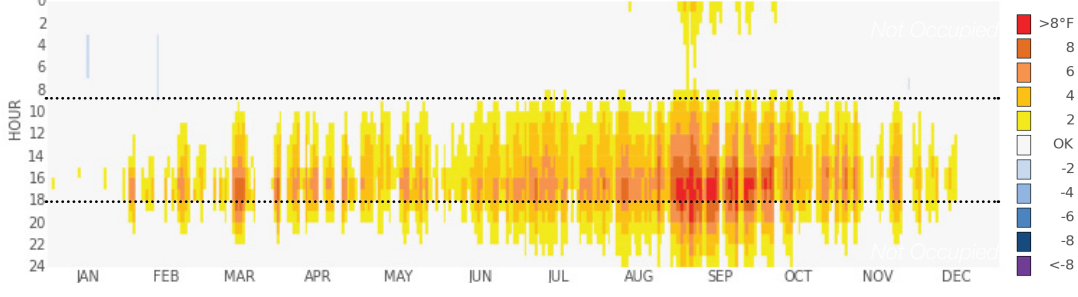
Degrees from comfort for bottom floor



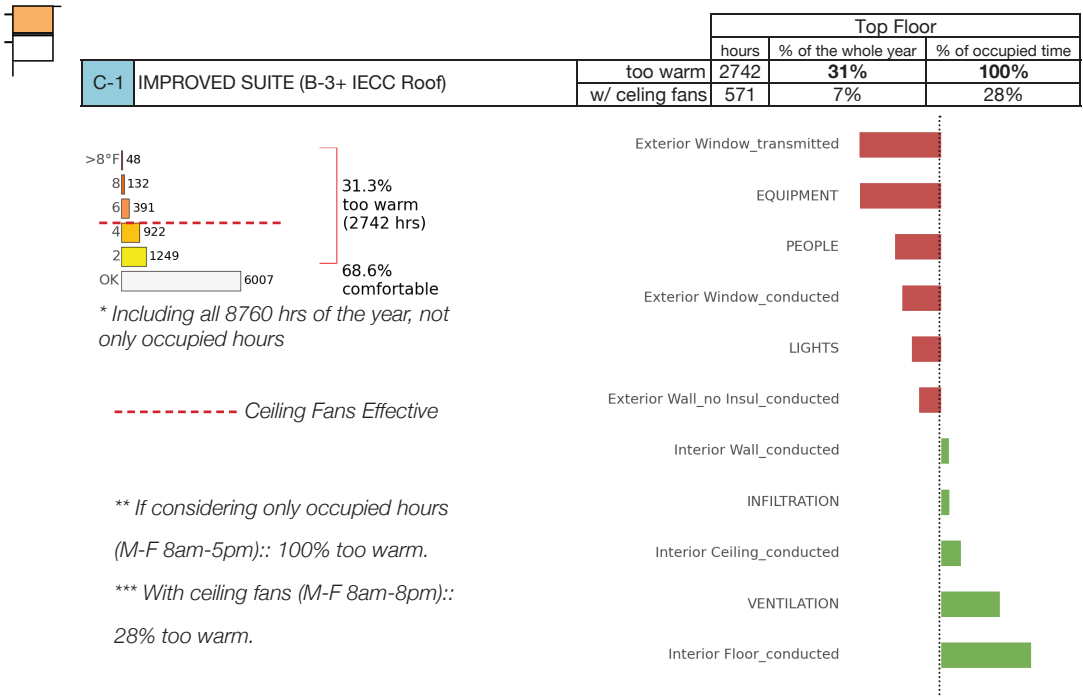
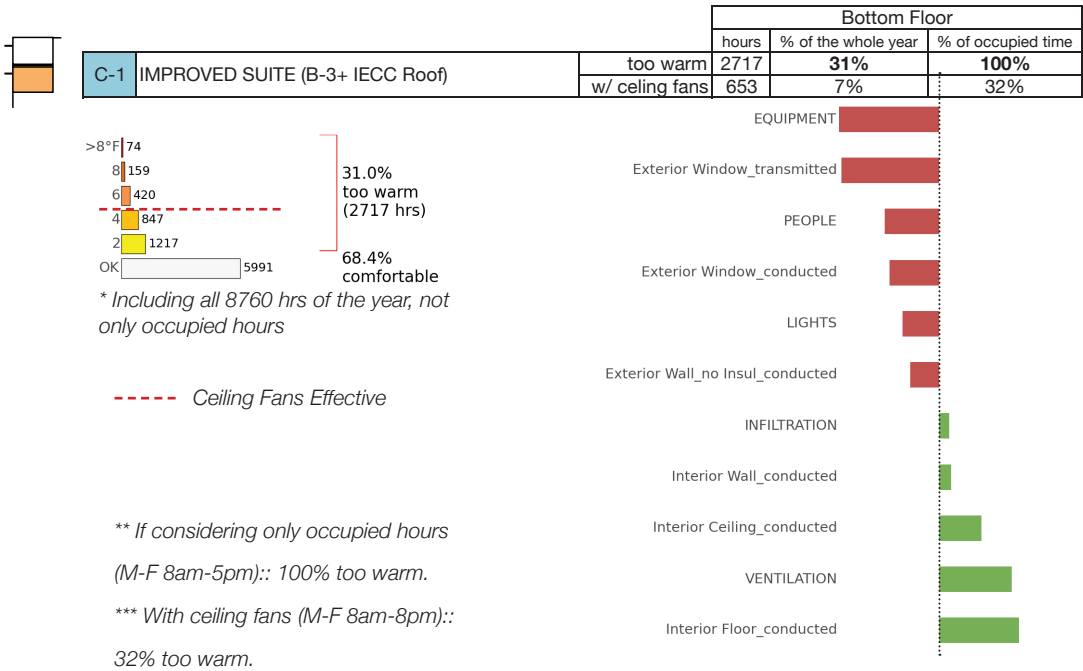
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.d.3 Office Analysis:: West Facing (Continued)



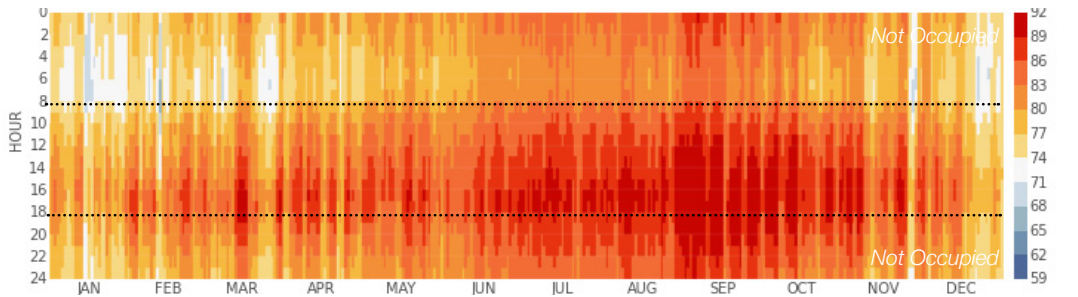
Add/C.4.d OFFICE ANALYSIS:: WEST FACING

C.4.d.4. CODE SUITE

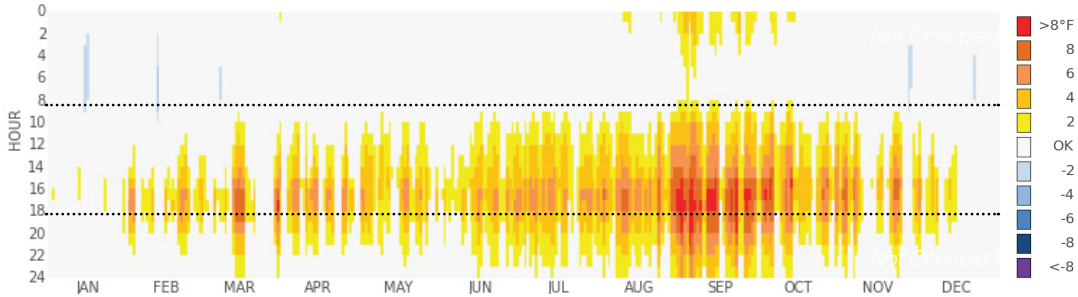
Equal to IMPROVED SUITE + IECC Walls



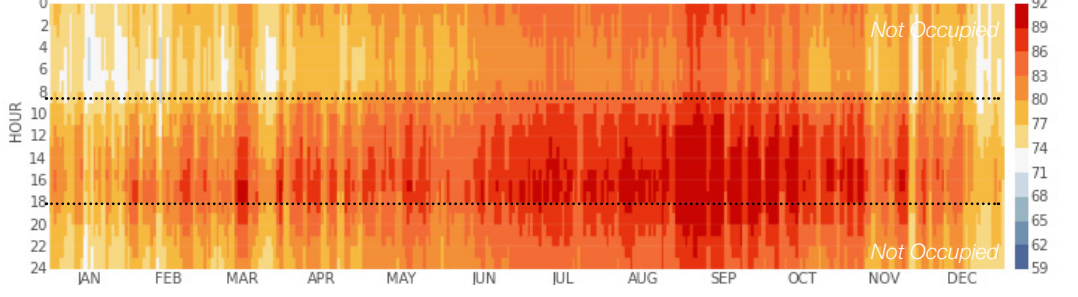
Operative temperature for bottom floor



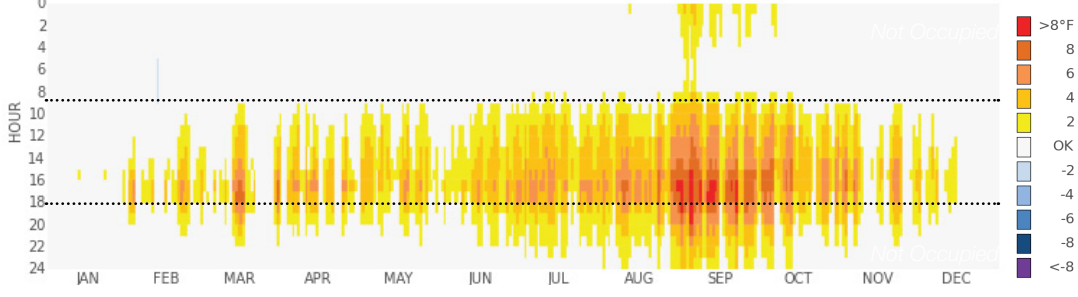
Degrees from comfort for bottom floor



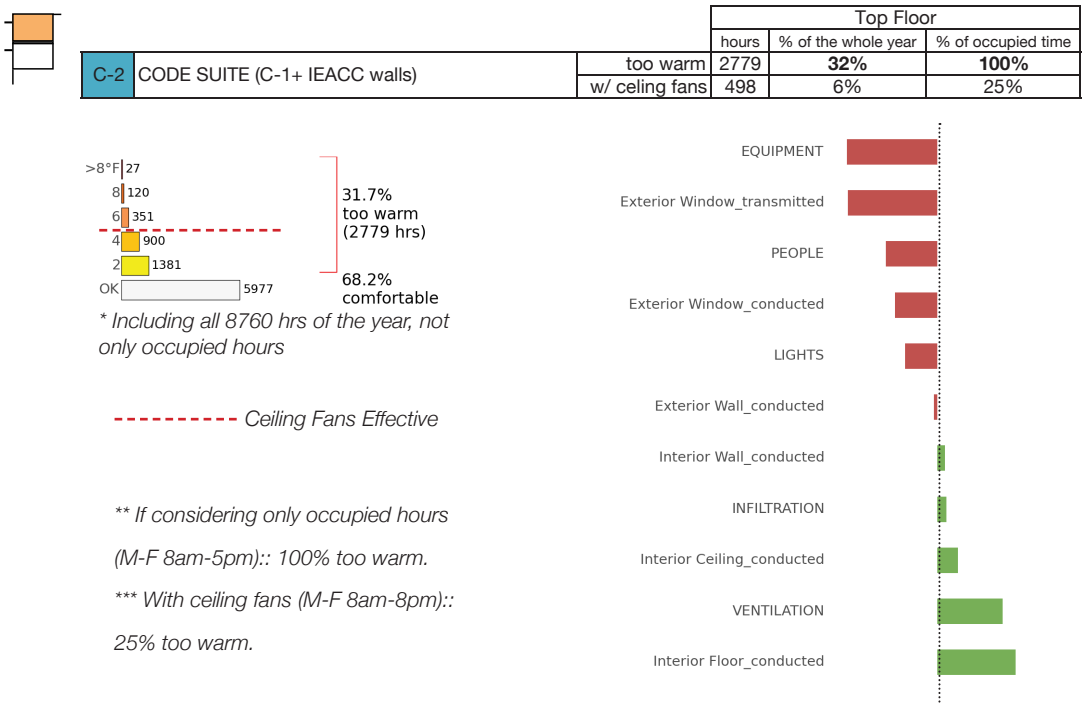
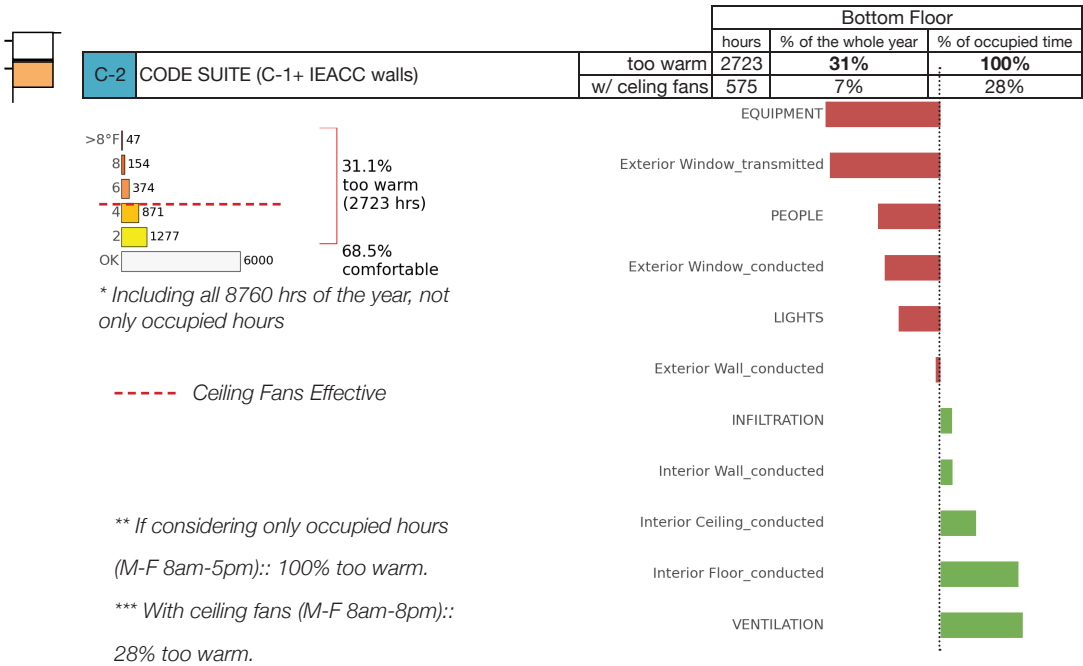
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.d.4 Office Analysis:: West Facing (Continued)



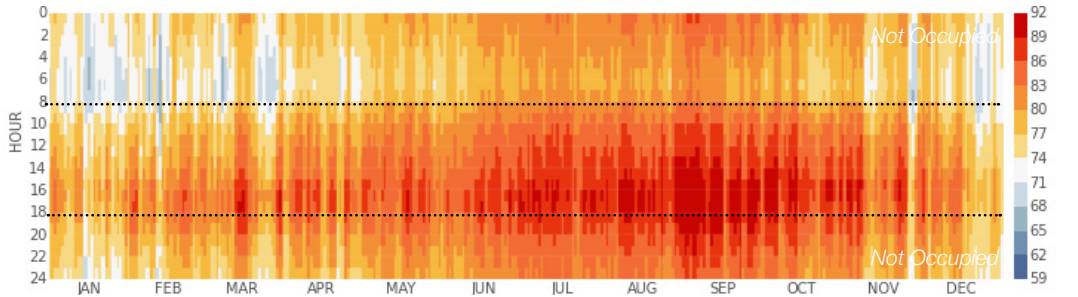
Add/C.4.d OFFICE ANALYSIS:: WEST FACING

C.4.d.5. IMPROVED SUITE WITH VENTILATION

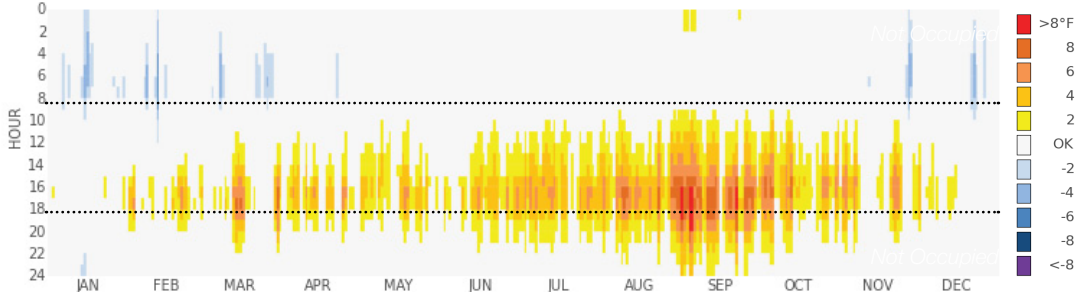
Equal to MPROVED SUITE +2ACH



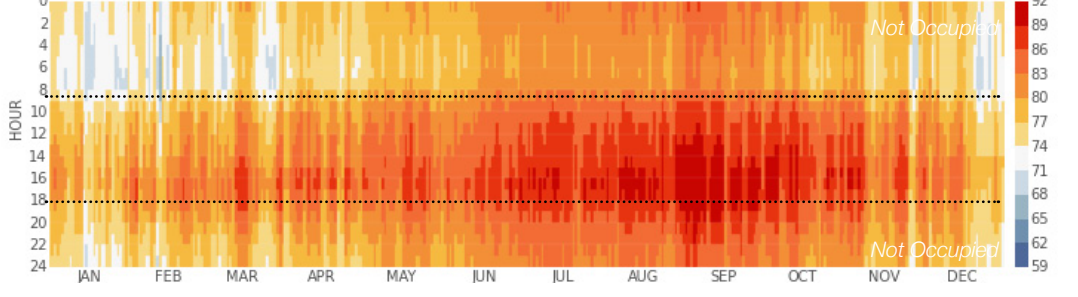
Operative temperature for bottom floor



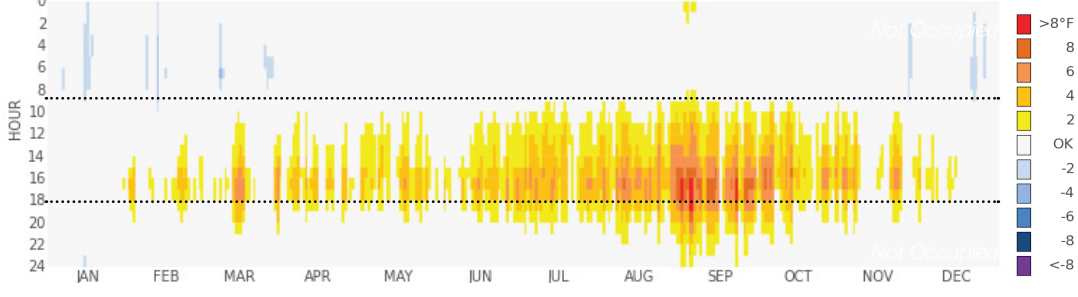
Degrees from comfort for bottom floor



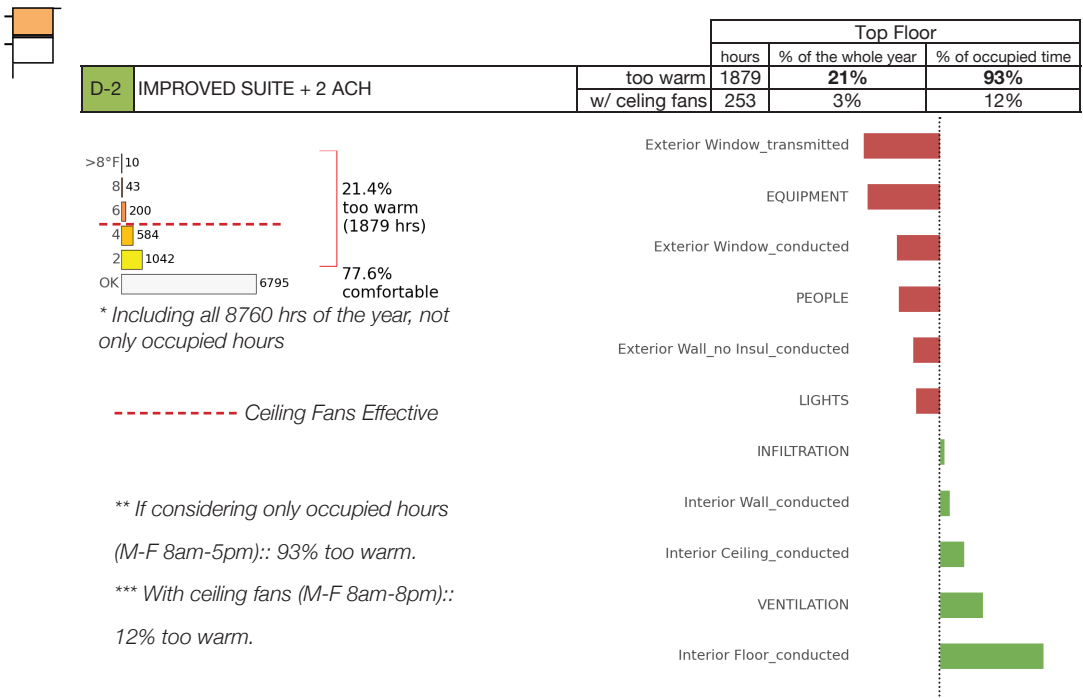
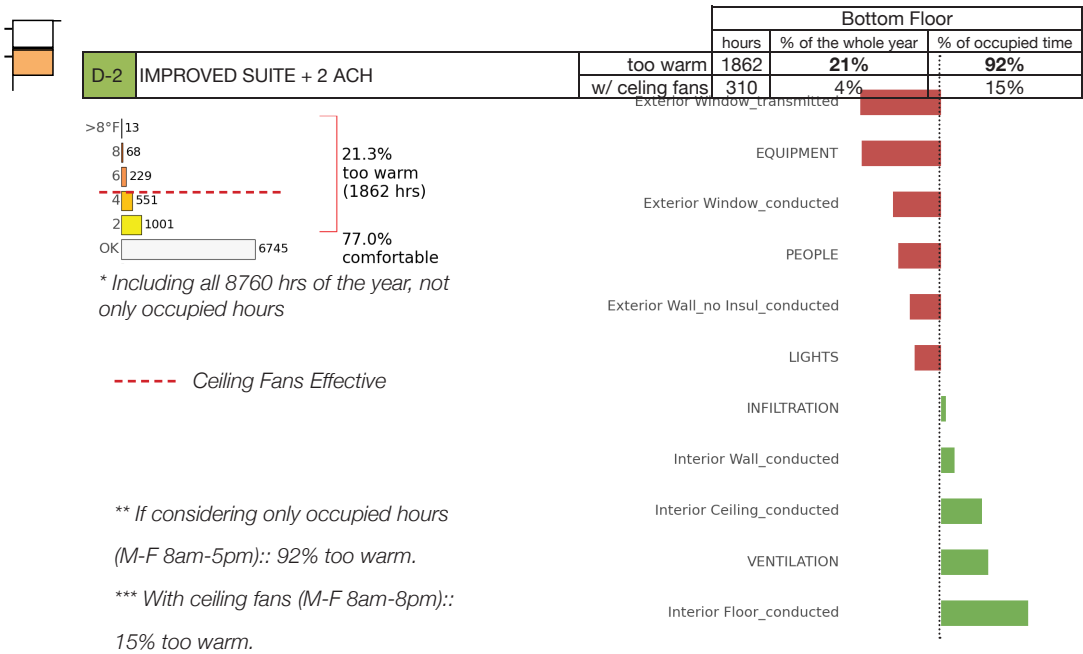
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.d.5 Office Analysis:: West Facing (Continued)



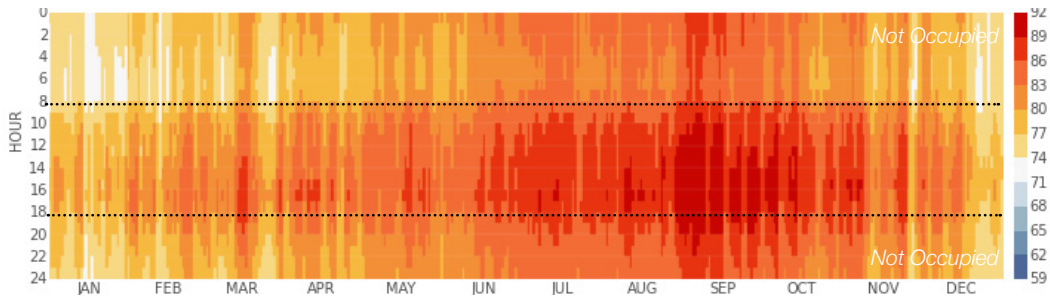
Add/C.4.d OFFICE ANALYSIS:: WEST FACING

C.4.d.6. IDEAL SUITE

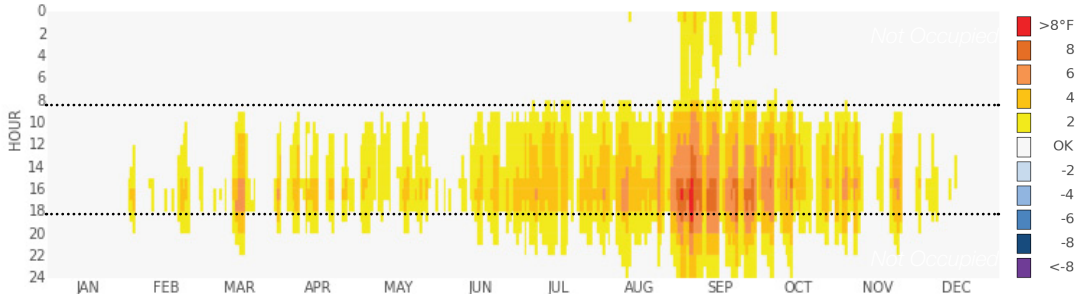
Equal to CODE SUITE + Thermal Mass



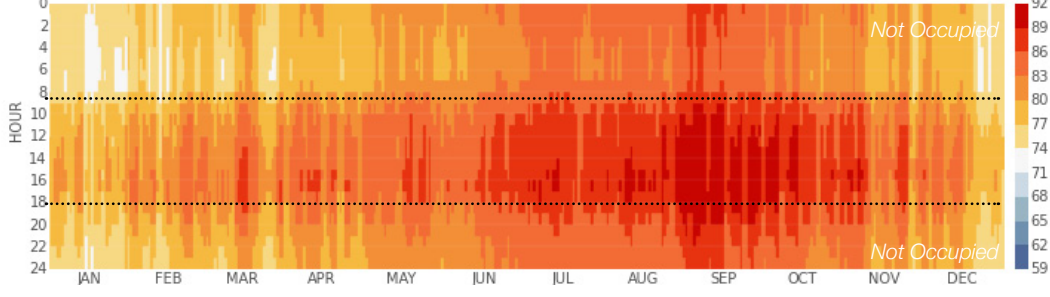
Operative temperature for bottom floor



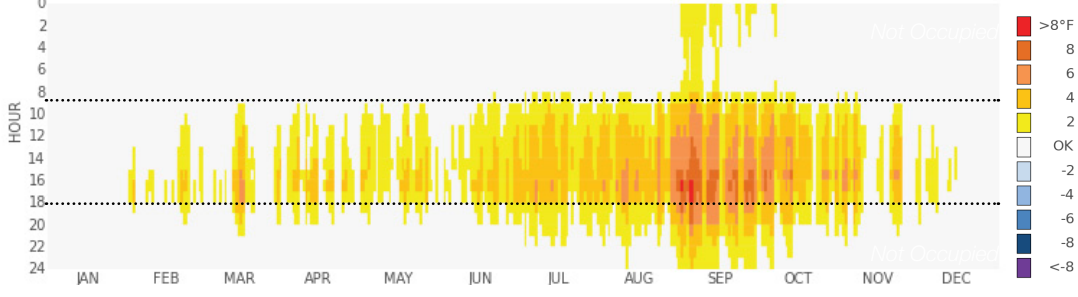
Degrees from comfort for bottom floor



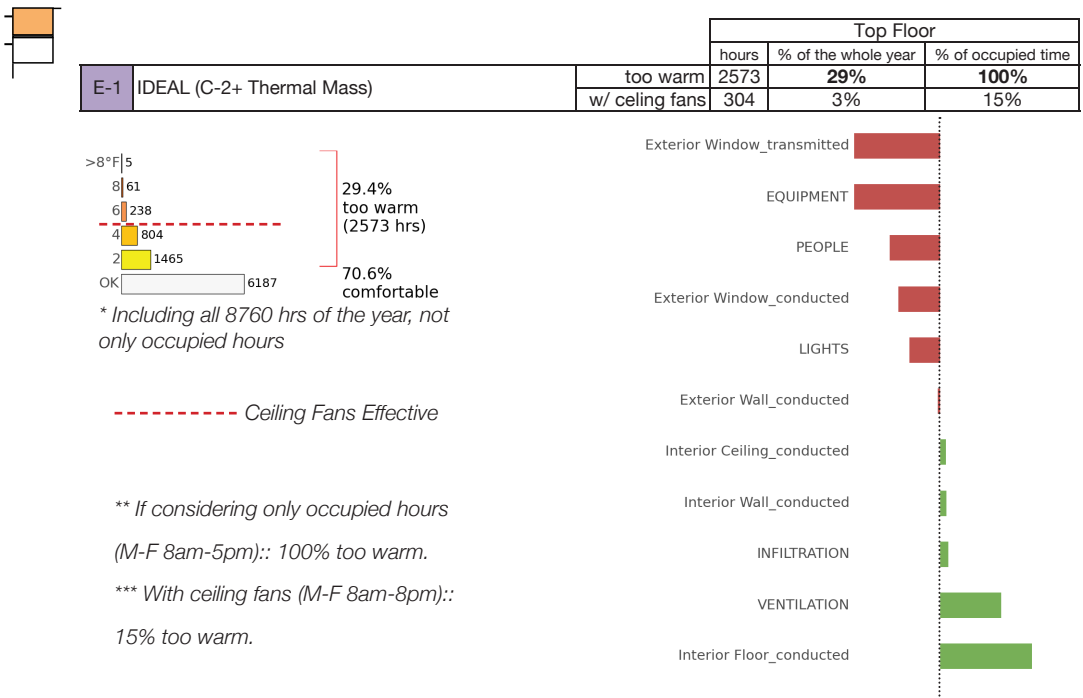
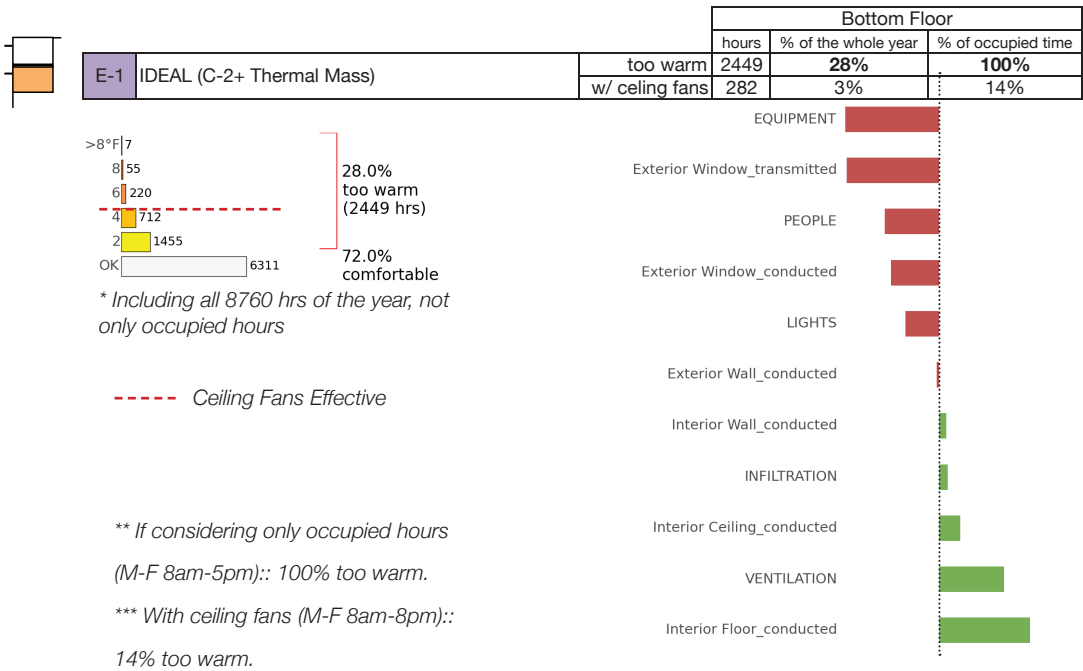
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.d.6 Office Analysis:: West Facing (Continued)



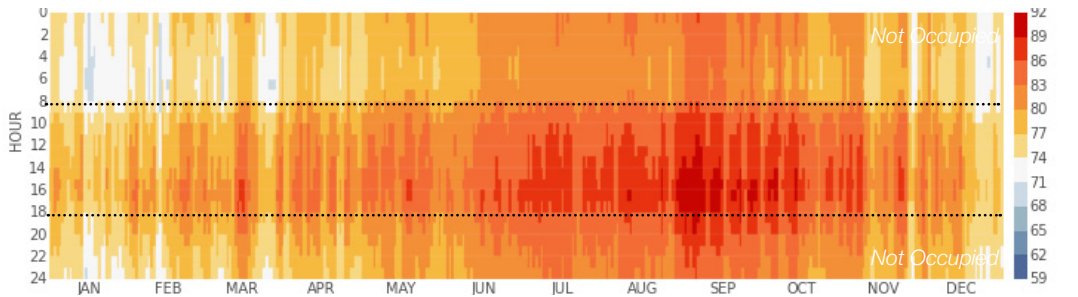
Add/C.4.d OFFICE ANALYSIS:: WEST FACING

C.4.d.7. IDEAL SUITE WITH VENTILATION

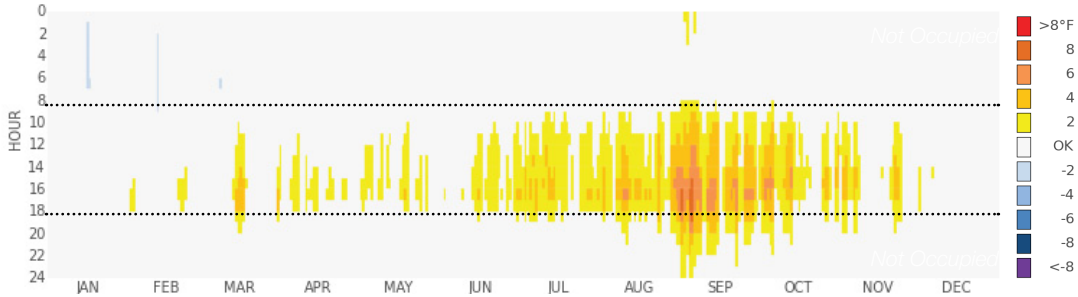
Equal to IDEAL SUITE + 2ACH



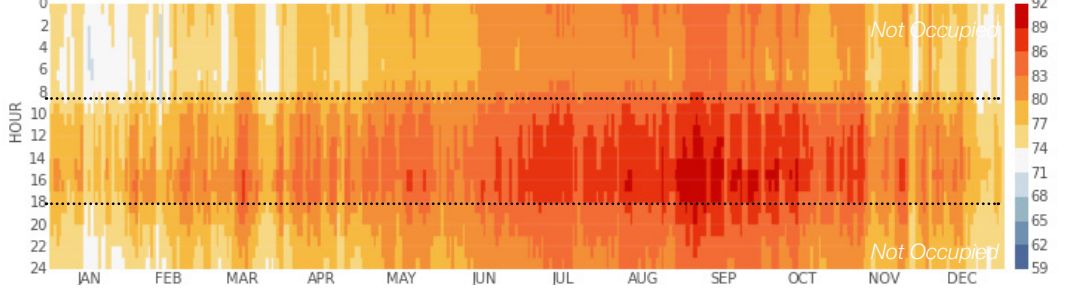
Operative temperature for bottom floor



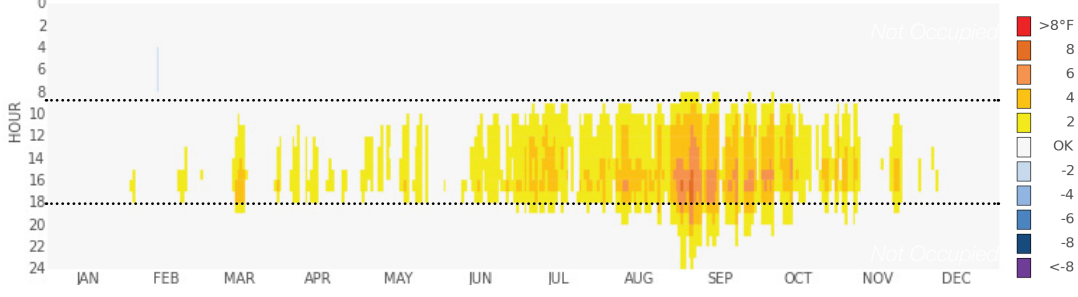
Degrees from comfort for bottom floor



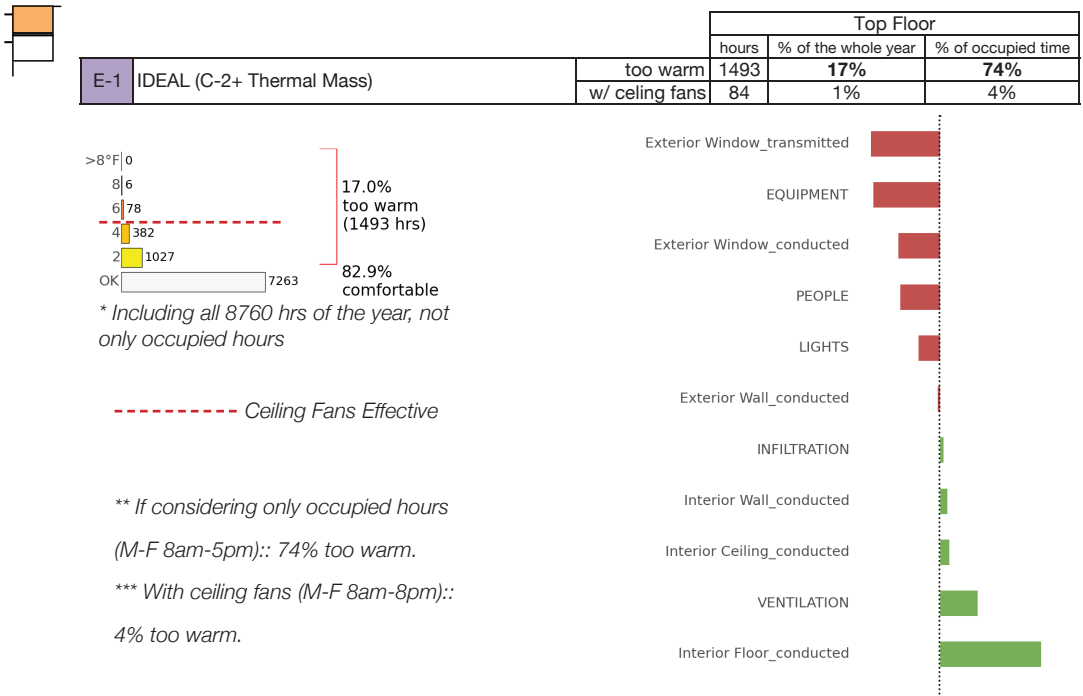
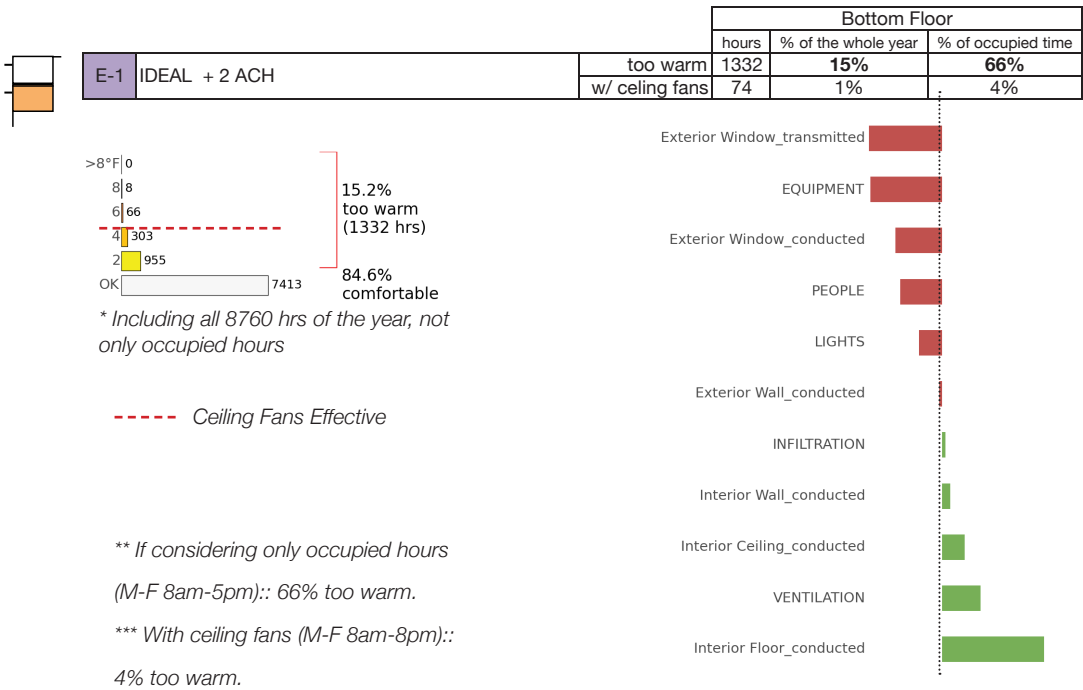
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.4.d.7 Office Analysis:: West Facing (Continued)



Add.3/C. HVAC AUTONOMY AND THERMAL COMFORT STUDIES**5. LABORATORY ANALYSIS**

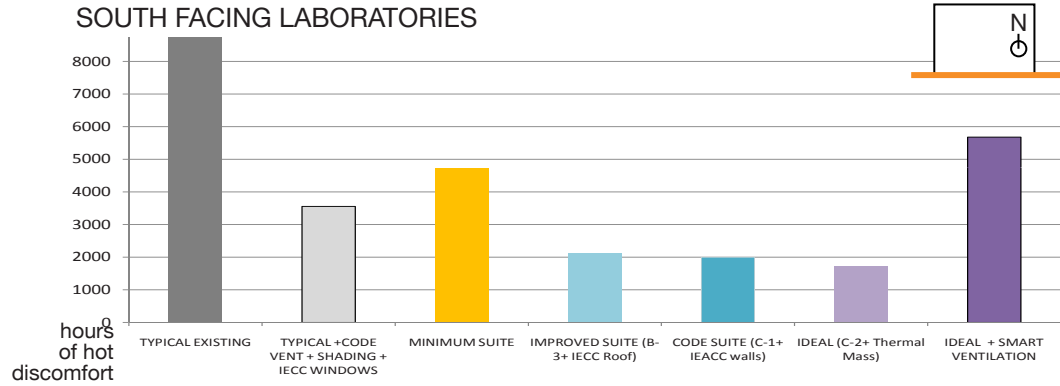
a. FOR SOUTH ORIENTATION

0. **TYPICAL EXISTING**:: No Insulation in Opaque Surfaces, Single Pane Glass Windows
1. TYPICAL + 1ACH + Shading + IECC Glazing + Code Ventilation
2. **MINIMUM SUITE**:: TYPICAL + IECC Glazing + Shading + Optimized Lighting and Equipment
3. **IMPROVED SUITE**:: Minimum Suite + IECC Roof
4. **CODE SUITE**:: Improved Suite + IECC Walls
5. **IDEAL SUITE**:: Code Suite + Thermal Mass
6. IDEAL SUITE + VENTILATION PARAMETRICS
7. IDEAL SUITE + SMART VENTILATION

b. FOR NORTH ORIENTATION

0. **TYPICAL EXISTING**:: No Insulation in Opaque Surfaces, Single Pane Glass Windows
1. TYPICAL + 1ACH + Shading + IECC Glazing
2. **MINIMUM SUITE**:: TYPICAL + 1ACH + IECC Glazing + Shading + Optimized Lighting and Equipment
3. **IMPROVED SUITE**:: Minimum Suite + IECC Roof
4. **CODE SUITE**:: Improved Suite + IECC Walls
5. **IDEAL SUITE**:: Code Suite + Thermal Mass
6. IDEAL SUITE + SMART VENTILATION

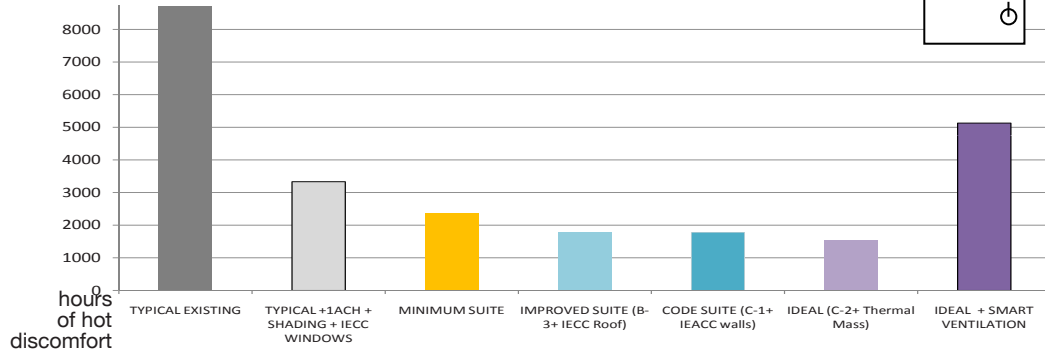
Add/C.5 Laboratory Analysis (Continued)



Scenario	Status	Bottom Floor			Top Floor		
		hours	% of the whole year	% of occupied time	hours	% of the whole year	% of occupied time
TYPICAL EXISTING	too warm	8760	100%	100%	8760	100%	100%
A-3 TYPICAL + CODE VENT + SHADING + IECC WINDOWS	too warm	3422	39%	100%	3558	41%	100%
B-3 MINIMUM SUITE	too warm	2154	25%	80%	2612	30%	97%
C-1 IMPROVED SUITE (B-3+ IECC Roof)	too warm	2140	24%	79%	2116	24%	78%
C-2 CODE SUITE (C-1+ IEACC walls)	too warm	2012	23%	75%	1991	23%	74%
E-1 IDEAL (C-2+ Thermal Mass)	too warm	1653	19%	61%	1733	20%	64%
E-2 IDEAL + SMART VENTILATION	too warm	5684	65%	100%	5682	65%	100%

Add/C.5 Laboratory Analysis (Continued)

NORTH FACING LABORATORIES



Scenario	w/ ceiling fans	Bottom Floor			Top Floor		
		hours	% of the whole year	% of occupied time	hours	% of the whole year	% of occupied time
TYPICAL EXISTING	too warm	6863	78%	100%	6181	71%	100%
	w/ ceiling fans	3001	57%	100%	4365	50%	100%
A-3 TYPICAL +1ACH + SHADING + IECC WINDOWS	too warm	3026	35%	100%	3458	39%	100%
	w/ ceiling fans	1077	12%	53%	1792	20%	88%
B-3 MINIMUM SUITE	too warm	2007	23%	99%	2850	33%	100%
	w/ ceiling fans	169	2%	8%	1162	13%	57%
C-1 IMPROVED SUITE (B-3+ IECC Roof)	too warm	1814	21%	90%	1835	21%	91%
	w/ ceiling fans	122	1%	6%	172	2%	8%
C-2 CODE SUITE (C-1+ IEACC walls)	too warm	1881	21%	93%	1949	22%	96%
	w/ ceiling fans	149	2%	7%	120	1%	6%
D-2 IMPROVED SUITE + 2 ACH	too warm	1175	13%	58%	1217	14%	60%
	w/ ceiling fans	29	0%	1%	17	0%	1%
E-1 IDEAL (C-2+ Thermal Mass)	too warm	1462	17%	72%	1653	19%	82%
	w/ ceiling fans	32	0%	2%	40	0%	2%
E-1 IDEAL + 2 ACH	too warm	728	8%	36%	934	11%	46%
	w/ ceiling fans	0	0%	0%	0	0%	0%

Add/C.5.a. LABORATORY ANALYSIS:: SOUTH FACING

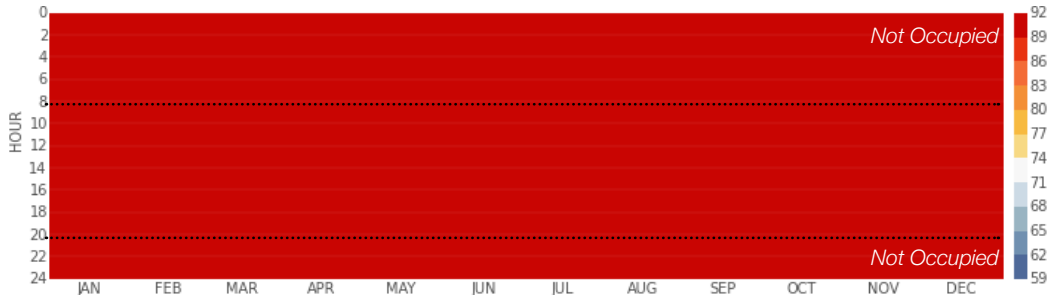
C.5.a.0. TYPICAL EXISTING CONDITIONS



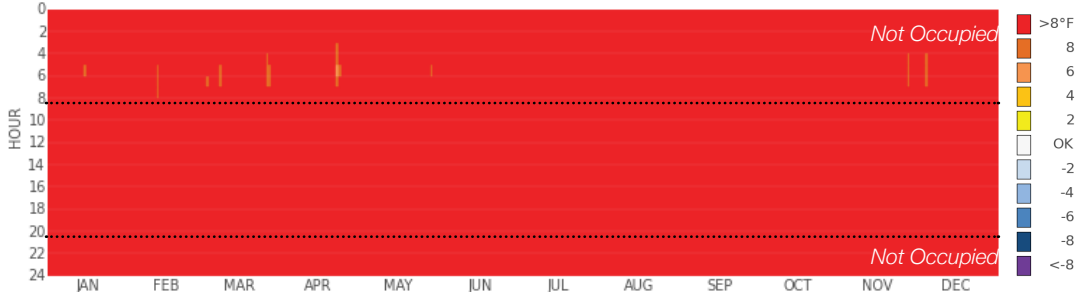
No Insulation in Opaque Surfaces and Single Pane Glass



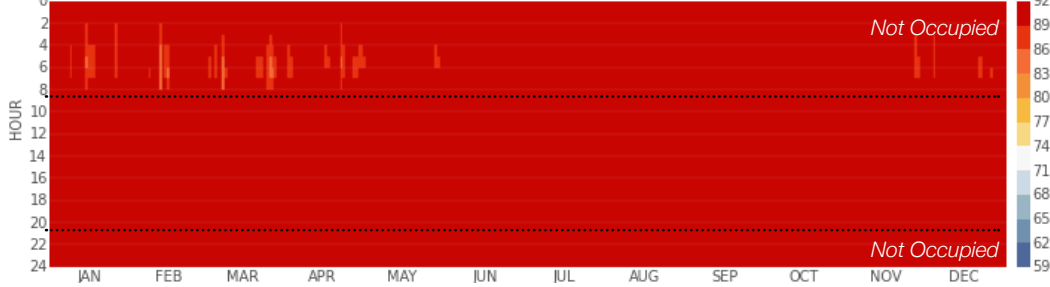
Operative temperature for bottom floor



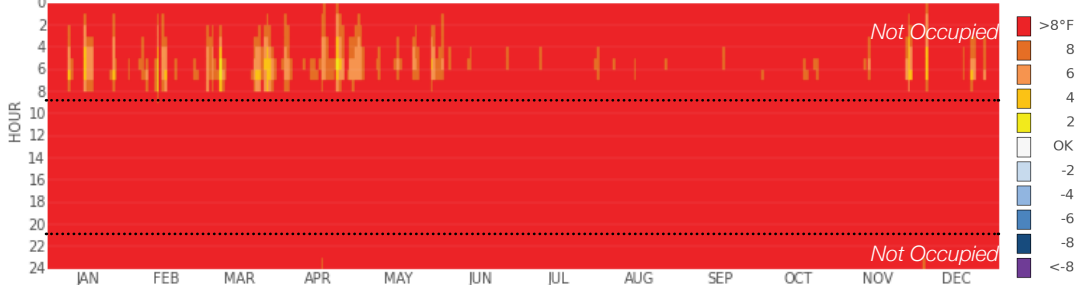
Degrees from comfort for bottom floor



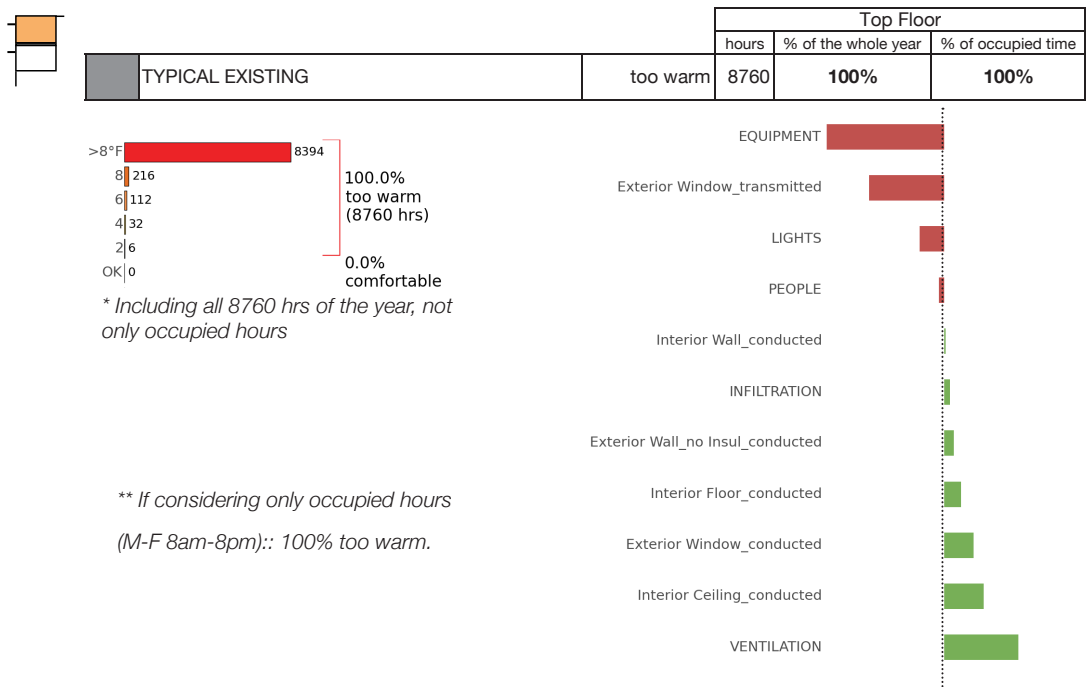
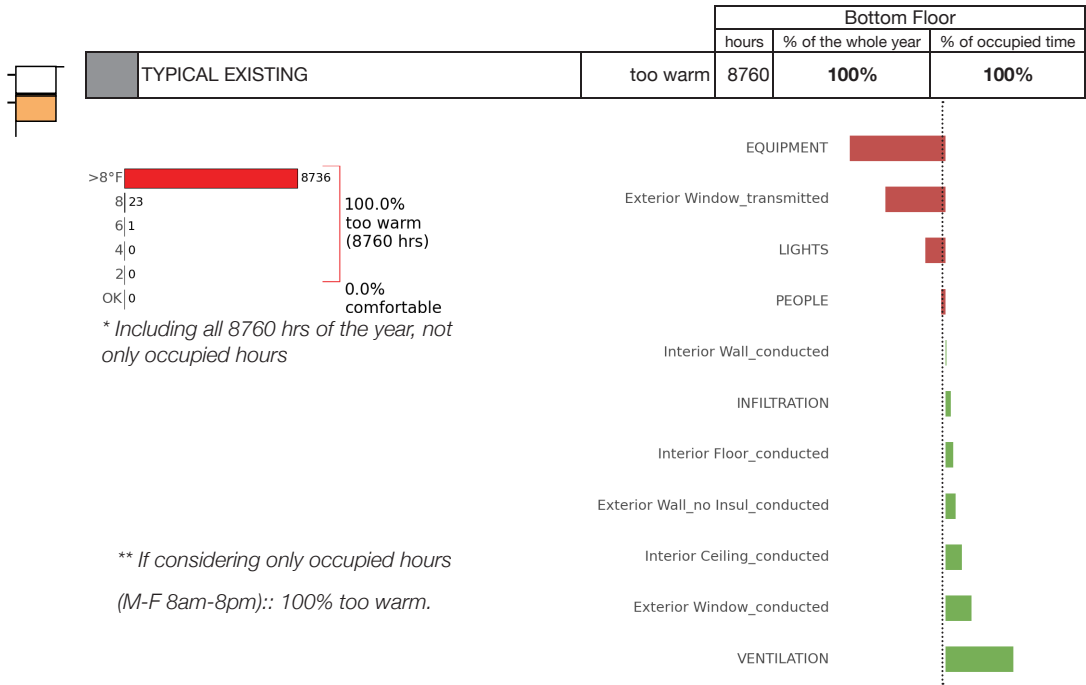
Operative temperature for top floor



Degrees from comfort for top floor

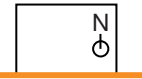


Add/C.5.a.0 Laboratory Analysis:: South Facing (Continued)

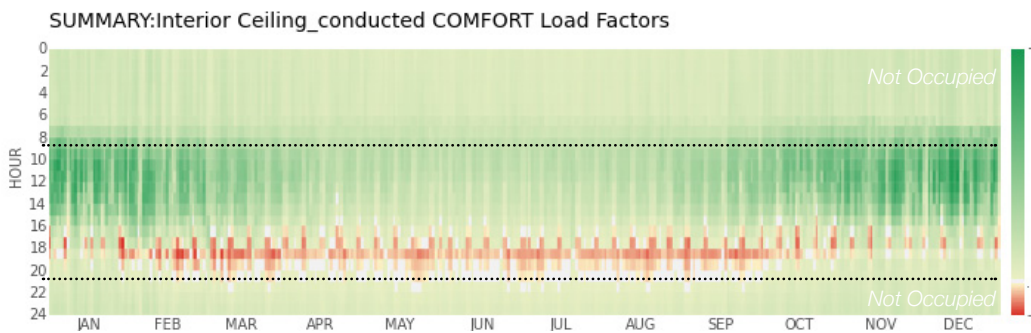
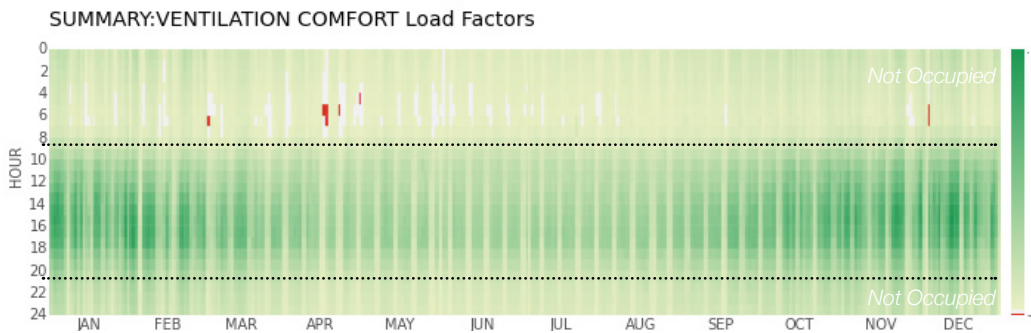
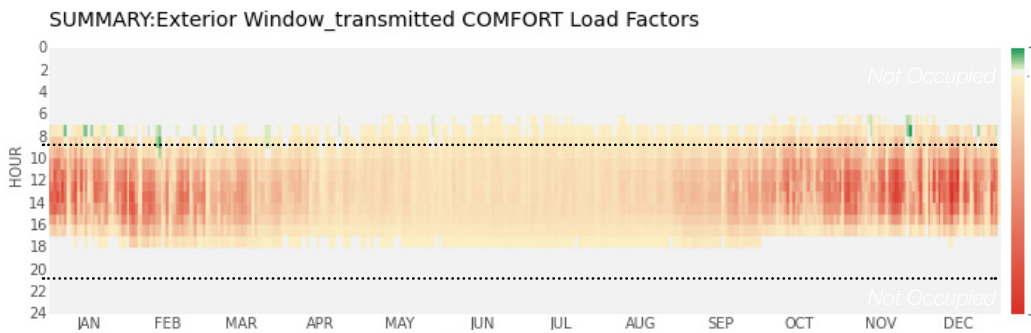
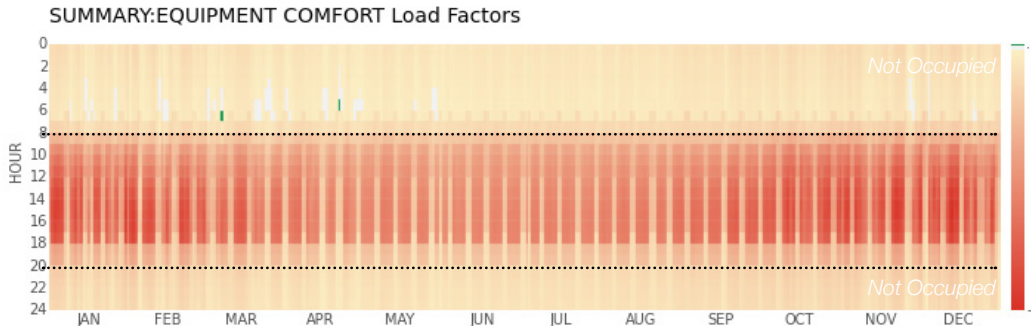


Add/C.5.a. LABORATORY ANALYSIS:: SOUTH FACING

TYPICAL EXISTING CONDITIONS:: Comfort Load Factors



No Insulation in Opaque Surfaces and Single Pane Glass



Add/C.5.a.0 Laboratory Analysis:: South Facing (Continued)

In order to provide more detailed information about what is affecting comfort, we analyzed the heat flows into and out of the spaces, as well as the difference between the space temperatures and the ideal space temperature (adaptive comfort range). We compared these space loads to the ideal temperature difference to determine which loads are improving comfort and which loads are decreasing comfort. The comfort load factors indicate the degree to which a particular load is pushing the temperature of a space towards the middle of the comfort zone or away from it.

In summary, the factors associated with decreased comfort in this analysis are the solar radiation through the windows and the internal loads (heat released to the space mostly by the equipment but also lighting).

This analysis also indicates that ventilation and thermal mass (interior ceiling and floor conduction) are improving building thermal performance and thus improving comfort and reducing future HVAC loads. On the one hand, by introducing outside air when heat is building up in the space due to high internal loads or solar radiation, interior spaces can prevent overheating. On the other hand, the thermal mass in the ceiling contributes to Achievingcomfort conditions by absorbing heat during the day and releasing it at night.

The graphs on the left show the times of the year when each load factor either decreases or increases comfort. For example, the solar transmitted radiation never increases comfort and decreases comfort the most during the fall and winter seasons, which is likely when the lower sun angles hit the windows for longer periods of time.

The internal heat coming from the equipment always decreases comfort while ventilation always increases comfort. The interior ceiling increases comfort during most of the occupied times, even if it decreases comfort during the late afternoons. This is likely due to the floors not being able to absorb any more internal heat and starting to release it into the space even if that further increases the interior temperature.

Add/C.5.a. LABORATORY ANALYSIS:: SOUTH FACING

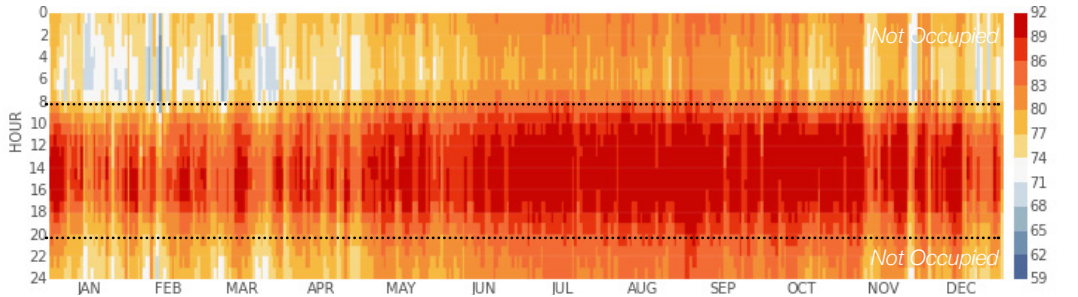
C.5.a.1.TYPICAL WINDOW IMPROVEMENTS



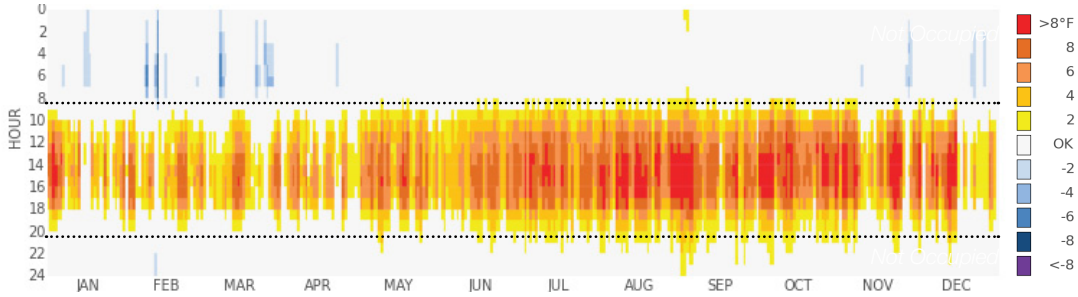
Equal to TYPICAL + 1ACH + Shading + IECC 2015 Windows + Code Ventilation



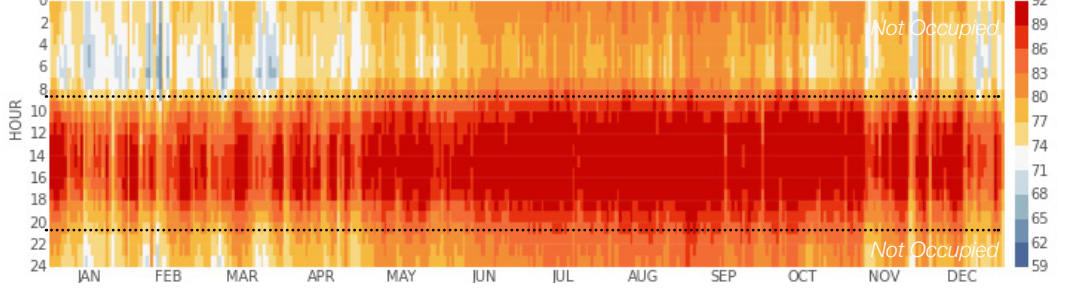
Operative temperature for bottom floor



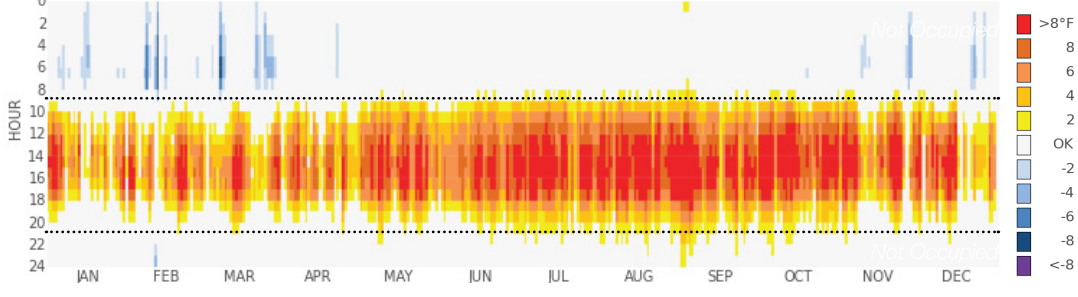
Degrees from comfort for bottom floor



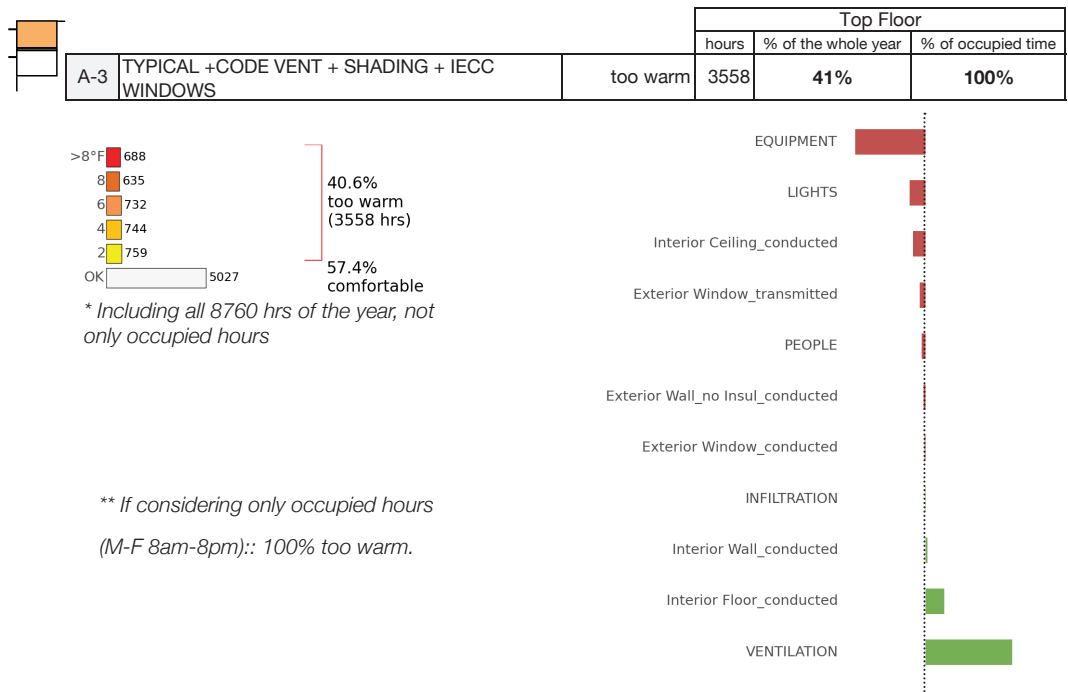
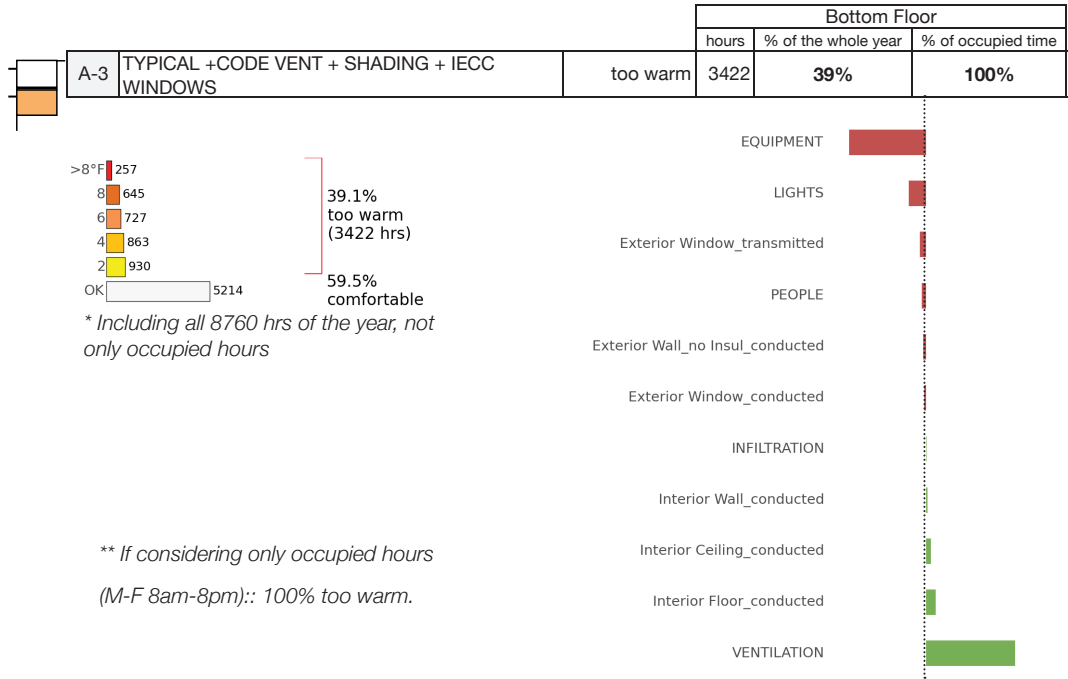
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.5.a.1 Laboratory Analysis:: South Facing (Continued)



Add/C.5.a. LABORATORY ANALYSIS:: SOUTH FACING

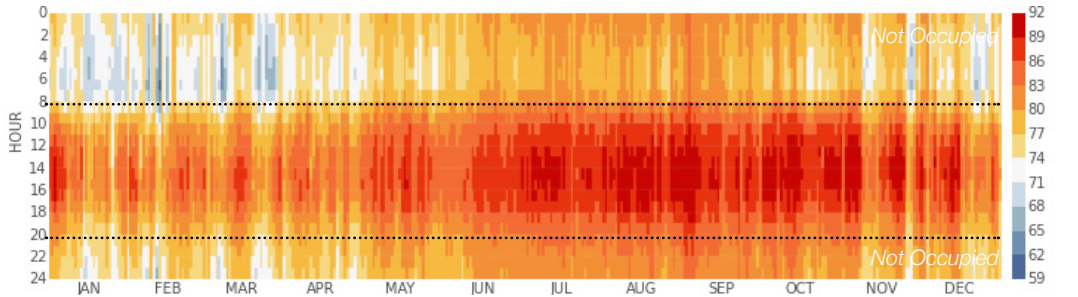
C.5.a.2. MINIMUM SUITE



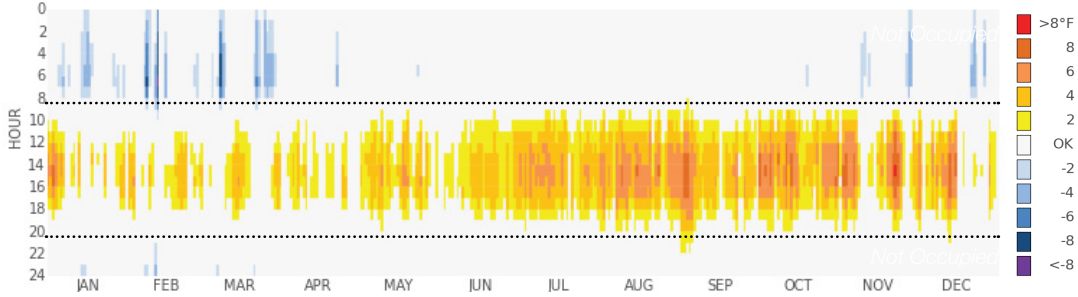
Equal to TYPICAL + IECC Windows + Shading +Optimized Lighting and Equipment



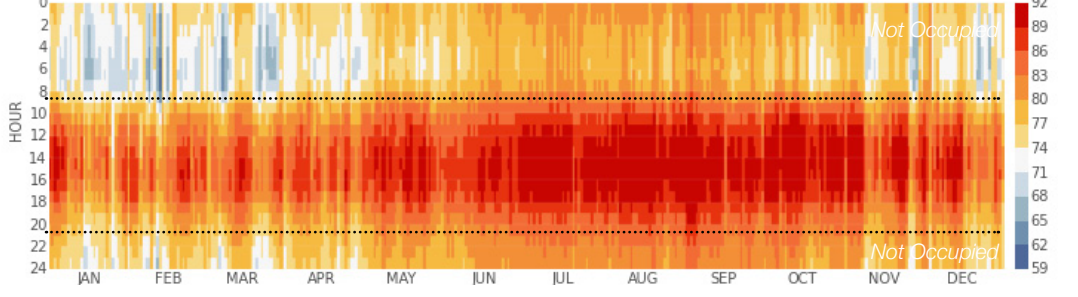
Operative temperature for bottom floor



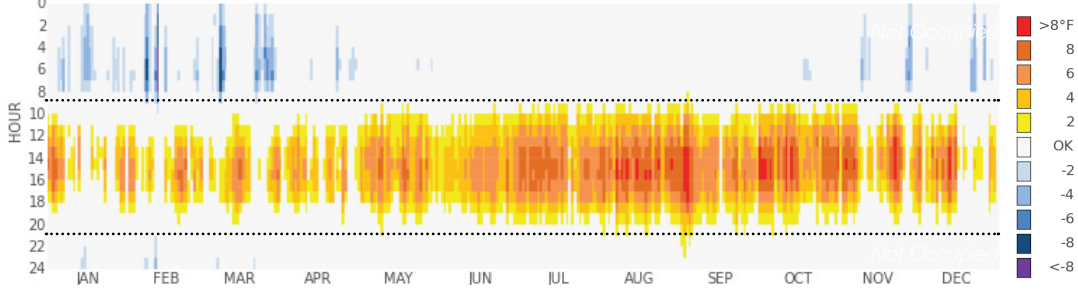
Degrees from comfort for bottom floor



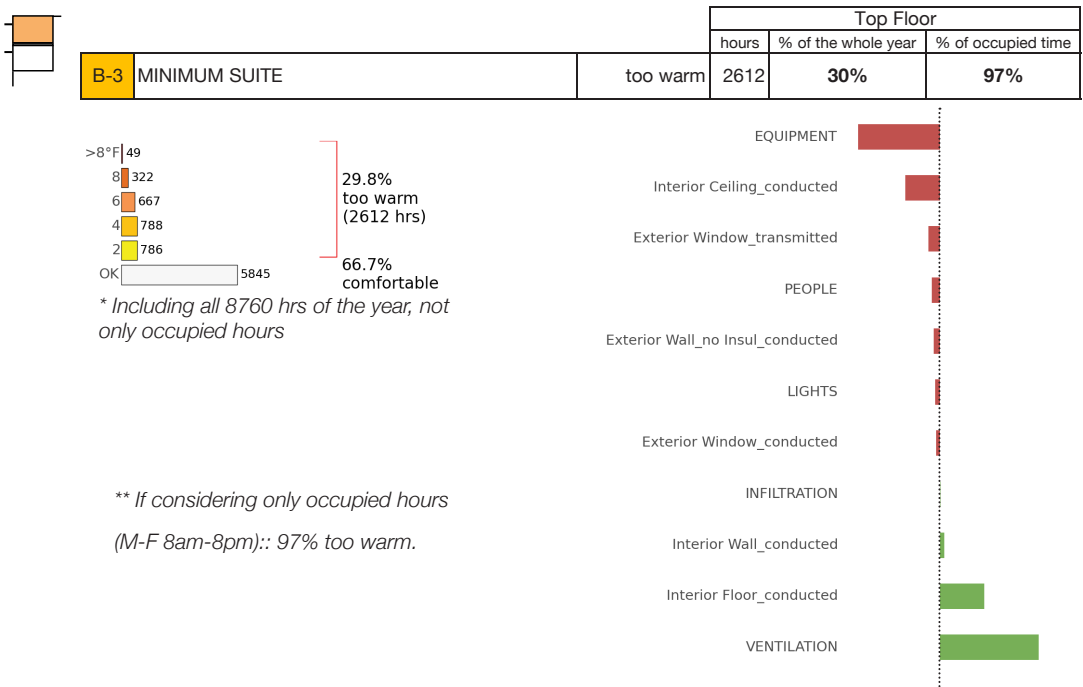
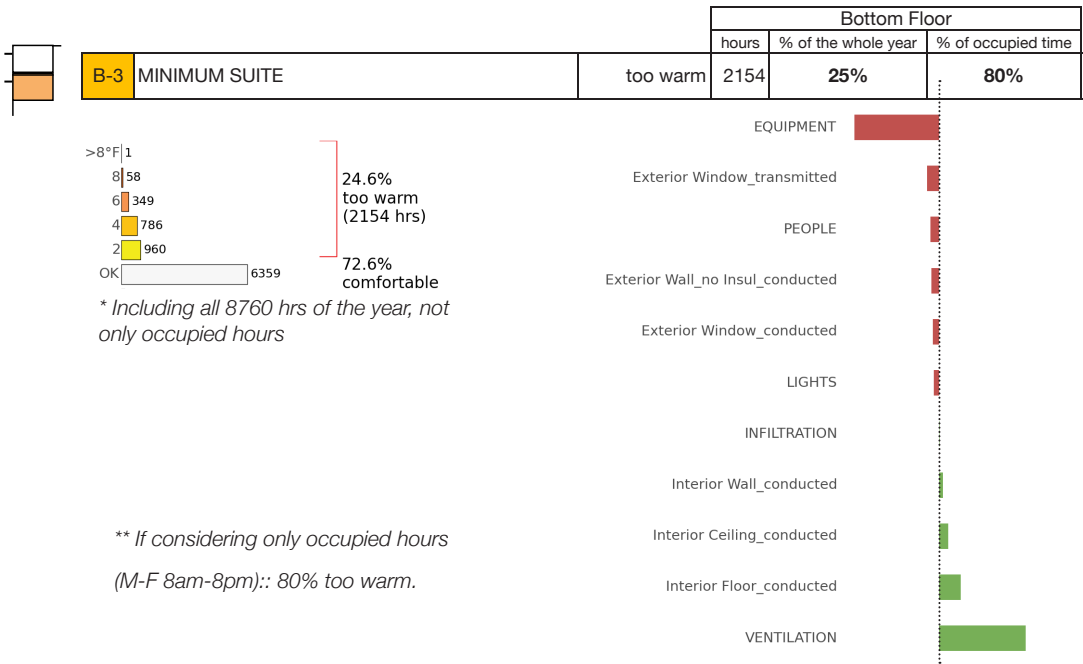
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.5.a.2 Laboratory Analysis:: South Facing (Continued)



Add/C.5.a. LABORATORY ANALYSIS:: SOUTH FACING

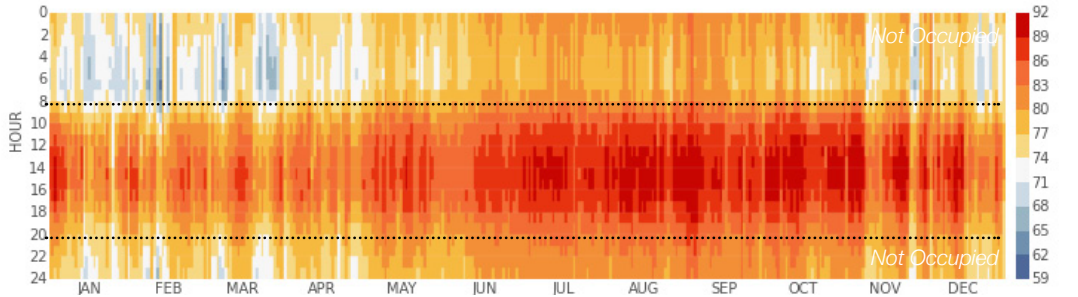
C.5.a.3. IMPROVED SUITE



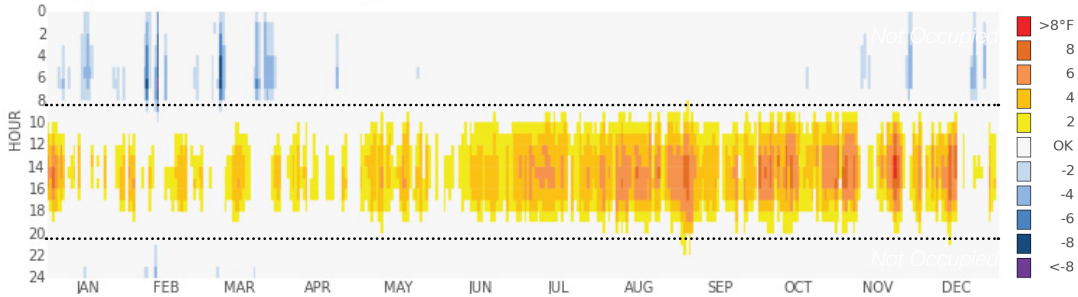
Equal to MINIMUM SUITE + IECC Roof



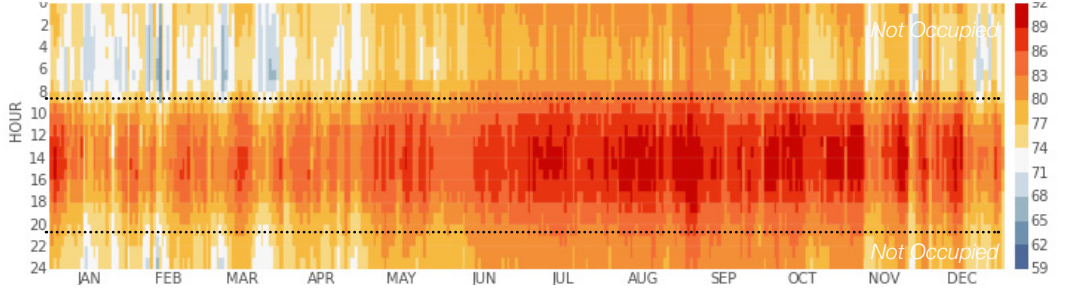
Operative temperature for bottom floor



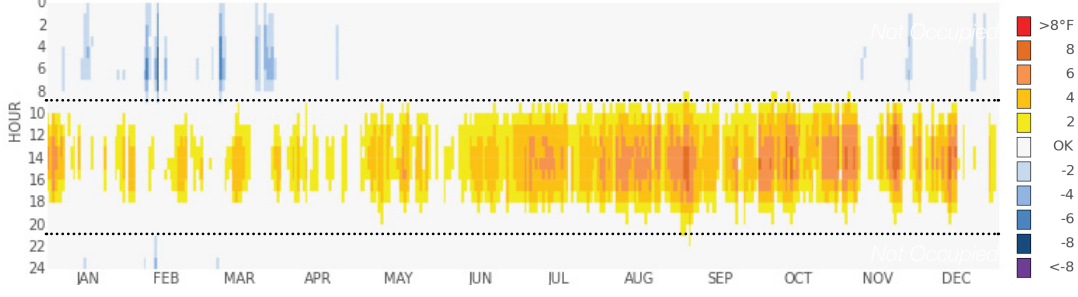
Degrees from comfort for bottom floor



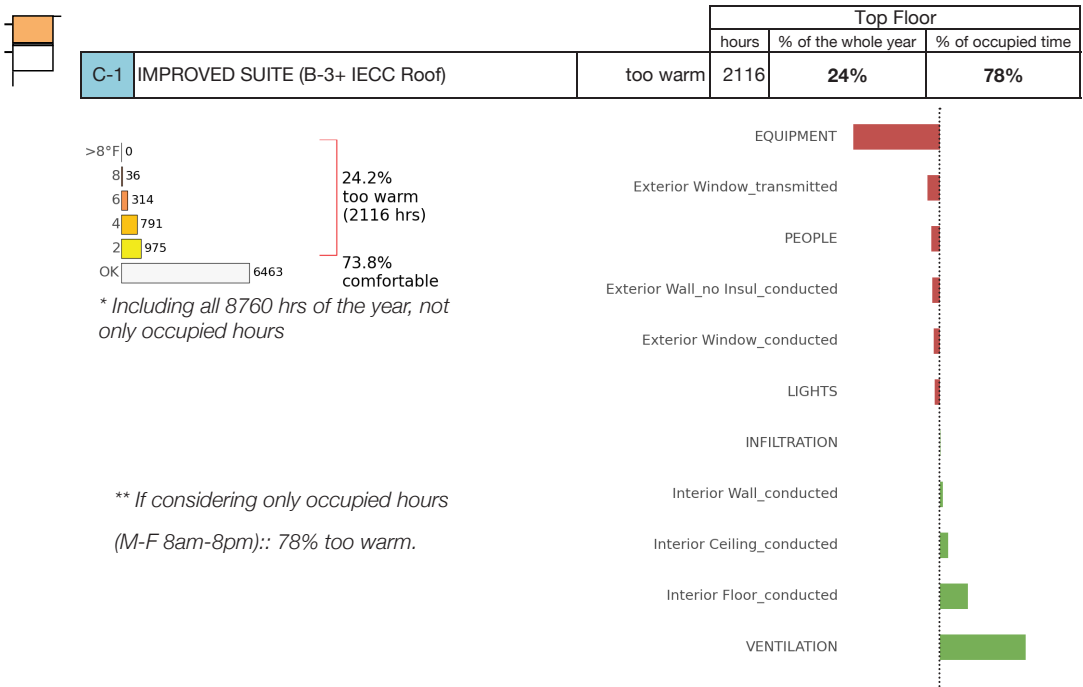
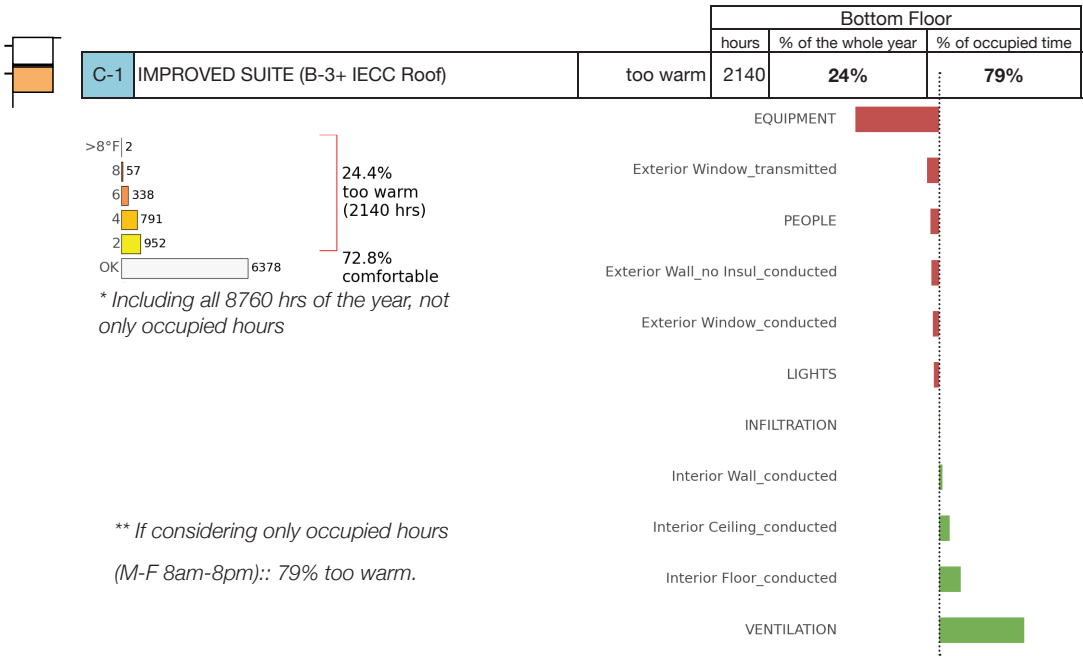
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.5.a.3 Laboratory Analysis:: South Facing (Continued)



Add/C.5.a. LABORATORY ANALYSIS:: SOUTH FACING

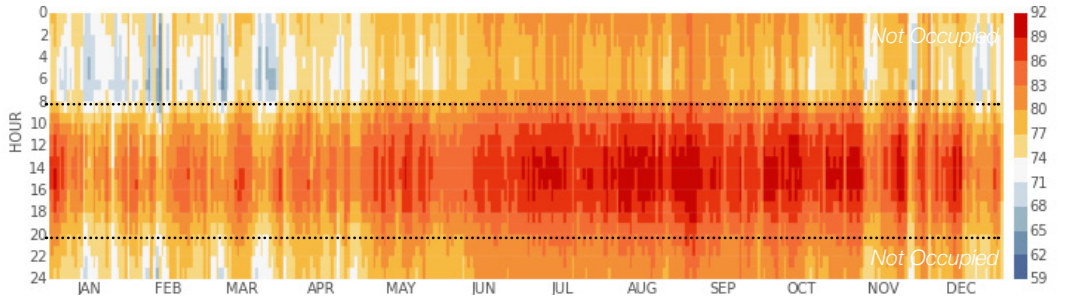
C.5.a.4. CODE SUITE



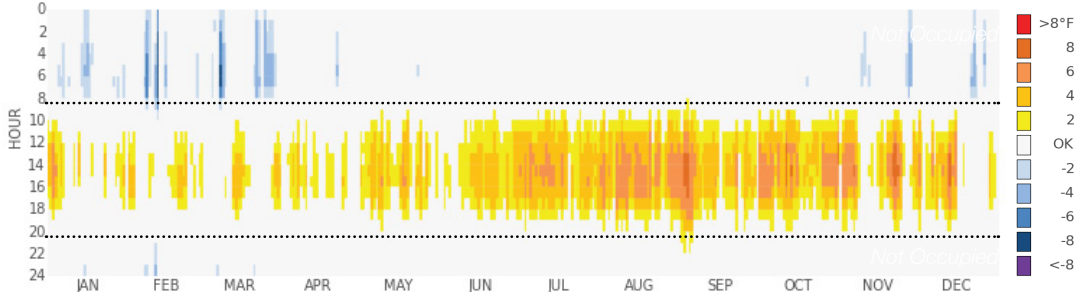
Equal to IMPROVED SUITE + IECC Walls



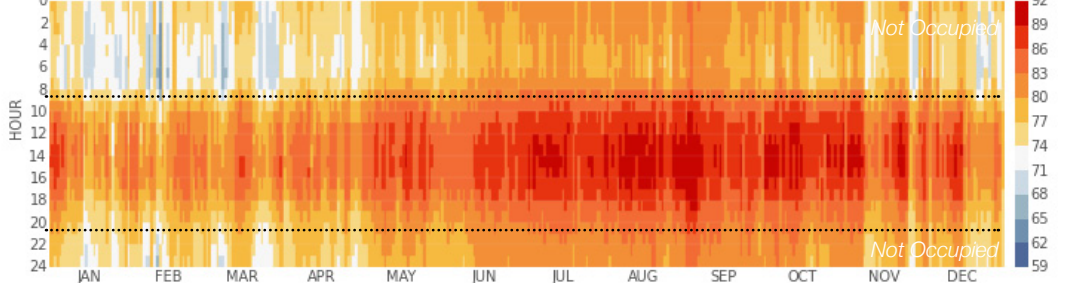
Operative temperature for bottom floor



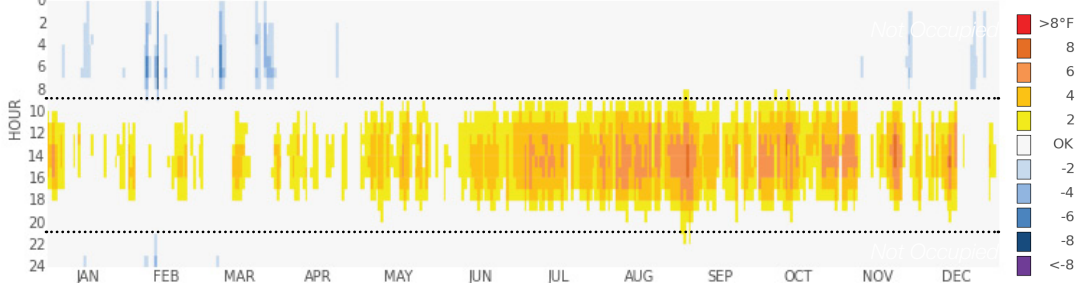
Degrees from comfort for bottom floor



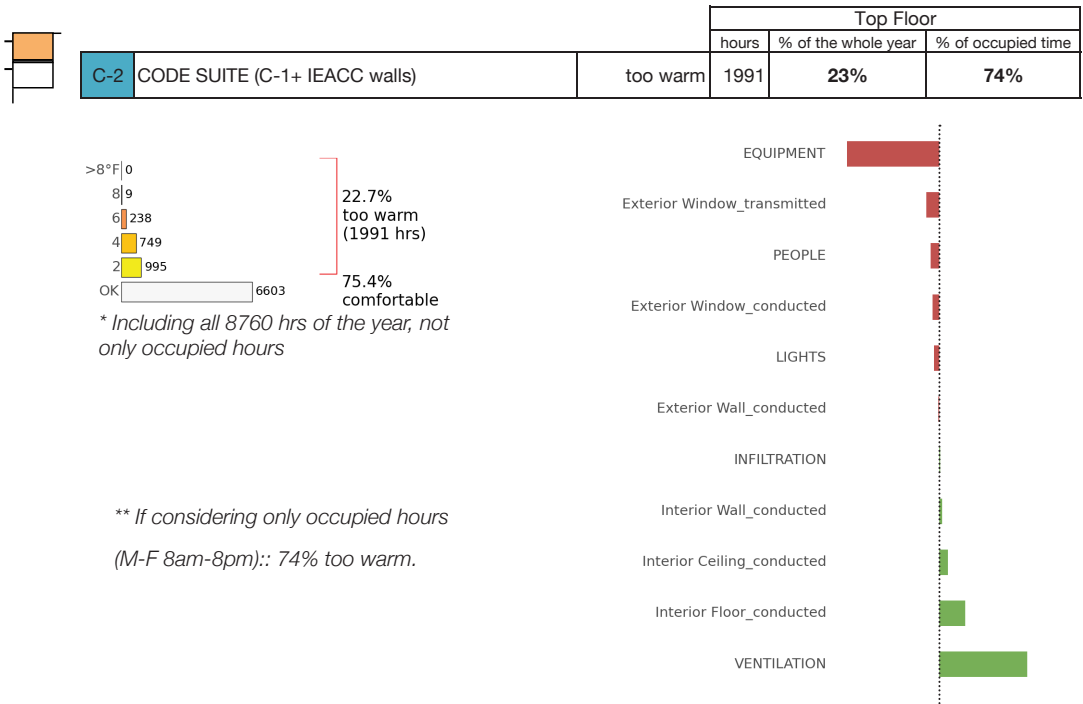
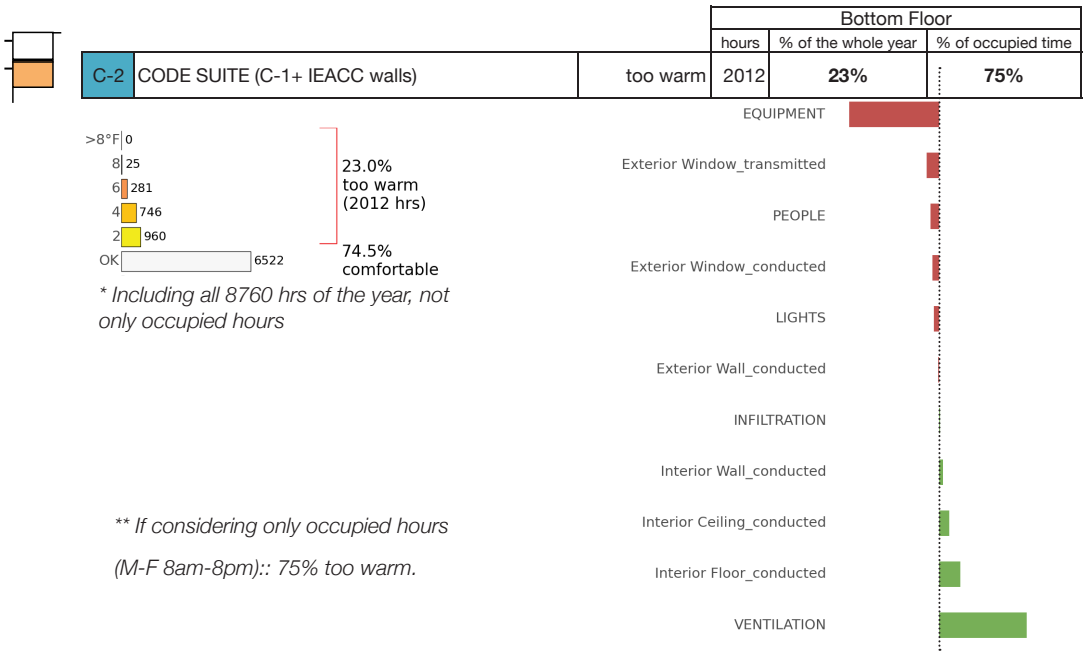
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.5.a.4 Laboratory Analysis:: South Facing (Continued)



Add/C.5.a. LABORATORY ANALYSIS:: SOUTH FACING

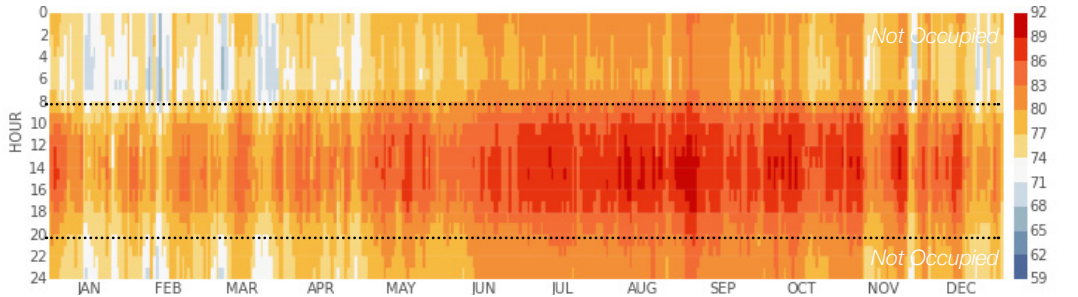
C.5.a.5. IDEAL SUITE



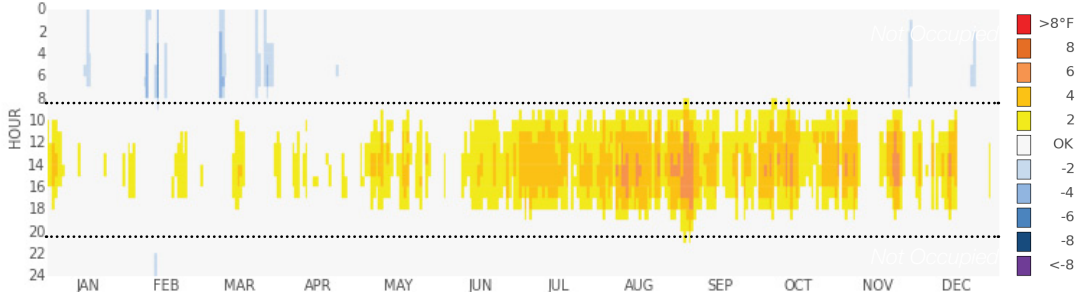
Equal to CODE SUITE + Thermal Mass



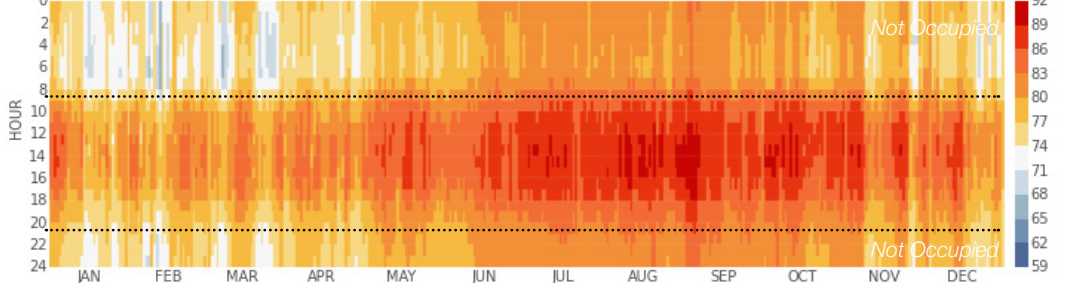
Operative temperature for bottom floor



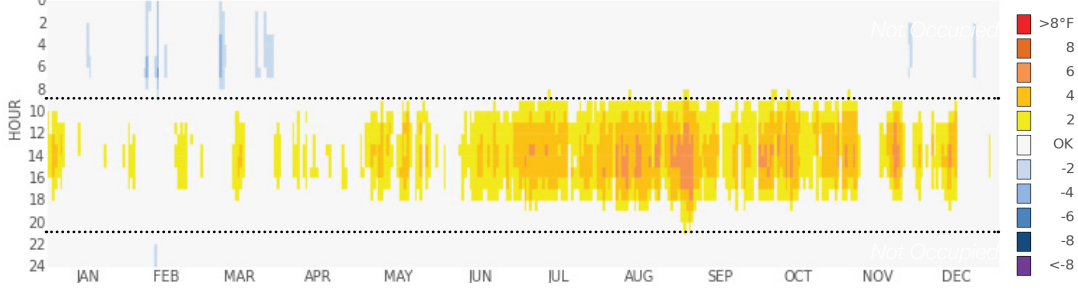
Degrees from comfort for bottom floor



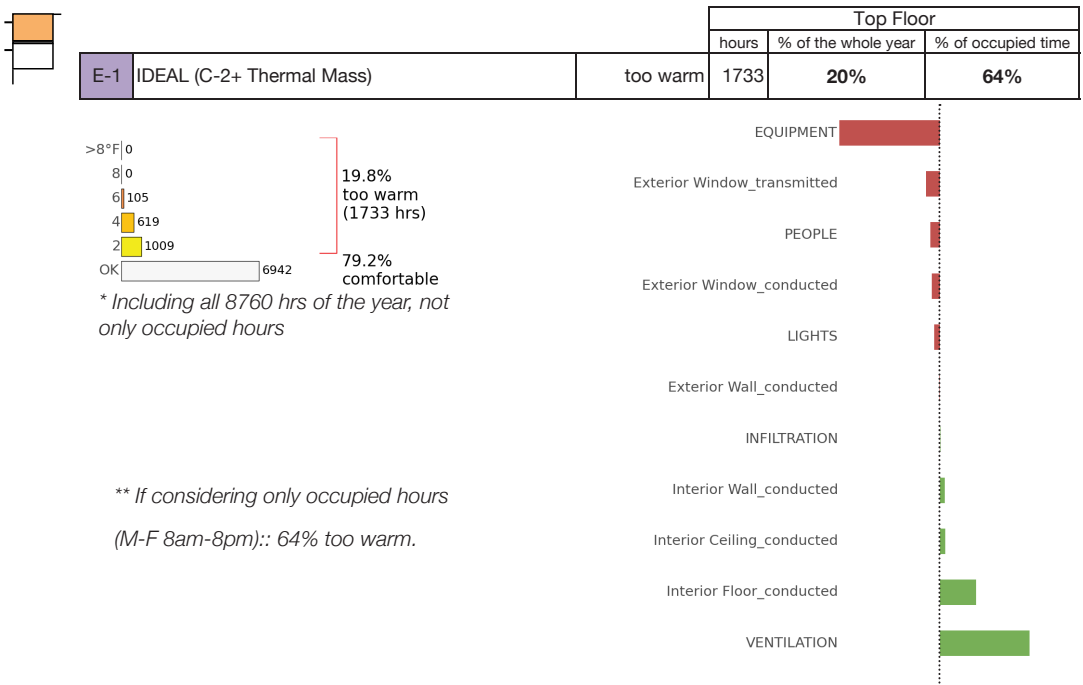
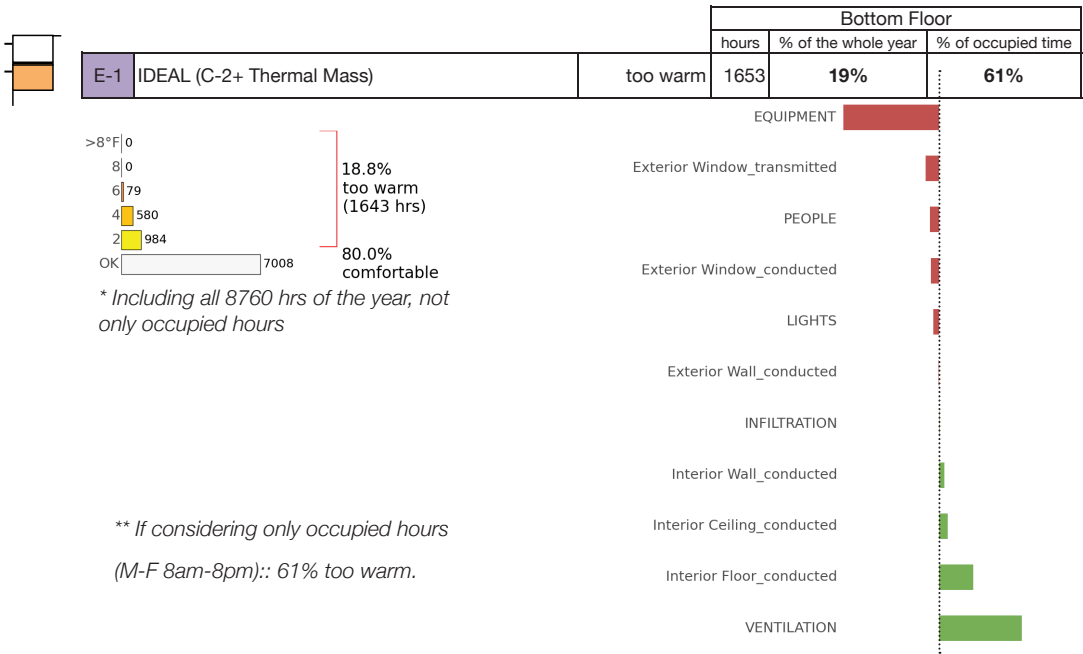
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.5.a.5 Laboratory Analysis:: South Facing (Continued)



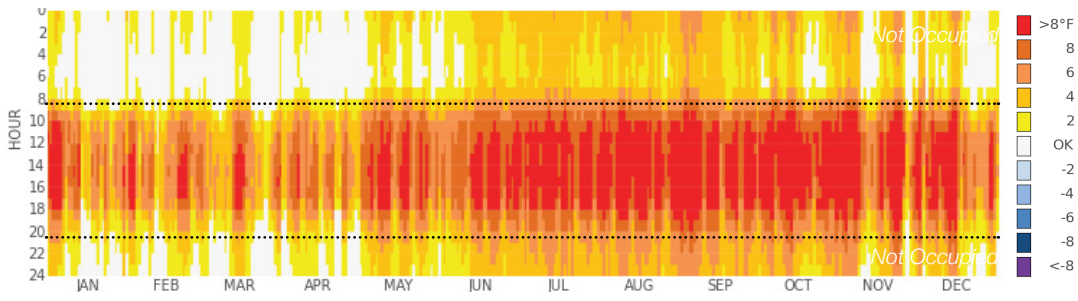
Add/C.5.a. LABORATORY ANALYSIS:: SOUTH FACING

C.5.a.6. IDEAL SUITE WITH VENTILATION PARAMETRICS

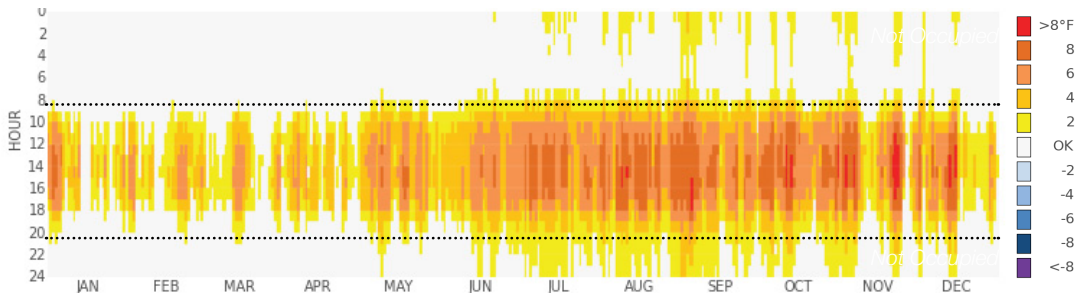


IDEAL SUITE + 3ACH, 5ACH, 7ACH, 9ACH, 11ACH, 13ACH

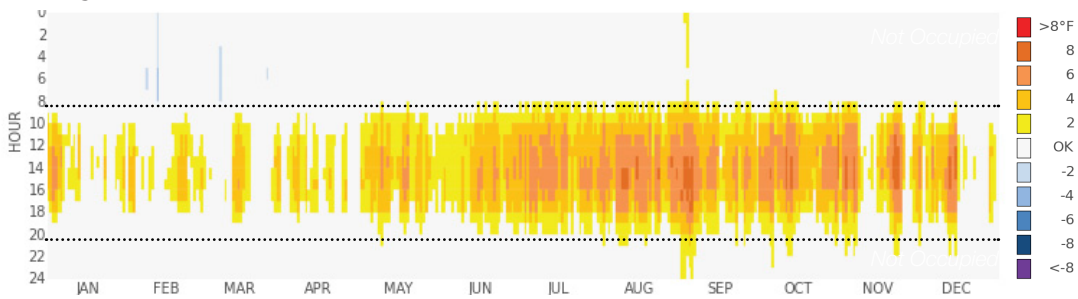
Degrees from comfort for bottom floor:: 3ACH



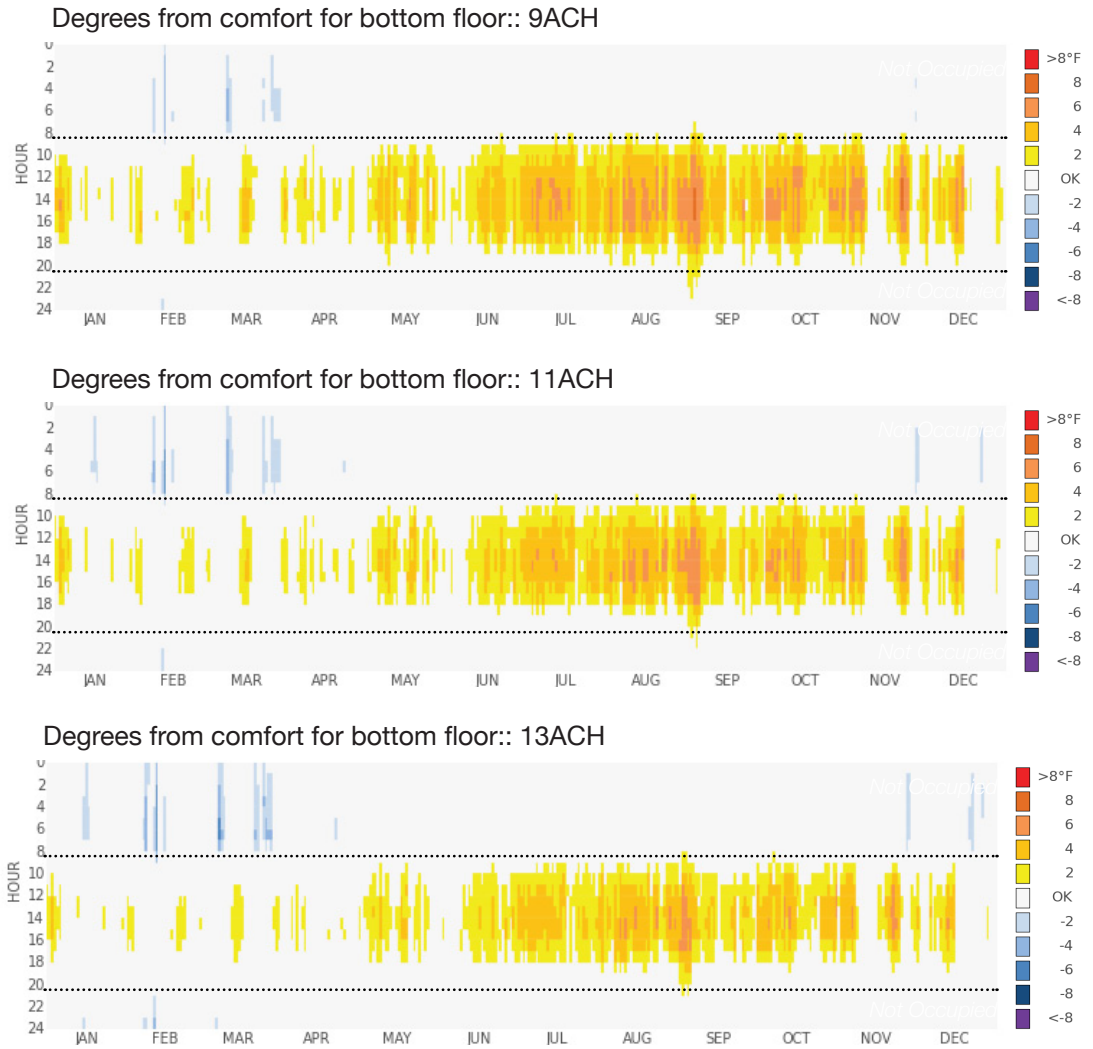
Degrees from comfort for bottom floor:: 5ACH



Degrees from comfort for bottom floor:: 7ACH



Add/C.5.a.6 Laboratory Analysis:: South Facing (Continued)



Add/C.5.a. LABORATORY ANALYSIS:: SOUTH FACING

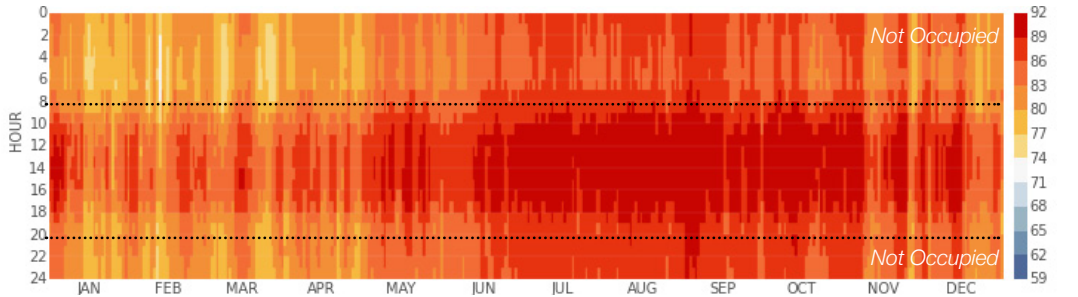
C.5.a.7. IDEAL SUITE WITH SMART VENTILATION



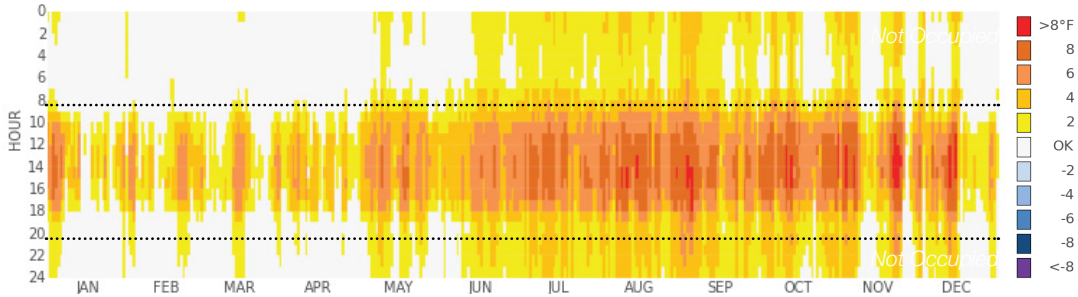
IDEAL SUITE + VARIABLE ACH (6ACH occupied, 3ACH unoccupied)



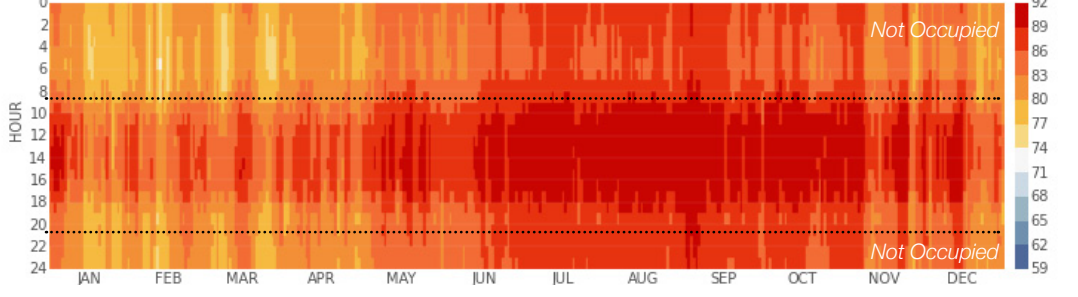
Operative temperature for bottom floor



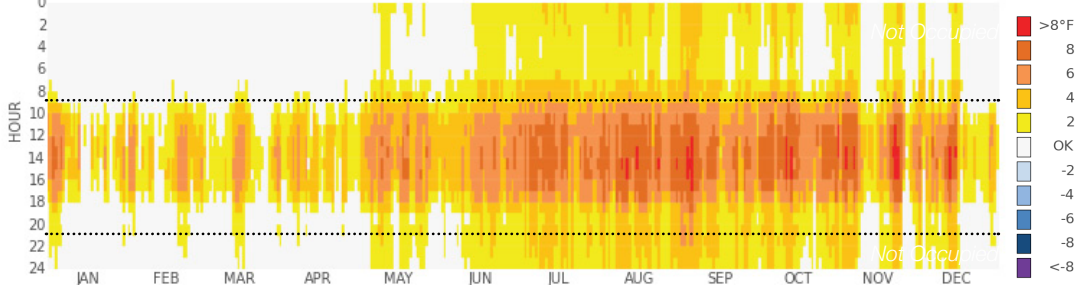
Degrees from comfort for bottom floor



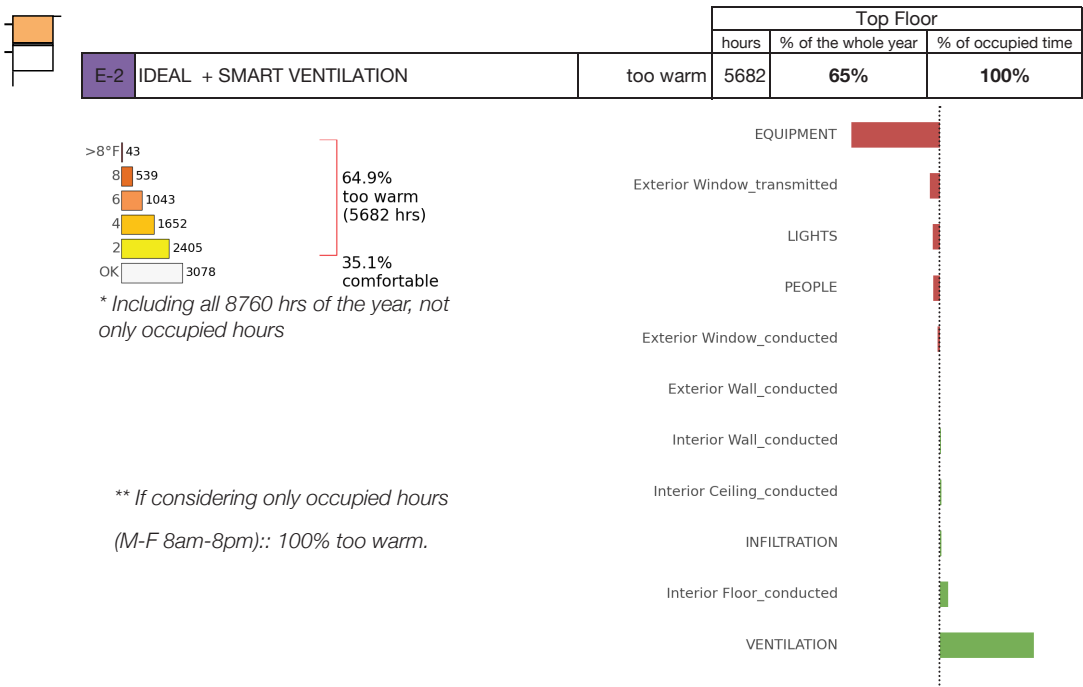
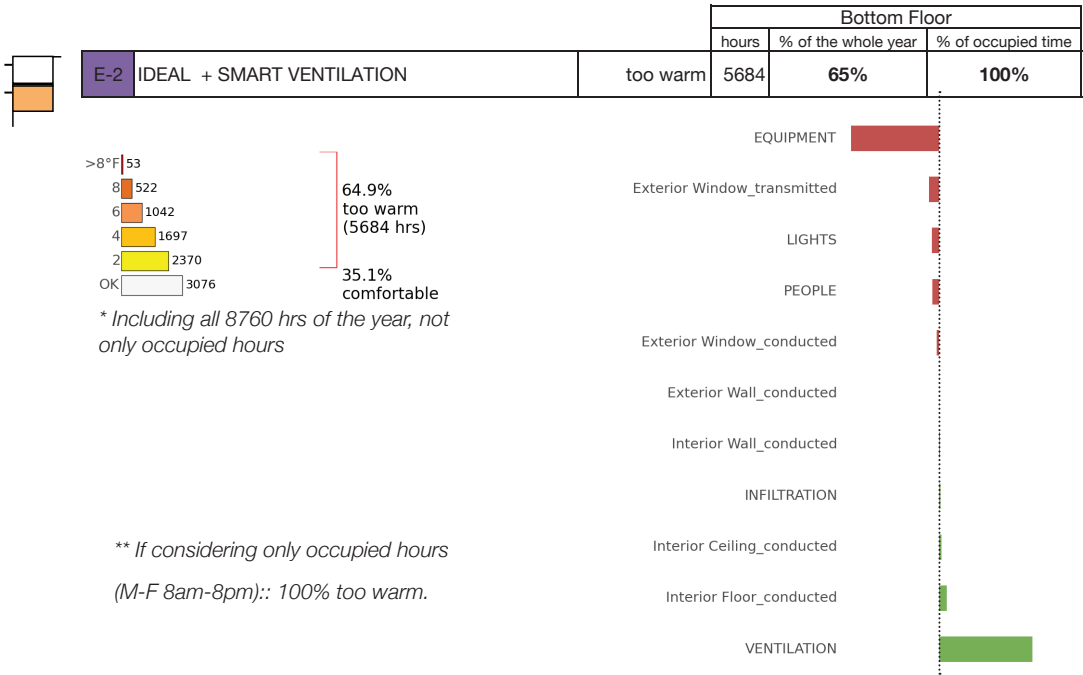
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.5.a.7 Laboratory Analysis:: South Facing (Continued)



Add/C.5.b. LABORATORY ANALYSIS:: NORTH FACING

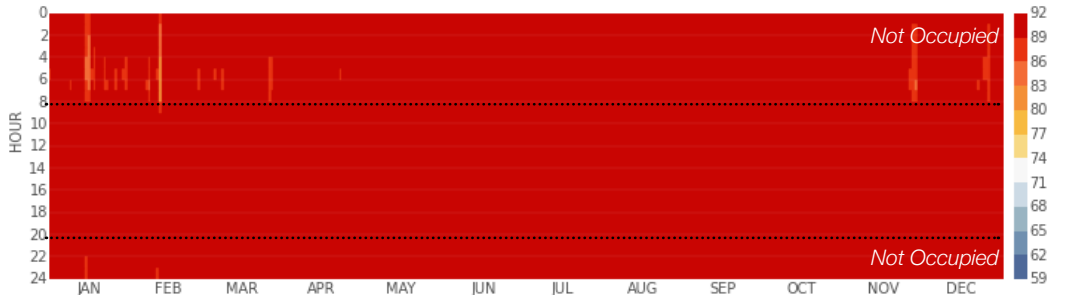


C.5.b.0. TYPICAL EXISTING

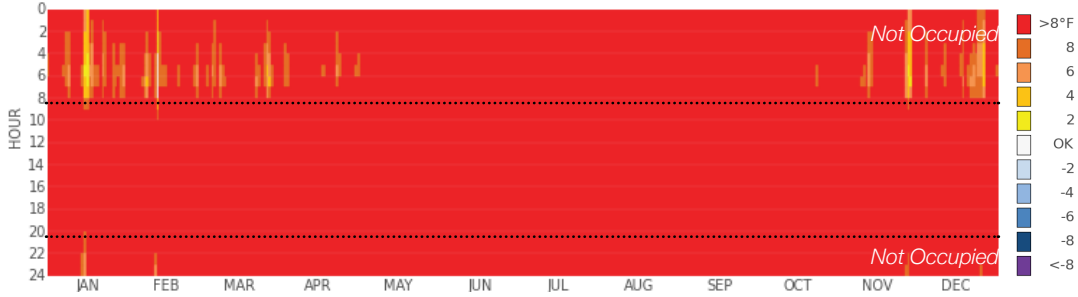
No Insulation in Opaque Surfaces and Single Pane Glass



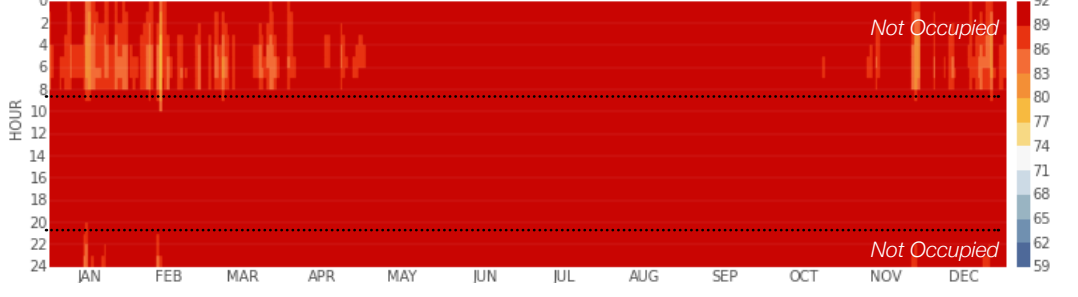
Operative temperature for bottom floor



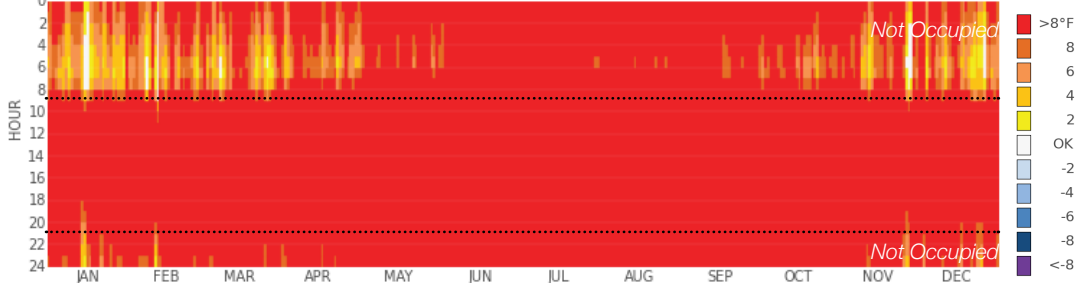
Degrees from comfort for bottom floor



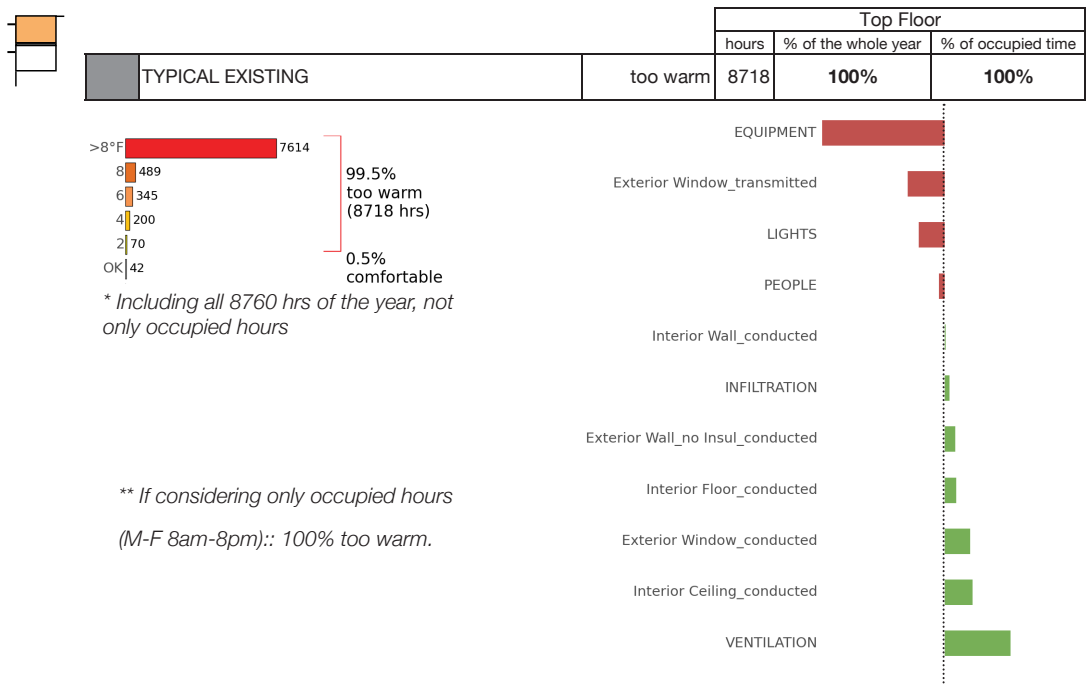
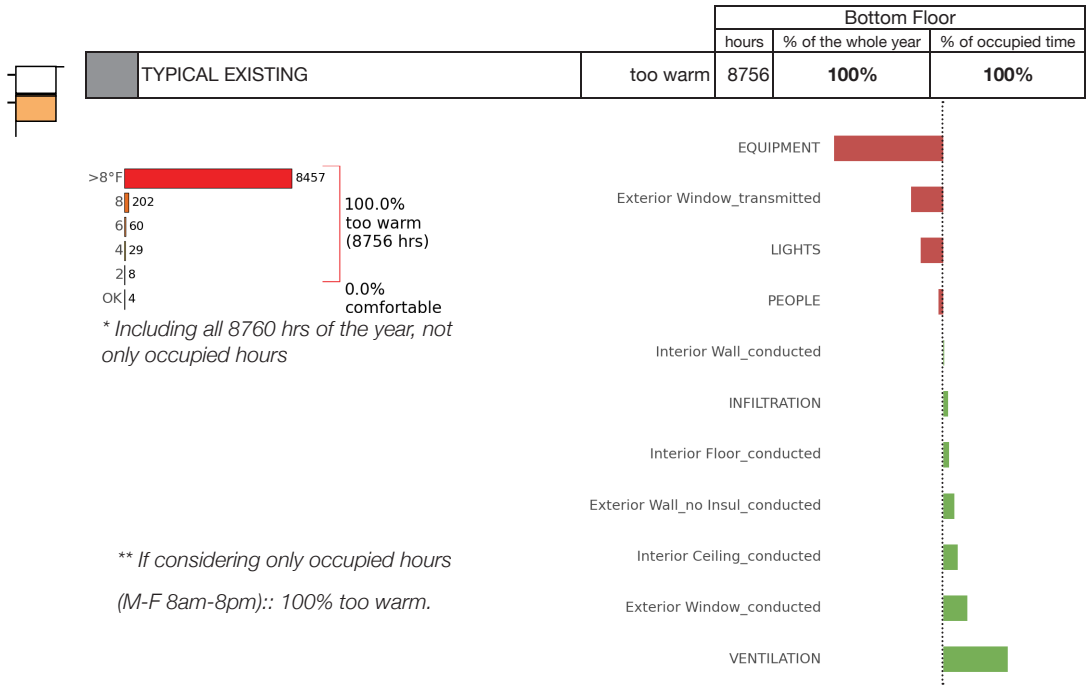
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.5.b.0 Laboratory Analysis:: North Facing (Continued)



Add/C.5.b. LABORATORY ANALYSIS:: NORTH FACING

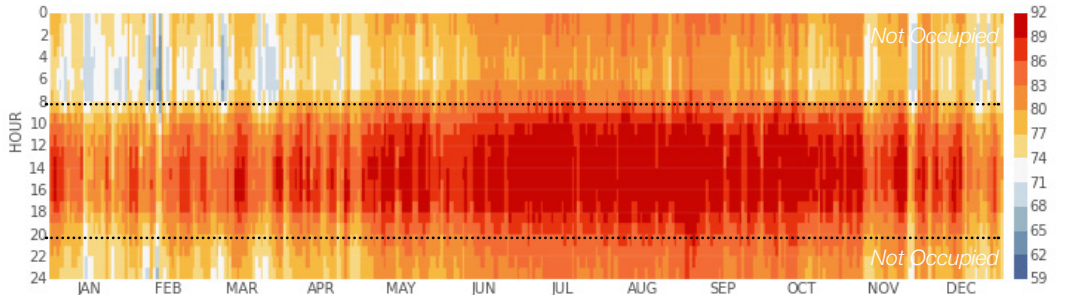


C.5.b.1. TYPICAL WITH WINDOW IMPROVEMENTS

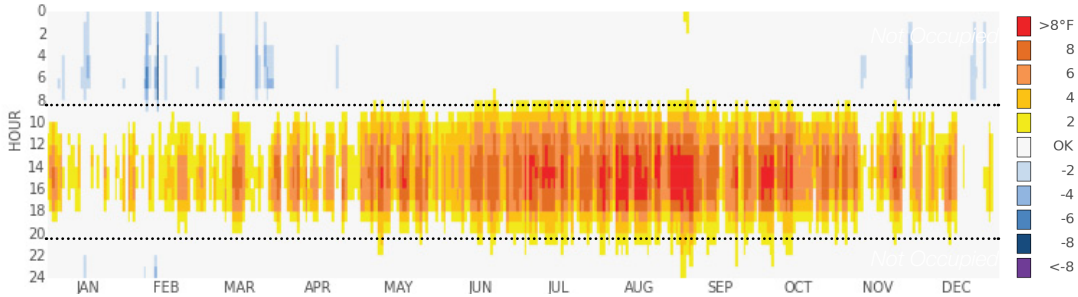
Equal to TYPICAL + Code Ventilation + Shading + IECC 2015 Windows



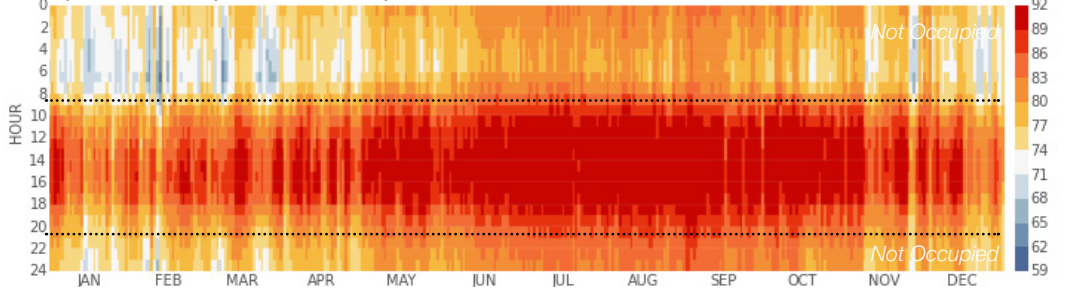
Operative temperature for bottom floor



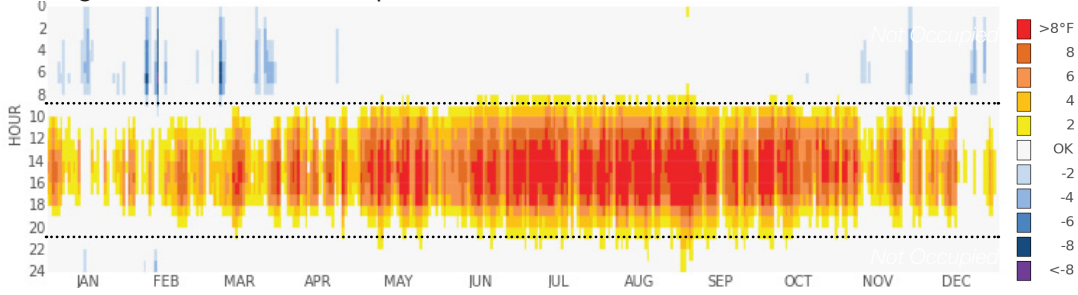
Degrees from comfort for bottom floor



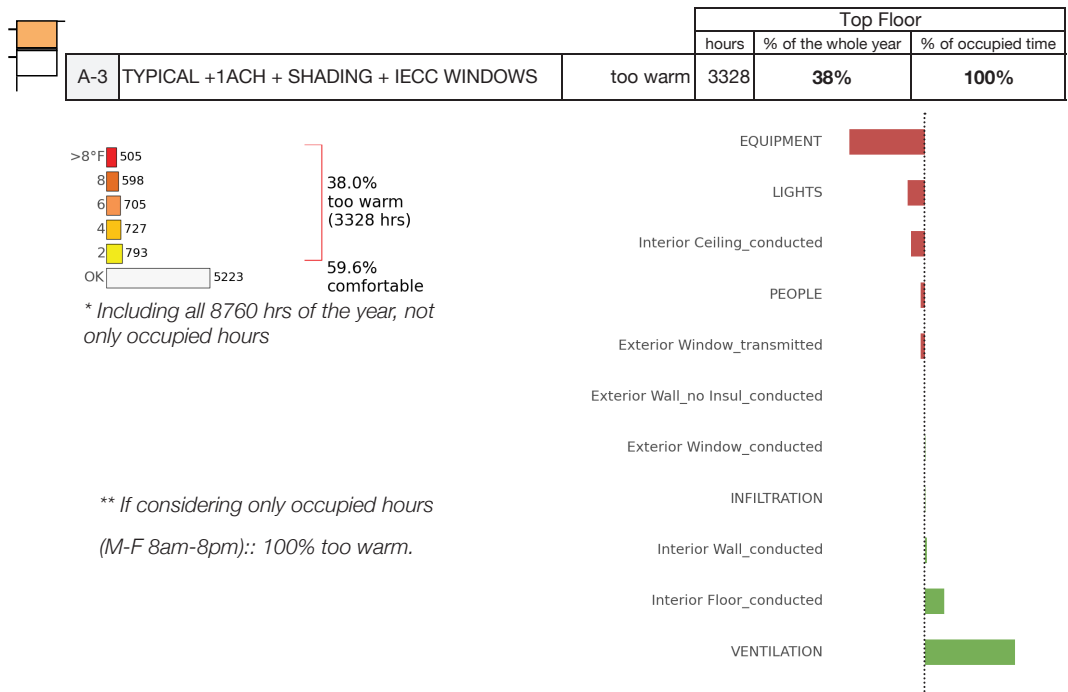
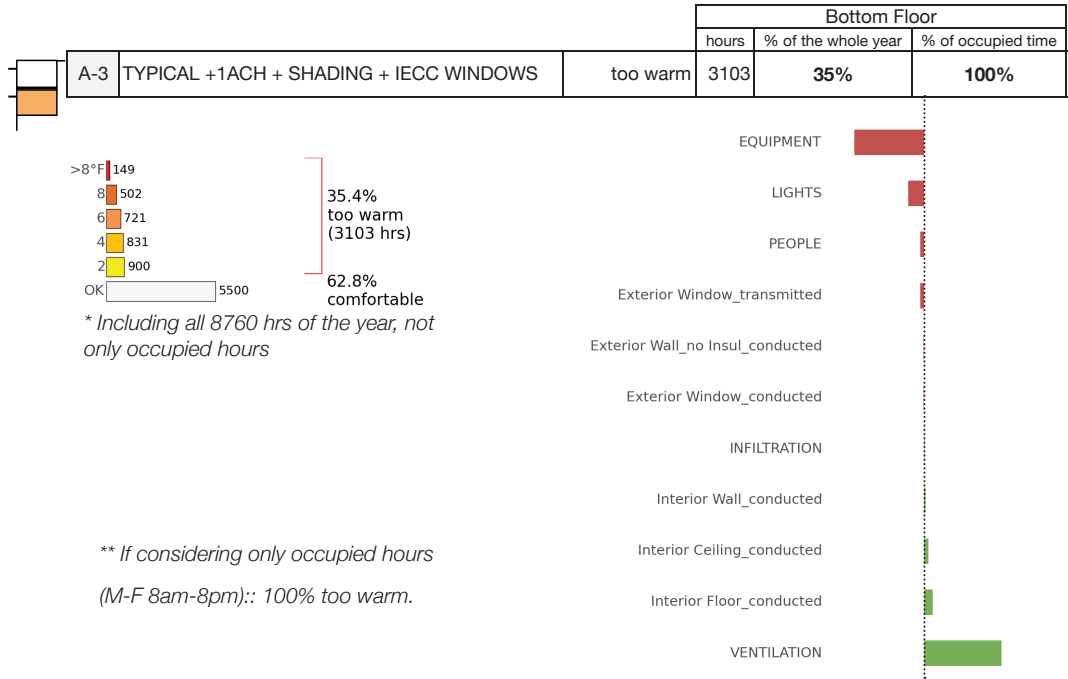
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.5.b.1 Laboratory Analysis:: North Facing (Continued)



Add/C.5.b. LABORATORY ANALYSIS:: NORTH FACING

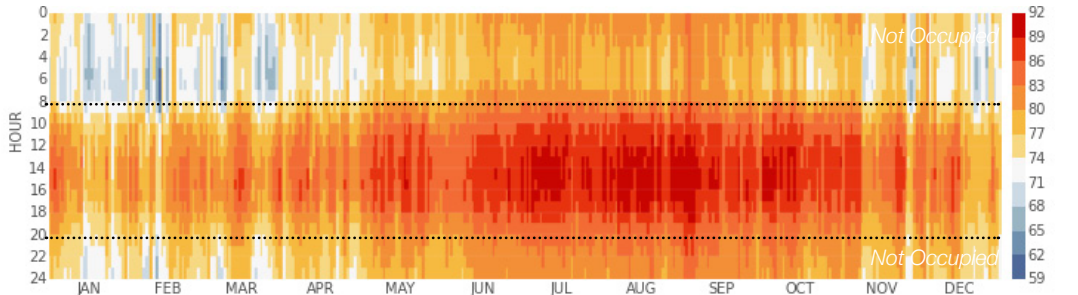


C.5.b.2. MINIMUM SUITE

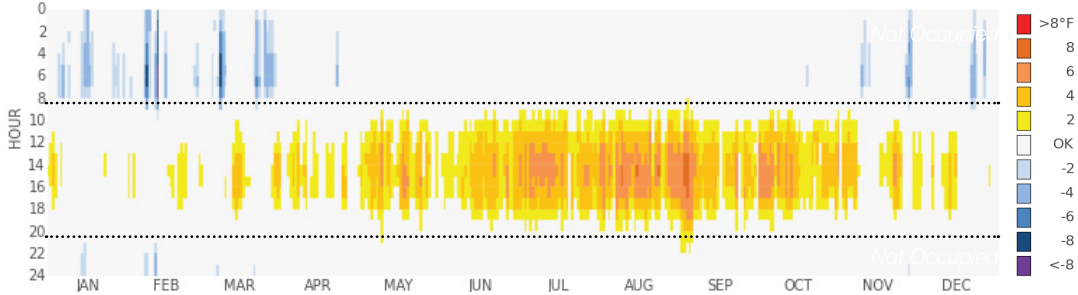
TYPICAL + IECC Windows + Shading +lower LPD + Daylight Controls +1ACH



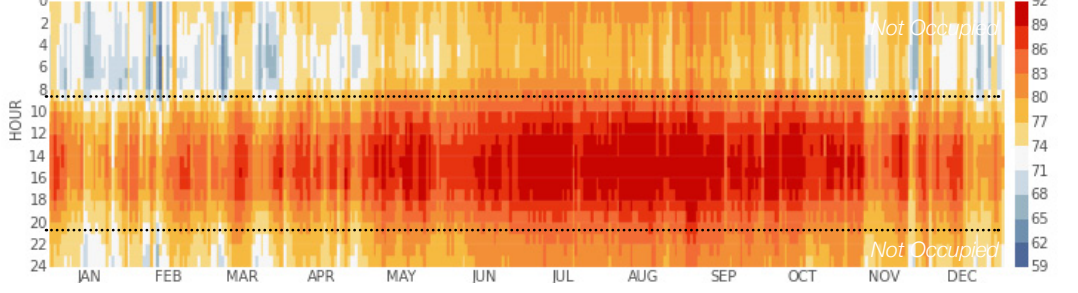
Operative temperature for bottom floor



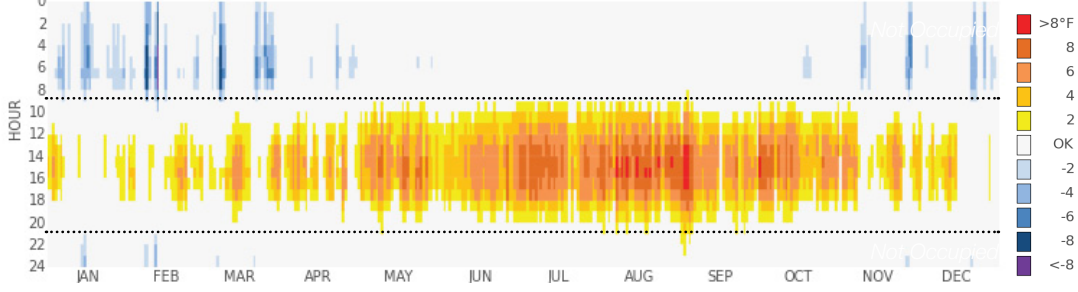
Degrees from comfort for bottom floor



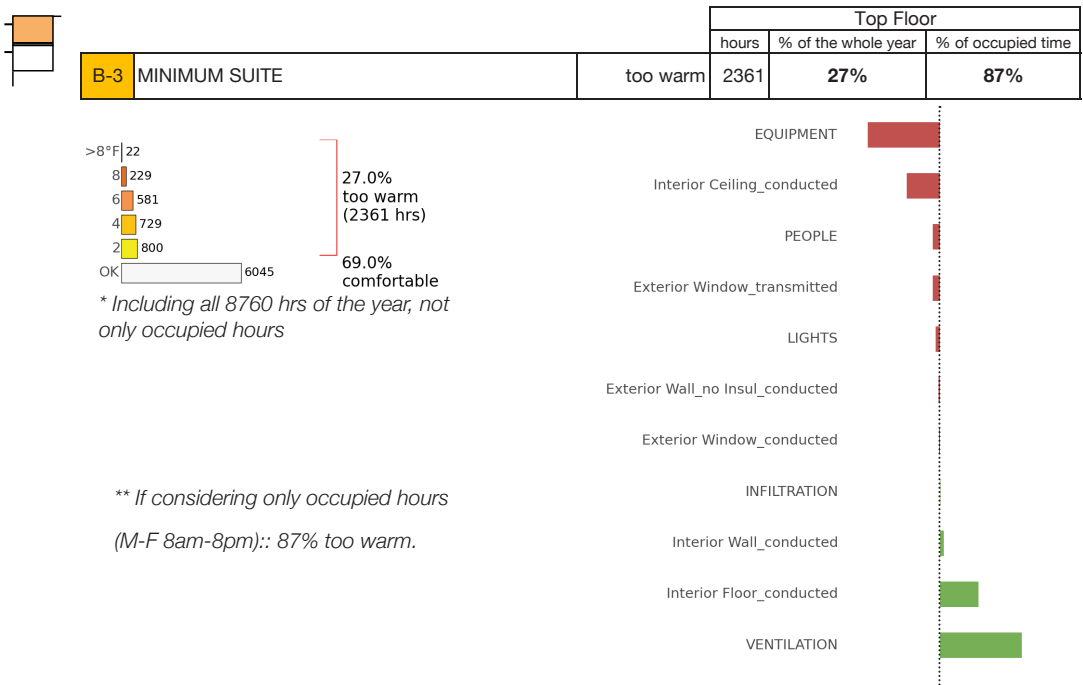
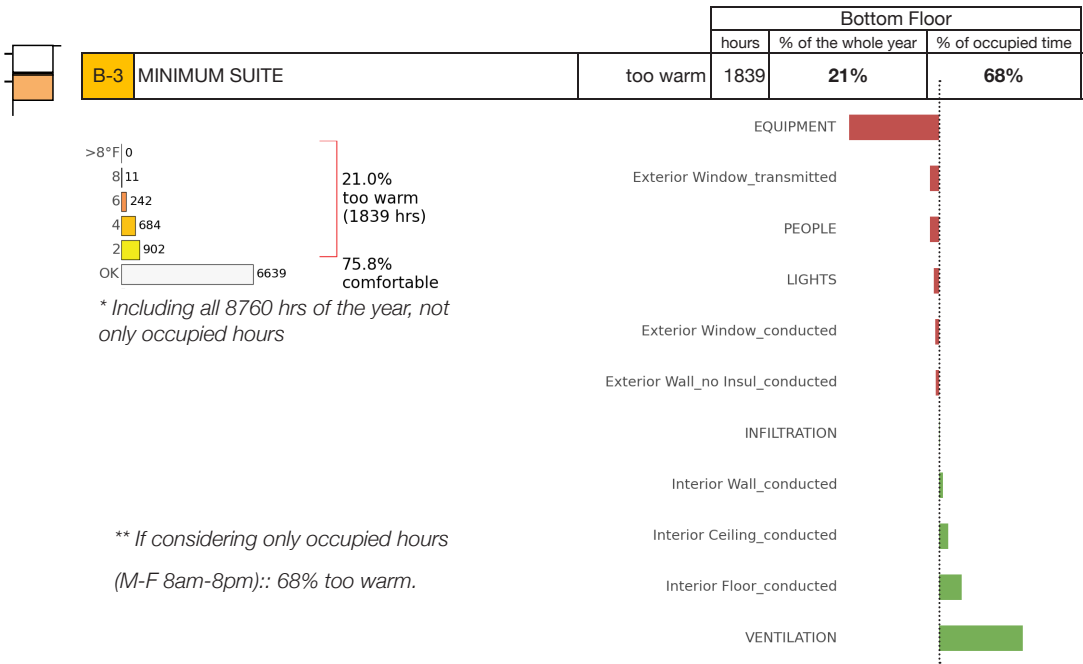
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.5.b.2 Laboratory Analysis:: North Facing (Continued)



Add/C.5.b. LABORATORY ANALYSIS:: NORTH FACING

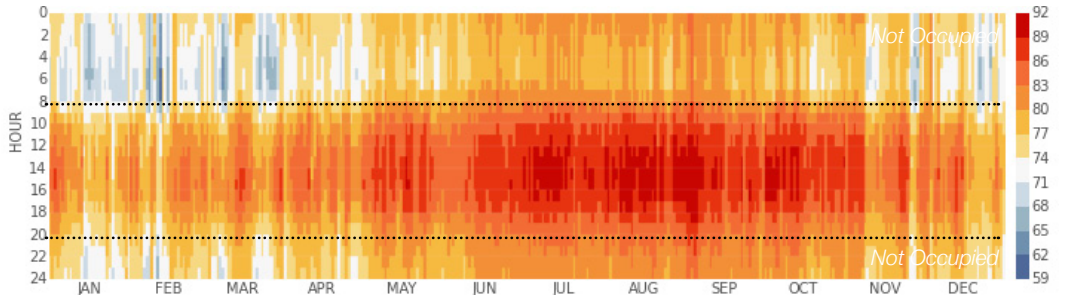


C.5.b.3. IMPROVED SUITE

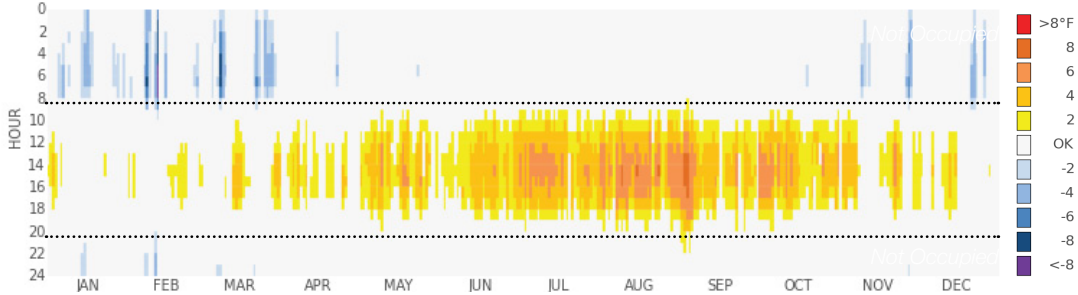
Equal to MINIMUM SUITE + IECC Roof



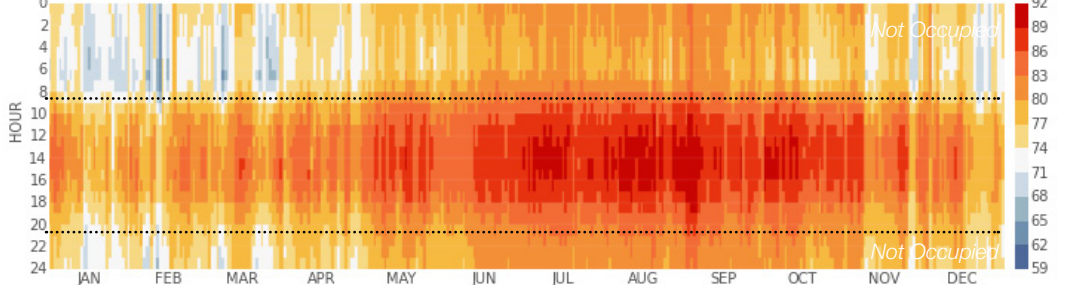
Operative temperature for bottom floor



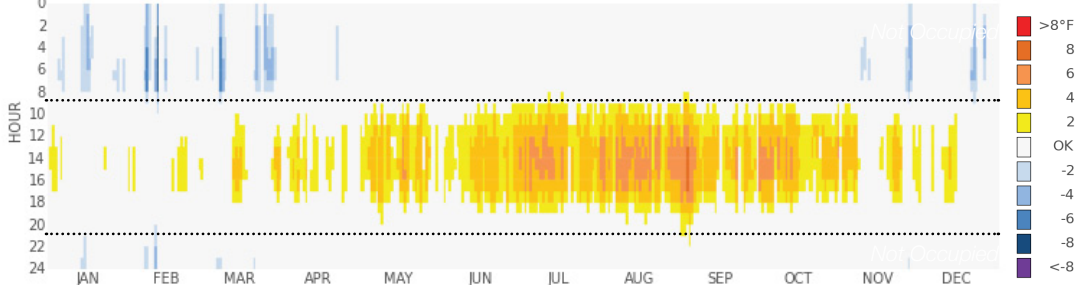
Degrees from comfort for bottom floor



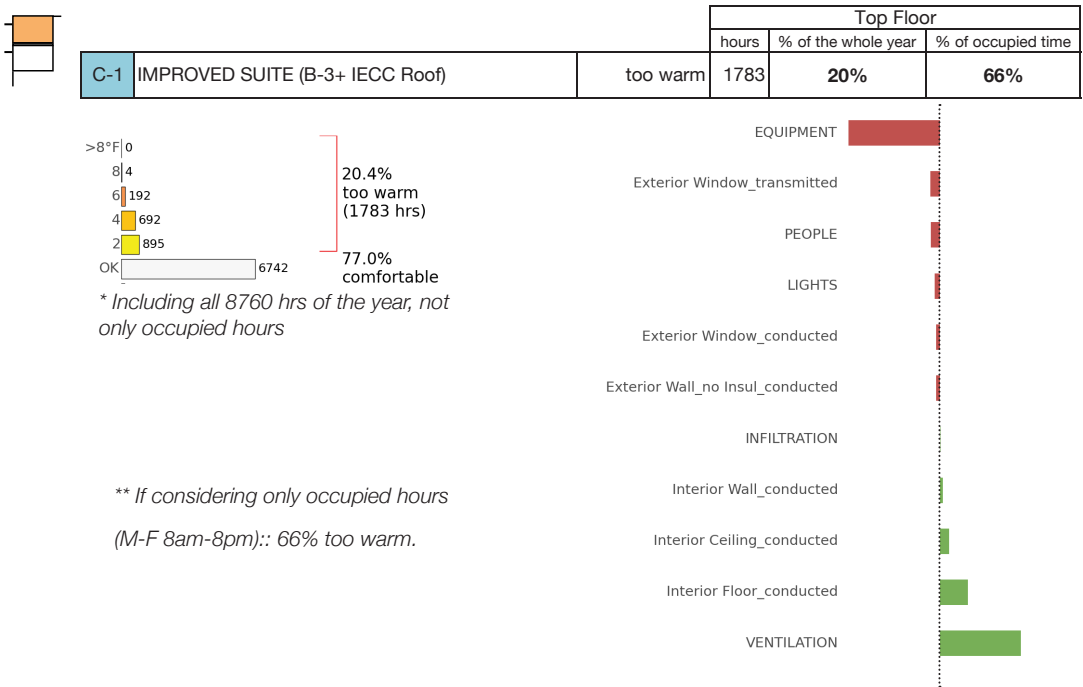
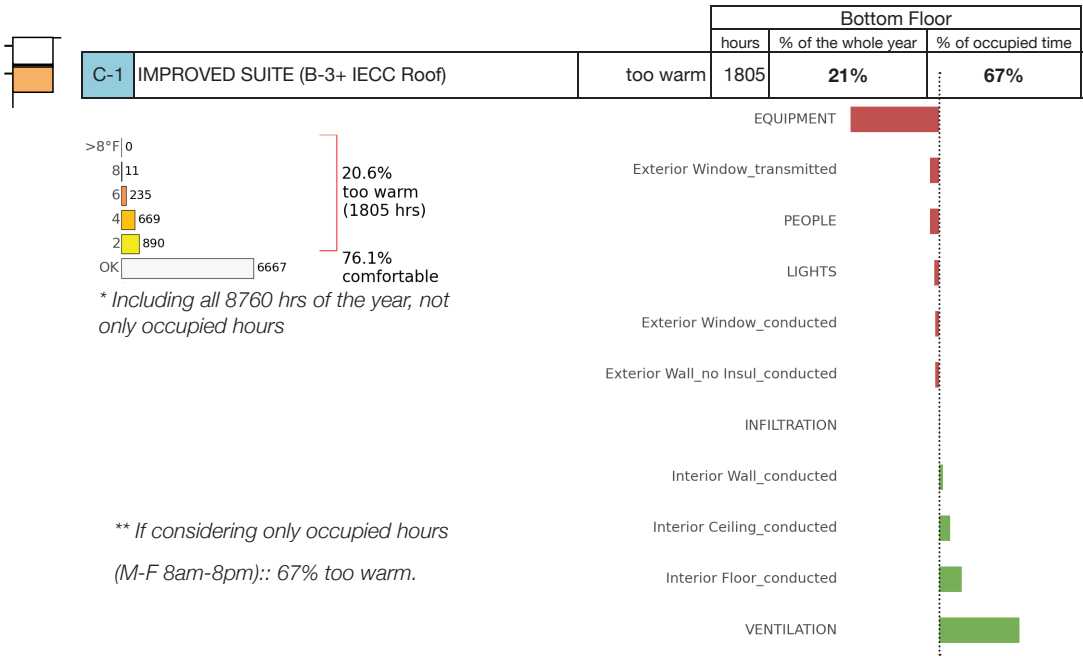
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.5.b.3 Laboratory Analysis:: North Facing (Continued)



Add/C.5.b. LABORATORY ANALYSIS:: NORTH FACING

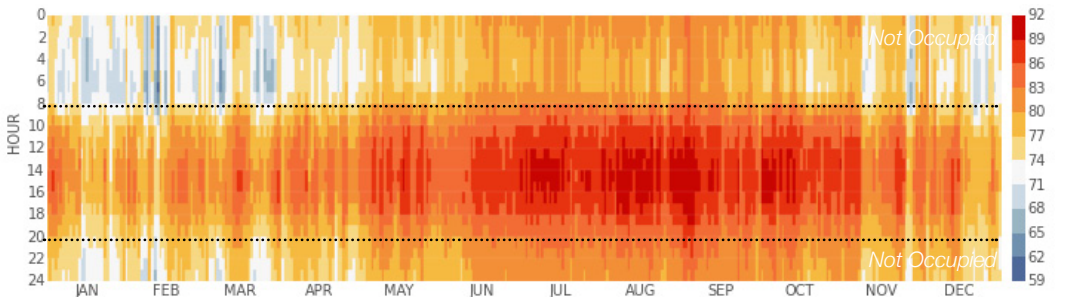


C.5.b.4. CODE SUITE

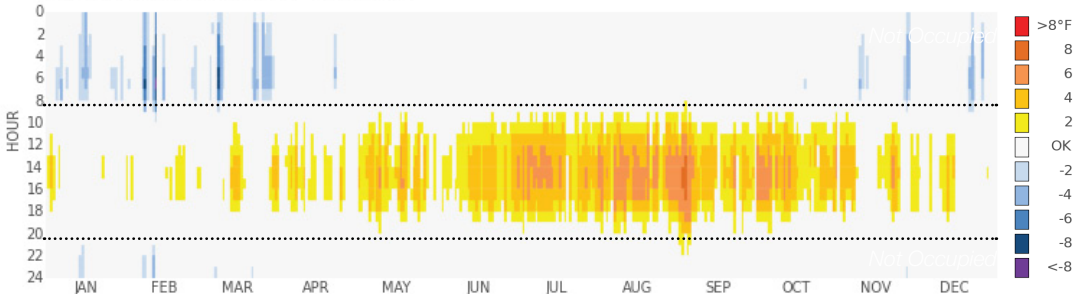
Equal to IMPROVED SUITE + IECC Walls



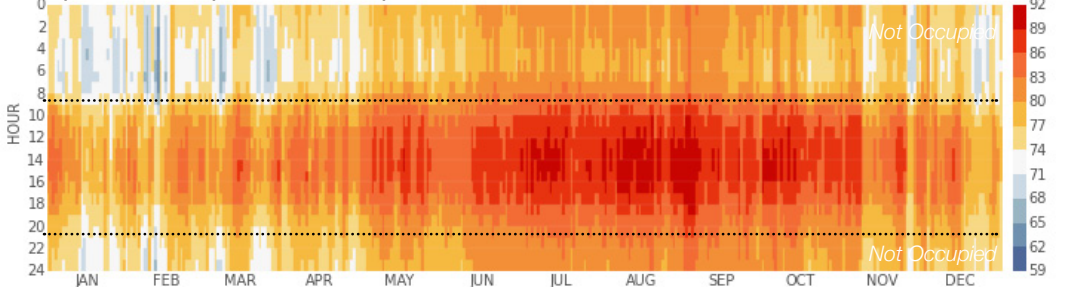
Operative temperature for bottom floor



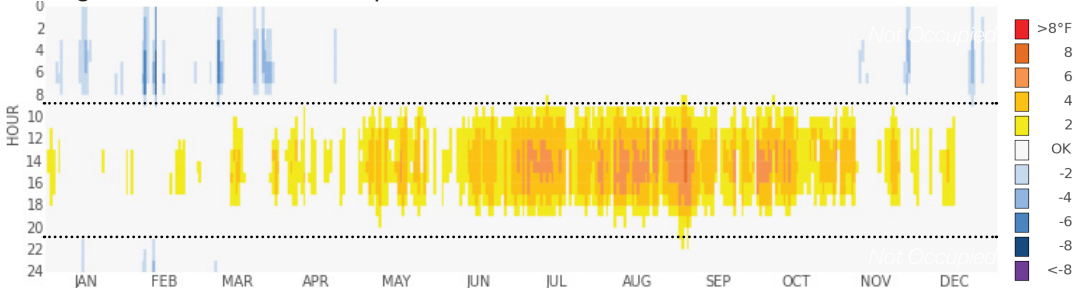
Degrees from comfort for bottom floor



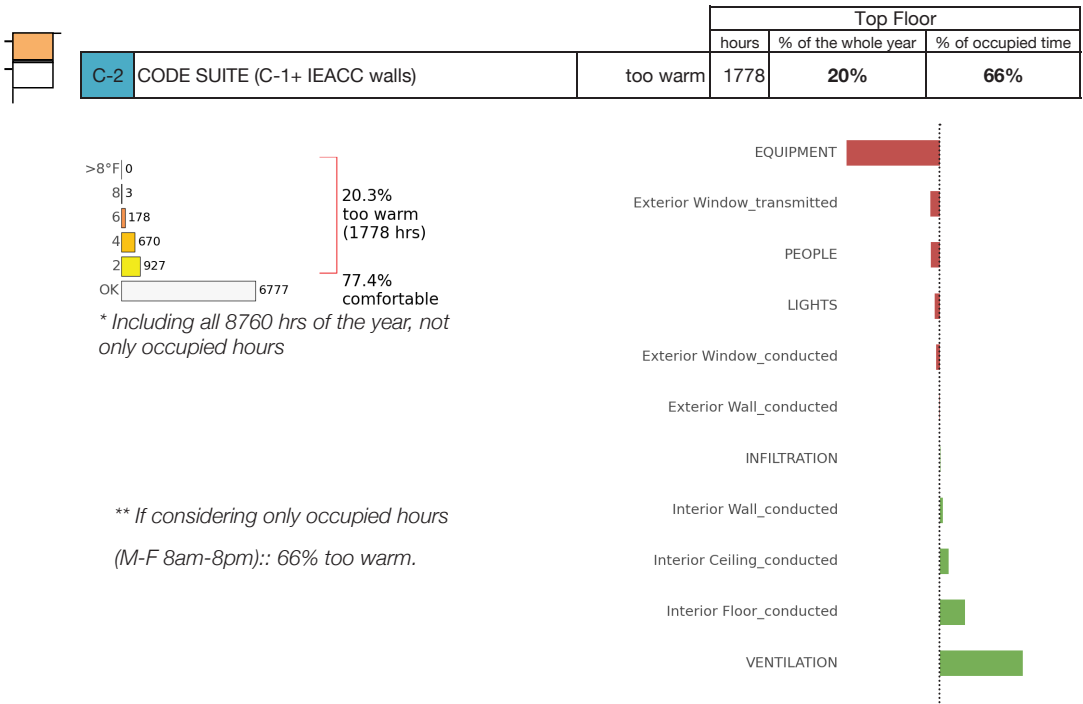
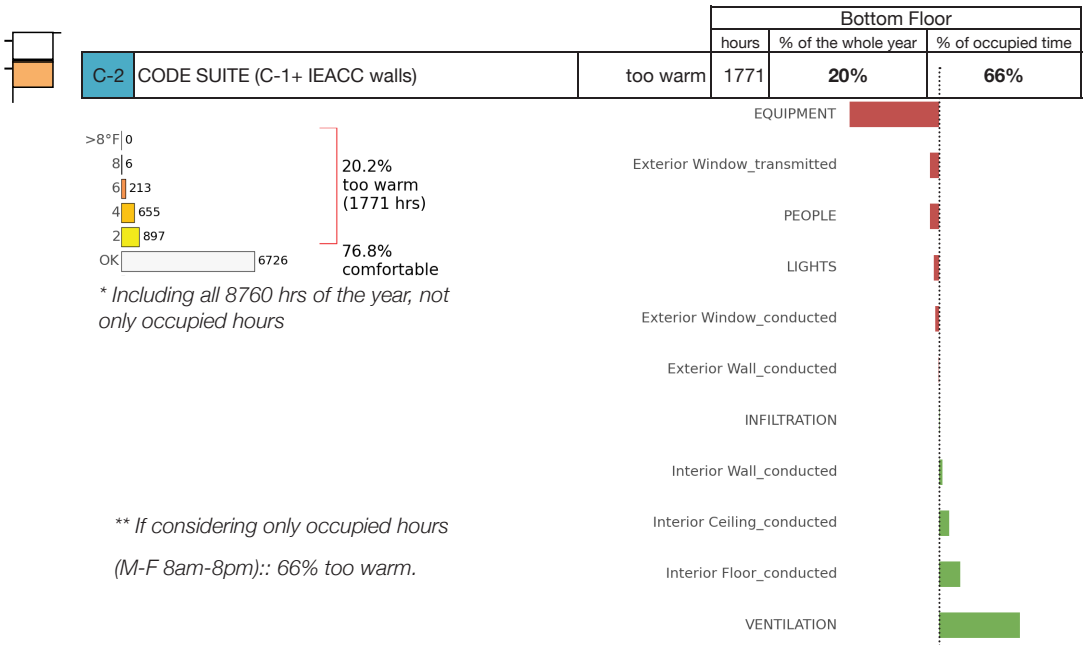
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.5.b.4 Laboratory Analysis:: North Facing (Continued)



Add/C.5.b. LABORATORY ANALYSIS:: NORTH FACING

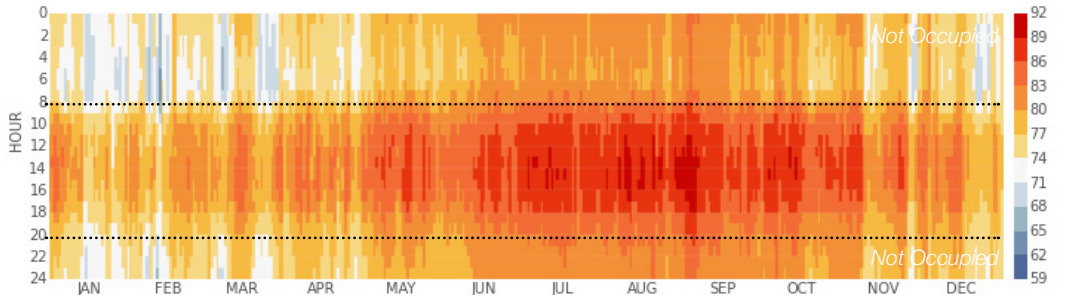


C.5.b.5. IDEAL SUITE

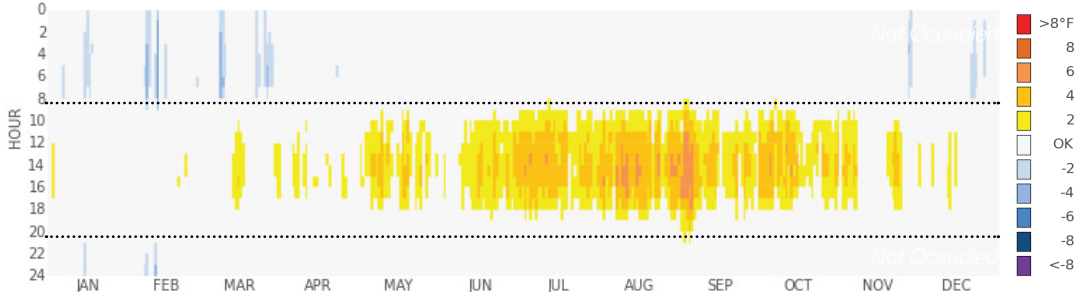
Equal to CODE SUITE + Thermal Mass



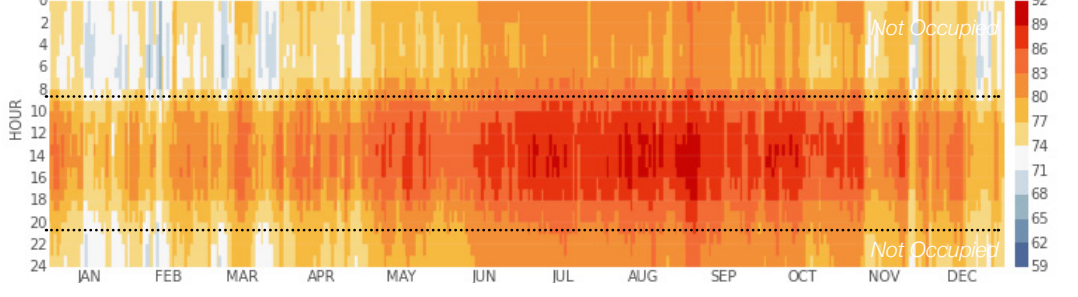
Operative temperature for bottom floor



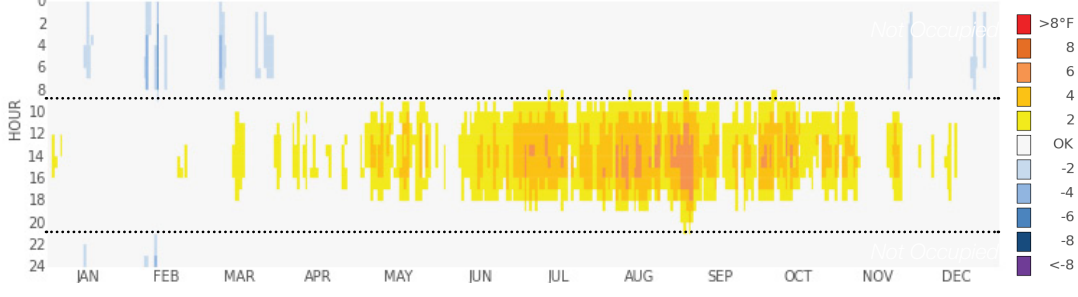
Degrees from comfort for bottom floor



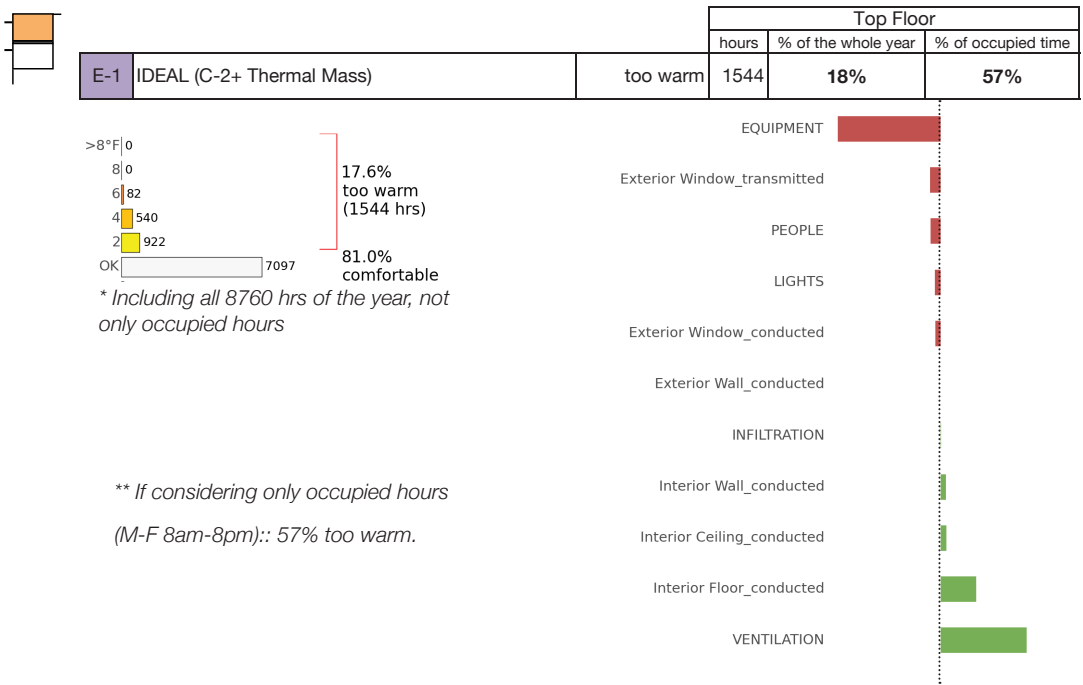
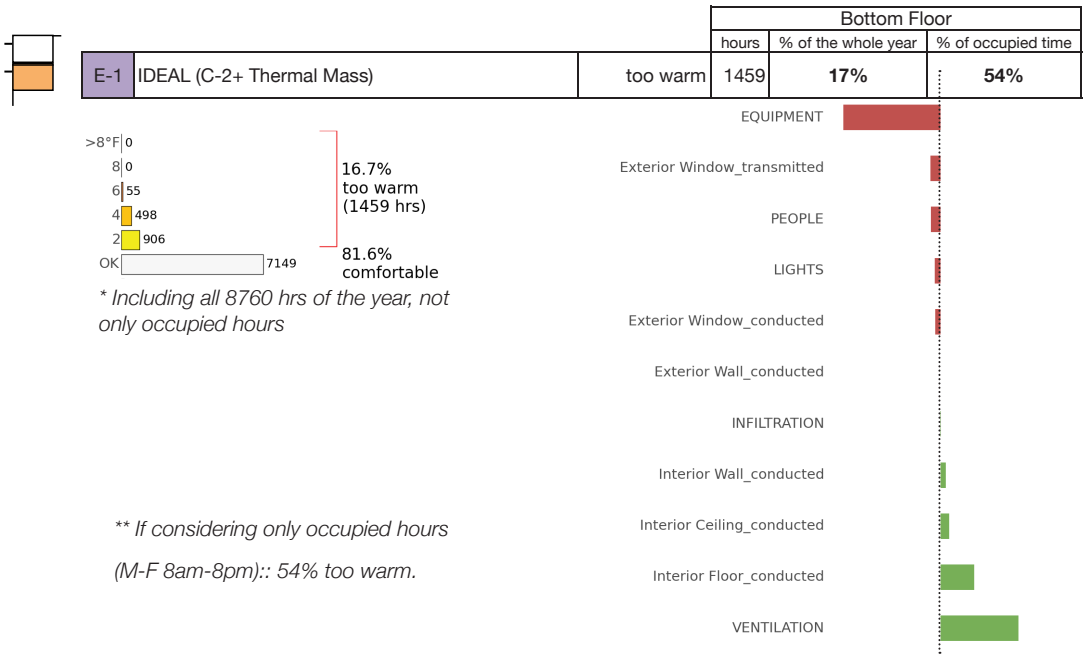
Operative temperature for top floor



Degrees from comfort for top floor



Add/C.5.b.5 Laboratory Analysis:: North Facing (Continued)



Add/C.5.b. LABORATORY ANALYSIS:: NORTH FACING

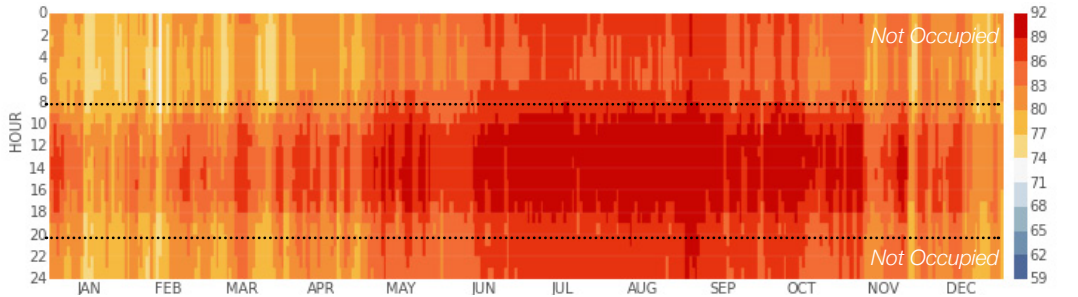


6. IDEAL SUITE WITH SMART VENTILATION

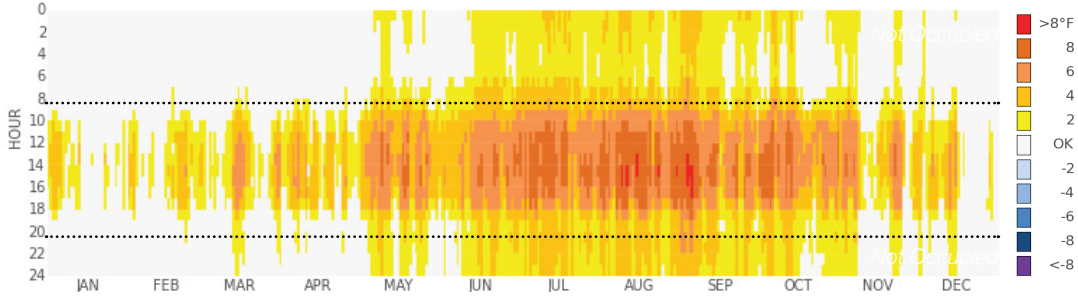
Equal to CODE SUITE + Variable ACH



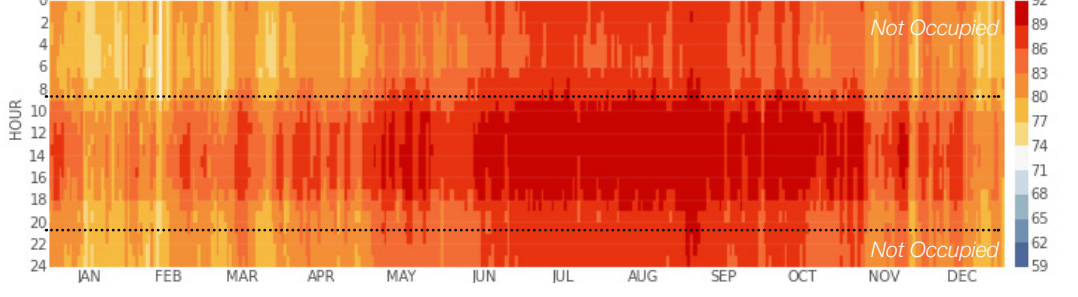
Operative temperature for bottom floor



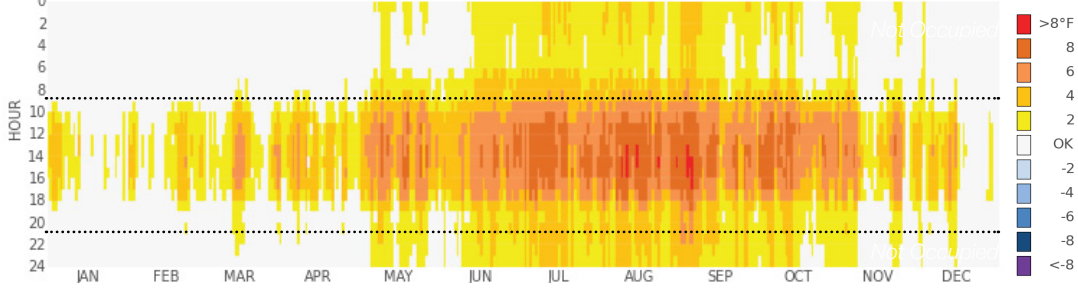
Degrees from comfort for bottom floor



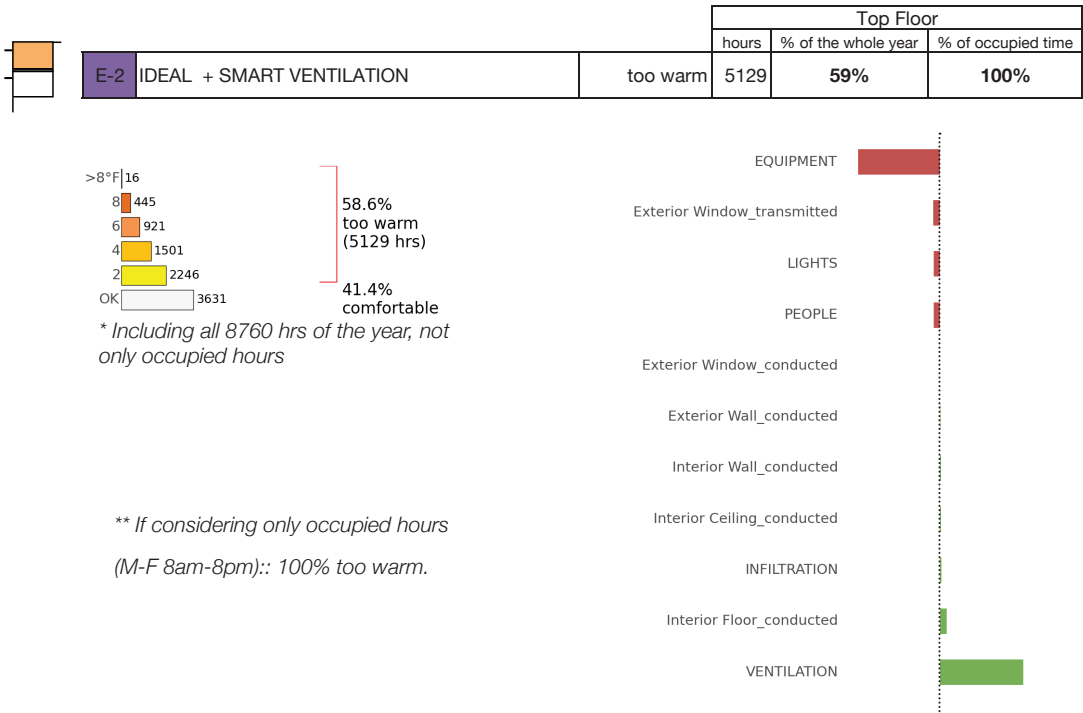
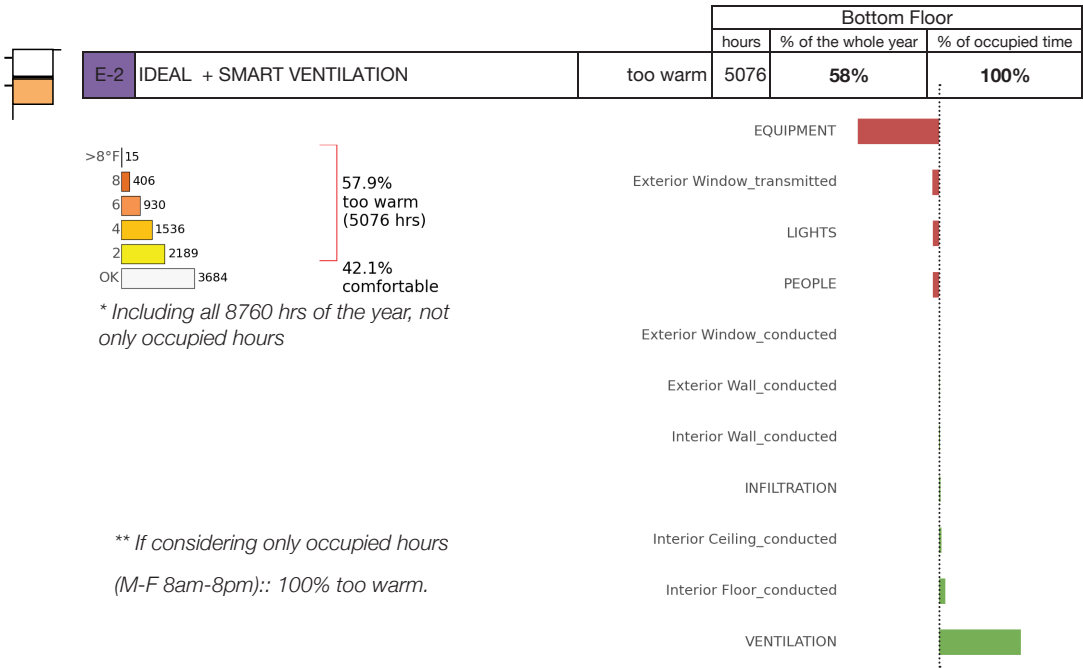
Operative temperature for top floor



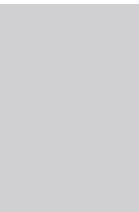
Degrees from comfort for top floor



Add/C.5.b.6 Laboratory Analysis:: North Facing (Continued)



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D. ENERGY STUDIES

1. EXECUTIVE SUMMARY

Based on the models used for the HVAC autonomy/ Thermal Comfort simulations, we developed a series of scenarios that included mechanical conditioning. For each building type, we ran Typical, Minimum Improved, Code and Ideal suites and compared the estimates of the total electricity use per building type area. (Please refer to the Executive Summary in Add.3/ HVAC Autonomy- Thermal Comfort Studies for a description of each suite).

The improved, code and ideal suites assume ceiling fans and thus, the possibility of setting a higher thermostat setpoint to activate the cooling systems. An increase in airspeed increases the acceptable operative temperature limits described in the proposed Addendum to ASHRAE Std 55 to take in to account impact of airspeed on comfort.

These results were then compared to data from the Commercial Buildings Energy Consumption Survey (CBECS) for similar buildings and UHM data from the UHM Benchmarking Study 2004 and the UHM Strategic Energy Plan 2011. Some of these comparisons are not as straight forward as expected, as they depend on the buildings included in or the definition of each “building type” category. For example, the CBECS data includes mostly K-12 schools under the “Education” category. Occupancy schedules and building form are likely very different from the assumptions included in our models. The UHM data from 2004 combines different occupancy types (Lab and classroom or Lab/ classroom/ office) and is not directly comparable with our modeling results either. However, all these data give a sense of the range of acceptable results.

Occupancy Type	Occupied Building Space (sq.ft.)	Building Space (sq.ft.)	Electricity Use (kWh/year)	Electricity Use per square foot (kWh/sq.ft.-year)	Energy Use	Energy Use to Area
LAB/CLASS	94,133	2	5,964,206	64.3	4.3	2.2
LAB/CLASS /OFFICE	855,234	14	38,263,645	44.7	27.4	2.0
OFFICE/LAB	476,381	8	16,487,311	34.7	11.6	1.5
OFFICE	426,497	7	10,111,205	23.7	7.2	1.0
CLASS/OFFICE	1,390,020	22	30,277,275	21.8	21.7	1.0

Fig 3.14. UHM Building Square Feet and Yearly Electricity Use*

* Source: UH Manoa Benchmarking Study 2004

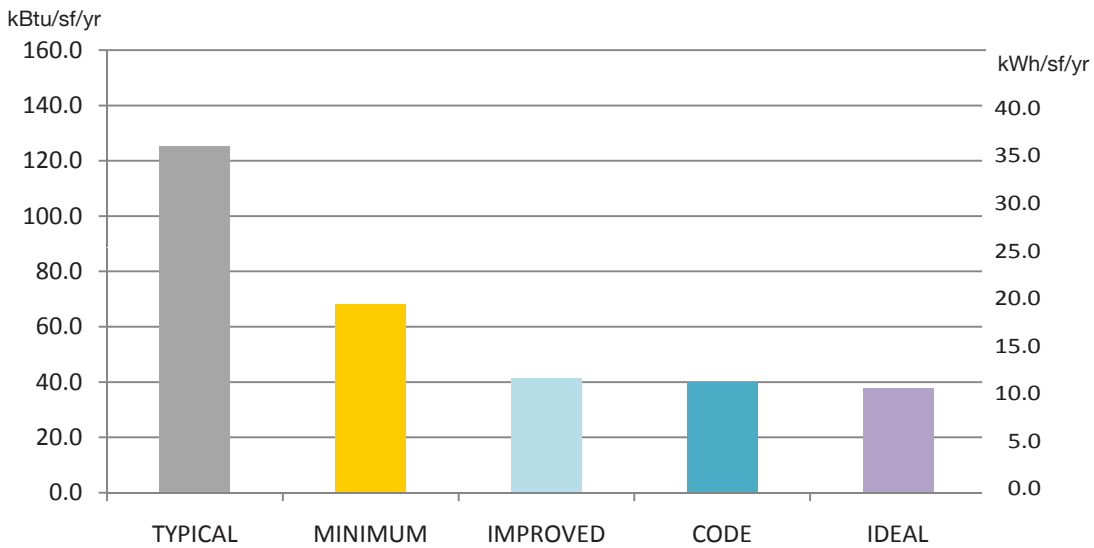
Add/D.1 Executive Summary (Continued)

a. Classroom Model Results

On average, for all orientations, classrooms in existing UHM buildings (Typical Existing) would use 122.1 kBtu/sqft/yr (35.8 kWh/sqft/yr). Examples and benchmarking data are on the next page.

By improving the windows (glazing specifications, installing shading devices and making those windows operable), in Addition to controlling the time the lights are on and effectively reducing the lighting loads during daytime hours (Minimum Suite), total energy use is reduced by 43%. This is due to both the reduction in lighting energy use (75%) but also the impact of turning off the lights on the interior temperature and consequently on the cooling energy needed for each classroom.

Adding IECC 2015 prescriptive requirements for the roof (Improved Suite), further reduces the energy use intensity to 65% less than typical existing conditions. Other improvements such as IECC 2015 prescriptive wall specifications (Code Suite) and exposed thermal mass (Ideal Suite) do not have such a significant impact on the total energy use (66% and 68% less than typical respectively),



	EUI (kBtu/sqft/yr)		Total Energy (Site) (kBtu)		Cooling (kBtu)		Lighting (kBtu)		Equipment (kBtu)		Reheat?	
TYPICAL	122.1		286952		255599		22177		8942		233	
MINIMUM	69.4	43%	163204	43%	148524	42%	5525	75%	8942		212	
IMPROVED	42.5	65%	99872	65%	82042	68%	5525	75%	11625		680	
CODE	41.3	66%	97173	66%	79286	69%	5525	75%	11625		736	
IDEAL	39.4	68%	92608	68%	74602	71%	5525	75%	11625		855	

Add/D.1 Executive Summary (Continued)

		EUI (kWh/sqft/yr)
TYPICAL		35.8
MINIMUM		20.3
IMPROVED		12.5
CODE		12.1
IDEAL		11.5

				EUI (kWh/sqft/yr)
				<i>class/office</i>
UHM Benchmarking Study 2004				21.8
CBECS				
	<i>by size</i>	<i>by age</i>	<i>by use</i>	
2003	12.2	11.9	8.2	
Strategic Energy Plan 2011 data				34.6



1175 - MOORE HALL



1017 - SHIDLER

UHM CLASSROOM BUILDINGS

Avg Size: 46,000 sqft
 Avg. Age: 51 years, built 1964
 Avg. EUI: 34.6 kWh/sf*
 Avg. EUI by end use:
 - lighting 4.6 kWh/sf* ~13%



1047 - SAKAMAKI HALL

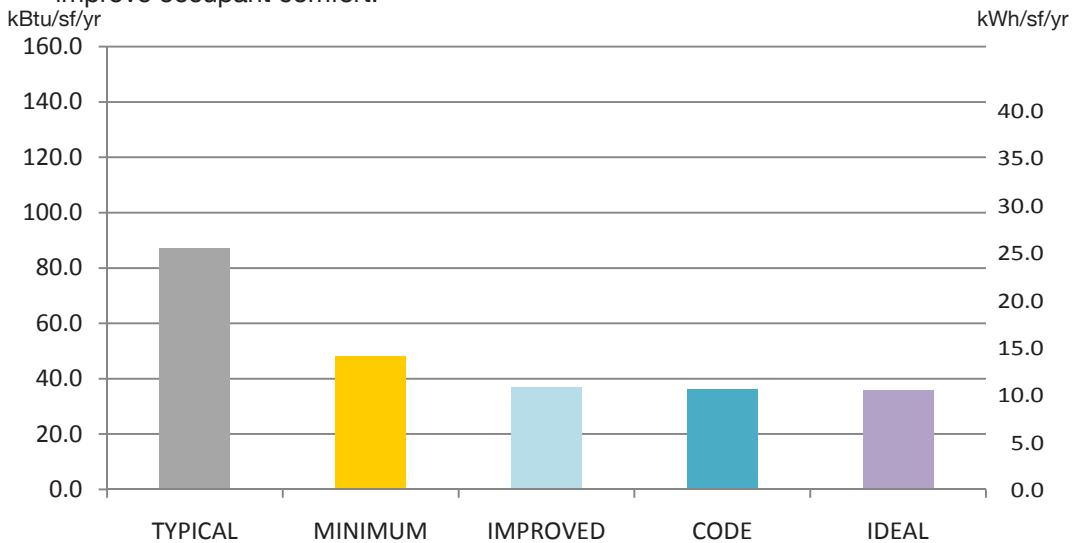
Add/D.1 Executive Summary (Continued)

b. Office Model Results

On average, for all orientations, offices in existing UHM buildings (Typical Existing) would use 87.3 kBtu/sqft/yr (25.6 kWh/sqft/yr). These results are higher than the CBECS data for similar building types in the same climate zone, due probably to non UHM buildings being included in the data.

By improving the windows (glazing specifications, installing shading devices and making those windows operable), in Addition to controlling the time the lights are on and effectively reducing the lighting loads during daytime hours (Minimum Suite), total energy use is reduced by 45%. This is due to both the reduction in lighting energy use (50%) but also the impact of turning off the lights on the interior temperature and consequently on the cooling energy needed for each classroom (48% reduction).

Adding IECC 2015 prescriptive requirements for the roof (Improved Suite), further reduces the energy use intensity to 58% less than typical existing conditions Other improvements such as IECC 2015 prescriptive wall specifications (Code Suite) and exposed thermal mass (Ideal Suite) do not have such a significant impact on the total energy use (59% less than typical maximum), although they improve occupant comfort.



	EUI (kBtu/sqft/yr)		Total Energy (Site) (kBtu)		Cooling (kBtu)		Lighting (kBtu)		Equipment (kBtu)		Reheat?
TYPICAL	87.3		205280		169237		22517		13414		113
MINIMUM	48.2	45%	113340	45%	88504	48%	11297	50%	13414		125
IMPROVED	37.0	58%	86937	58%	56240	67%	11297	50%	19004		395
CODE	36.3	58%	85288	58%	54561	68%	11297	50%	19004		425
IDEAL	35.8	59%	84254	59%	53474	68%	11297	50%	19004		479

Add/D.1 Executive Summary (Continued)

EUI (kWh/sqft/yr)	
TYPICAL	25.6
MINIMUM	14.1
IMPROVED	10.8
CODE	10.6
IDEAL	10.5

EUI (kWh/sqft/yr)			
<i>class/office</i>			
UHM Benchmarking Study 2004			
23.7			
CBECS		<i>by size</i>	<i>by age</i>
2003		10.5	15.9
Strategic Energy Plan 2011 data		30.6	



1020 - Q.L. CENTER FOR STUDENT SERVICES



1012 - INSTITUTE FOR ASTRONOMY

UHM OFFICE BUILDINGS - TYPICAL

Avg Size: 12,000 sqft
 Avg. Age: 45 years, built 1970
 Avg. EUI: 30.6 kWh/sf*

*Strategic Energy Plan 2011 data



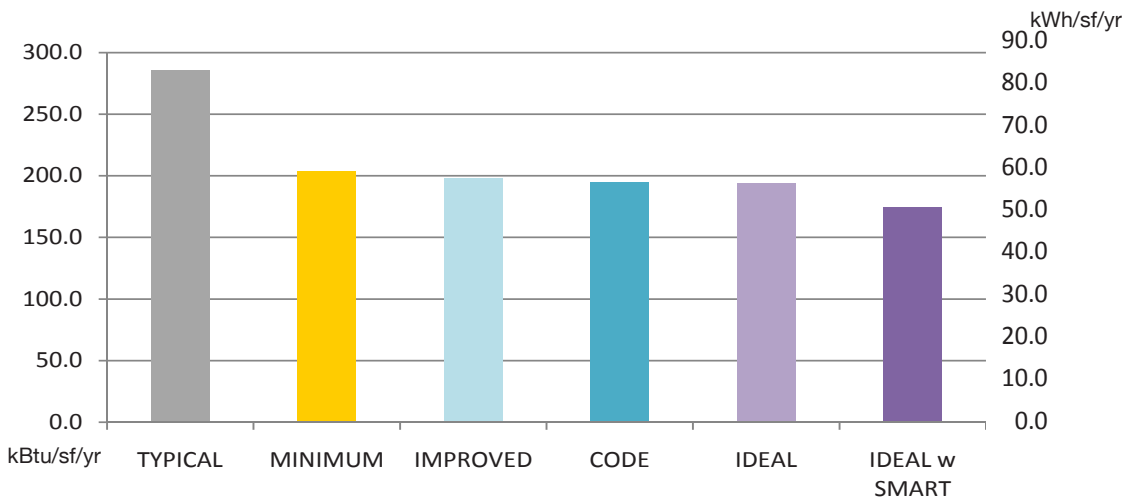
1011 - WOODLAWN BLDG.S

Add/D.1 Executive Summary (Continued)

c. Laboratory Model Results

In laboratory facilities, observation of facility operation reveals that laboratory air systems and the associated HVAC loads are the primary end-use of energy in UC laboratory buildings, averaging roughly three times the energy intensity of non-laboratory buildings (Huizenga, Van Liere and Bauman 1998).

The results from our models confirm these observations. On average, for all orientations, laboratories in existing UHM buildings (Typical Existing) would use 285.6.3 kBtu/sqft/yr (83.7 kWh/sqft/yr). The Labs 21 toolkit only provides energy use data for a subset of the database – facilities located in cool-humid climate zone, with total site energy use intensity that varies from about 200 kBtu/sf-yr to almost 600 kBtu/sf-yr. Labs 21 emphasizes the correlation between the energy use intensity and the lab area ratio, underscoring the importance of normalizing for this parameter when comparing labs. However, these values are out of range compared to both CBECS and UHM data. As mentioned before, the UHM data combines laboratory uses with offices and classrooms, which lowers the averaged energy use intensity.



	EUI (kBtu/sqft/yr)		Total Energy (Site) (kBtu)		Cooling (kBtu)		Lighting (kBtu)	Equipment (kBtu)	Reheat?
TYPICAL	285.6		671378		409550		42910	218907	6
MINIMUM	203.9	29%	479322	29%	335037	18%	11755	131344	594
IMPROVED	198.2	31%	465859	31%	321613	21%	11755	131344	576
CODE	195.1	32%	458513	32%	314241	23%	11755	131344	589
IDEAL	193.7	32%	455161	32%	310882	24%	11755	131344	592
IDEAL w SMART	174.3	39%	409599	39%	265743	35%	11755	131344	391

Add/D.1 Executive Summary (Continued)

Simulations for improved suites show that lighting energy use can be reduced by 73% on average for all orientations and that cooling energy use and total energy use intensity Achieve up to 32% reductions with overestimated airflow rates or up to 39% reductions if airflow rates follow the best-practices recommendations

	EUI (kWh/sqft/yr)
TYPICAL	83.7
MINIMUM	59.8
IMPROVED	58.1
CODE	57.2
IDEAL	56.8
IDEAL w SMART	51.1

	EUI (kWh/sqft/yr)		
	lab/class	lab/class/office	office/lab
UHM Benchmarking Study 2004	64.3	44.7	34.7
CBECs 2003	by size	by age	by use
	15.7	15.9	23.1
Strategic Energy Plan 2011 data	35.6		



C-More Hale, Most recent Laboratory Building on UHM campus

Avg Size: 54,900 sqft
 Avg. Age: 45 years, built 1970
 Avg. EUI: 35.6 kWh/sf*

*Strategic Energy Plan 2011 data

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Add/D ENERGY STUDIES

2. MODEL ASSUMPTIONS

All assumptions are the same as for the HVAC Autonomy/ Thermal Comfort Models. The models also now use a purchased air system where the supply air temperature is at 13C. The thermostat set-point for cooling is either 25C (77F) or 27C (80.6F). The system has a differential dry bulb economizer that will use the outside air if the outside air temperature is below the cooling set-point.

It is also important to note that the controls for the HVAC system in these simulations are not fine tuned to mixed mode conditioning. This means that the system is available at all times and brings in the required airflow rates for breathing (and one Additional Air Change per Hour for some models) whenever cooling is not needed.

We have prepared a template summarizing the critical information per building type, that should be included in the “project definition” and submitted to the design teams for both new or retrofit projects, in order to provide useful assumptions for predictive performance models.

Information included in these templates would be as follows:

1. Energy Benchmarks:

By Building Type (for new building projects) + Building Specific (for renovation projects), UHM data::

- Average Size / Building Squarefootage
- Average Age / Year built
- Average Energy Use Intensity / Total Energy Use
- Average or Total Lighting Energy Use
- Average or Total HVAC Energy Use
- Average or Total Equipment Energy Use
- Average Water Use / Total Water Use

2. Internal loads::

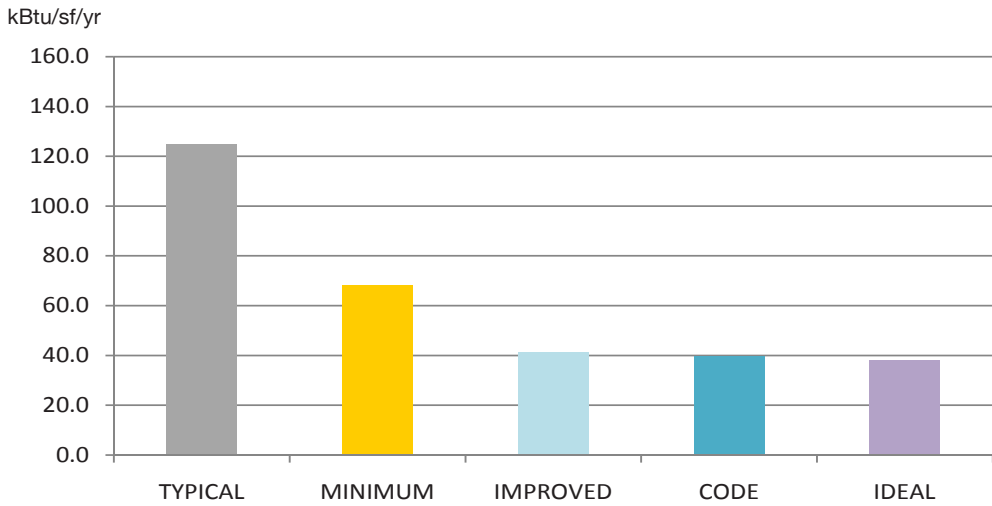
Typical occupancy (sft/ person)

Typical existing Lighting Power and Equipment Power Density

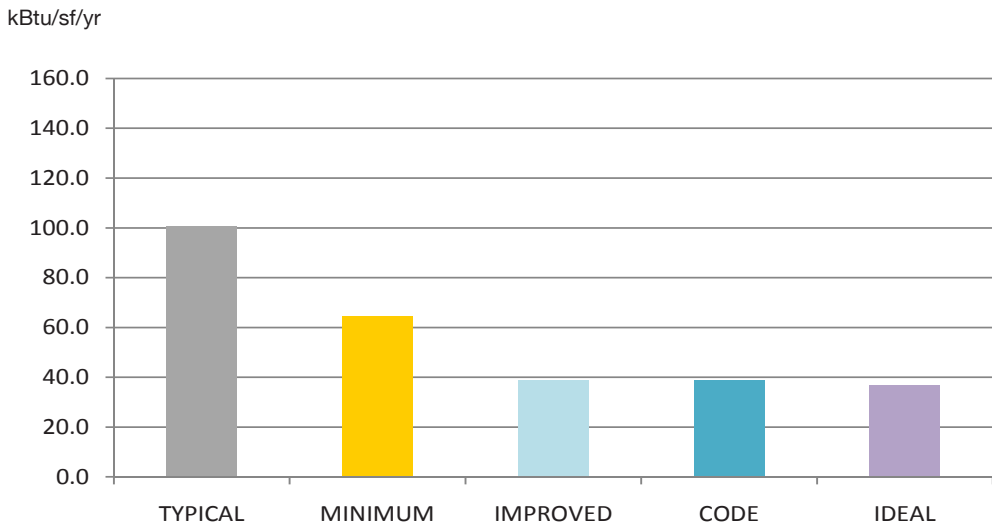
Typical Schedules

Add/D ENERGY STUDIES

3. CLASSROOM ANALYSIS

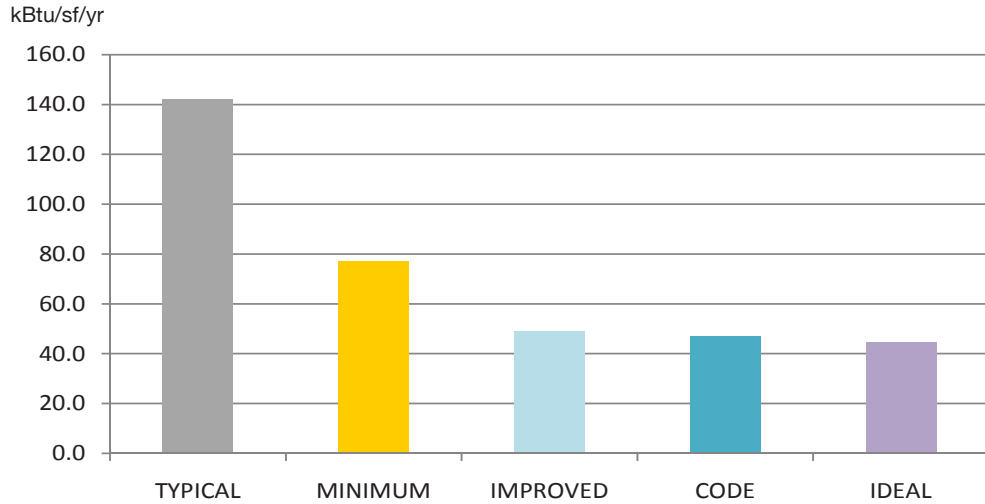


	EUI (kBtu/sqft/yr)	Total Energy (Site) (kBtu)	Cooling (kBtu)	Lighting (kBtu)	Equipment (kBtu)	Reheat?
TYPICAL	125.0	293834	262447	22177	8942	267
MINIMUM	68.0	159860	145828	4879	8942	211
IMPROVED	41.3	97037	79738	4879	11625	794
CODE	39.8	93636	76259	4879	11625	873
IDEAL	37.9	89150	71571	4879	11625	1075

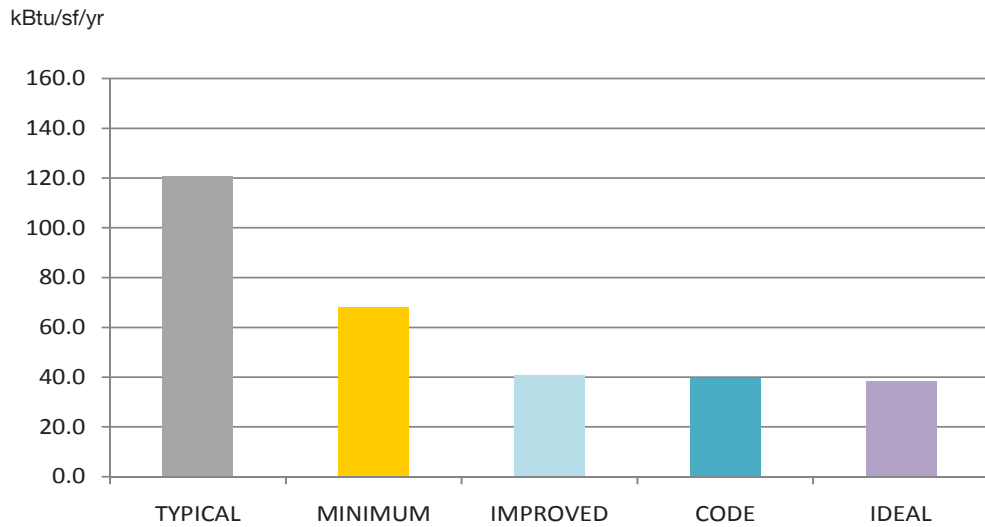


	EUI (kBtu/sqft/yr)	Total Energy (Site) (kBtu)	Cooling (kBtu)	Lighting (kBtu)	Equipment (kBtu)	Reheat?
TYPICAL	100.4	236080	204768	22177	8942	192
MINIMUM	64.3	151119	135537	6438	8942	201
IMPROVED	38.9	91377	72868	6438	11625	445
CODE	38.9	91396	72814	6438	11625	518
IDEAL	36.8	86449	67804	6438	11625	581

Add/D.3 Classroom Analysis (Continued)



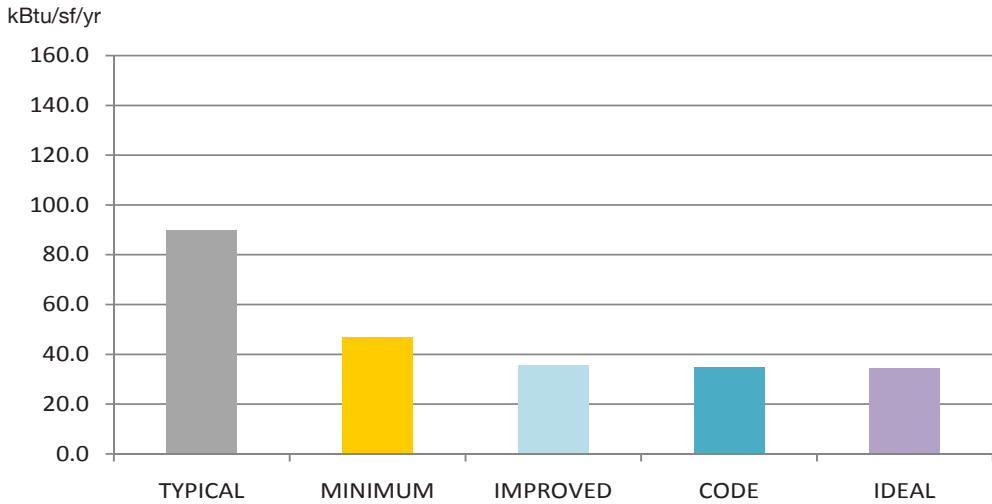
	EUI (kBtu/sqft/yr)	Total Energy (Site) (kBtu)	Cooling (kBtu)	Lighting (kBtu)	Equipment (kBtu)	Reheat?
TYPICAL	142.2	334149	302794	22177	8942	235
MINIMUM	77.2	181380	166574	5640	8942	224
IMPROVED	49.0	115159	97074	5640	11625	820
CODE	46.9	110121	91996	5640	11625	860
IDEAL	44.7	104973	86722	5640	11625	986



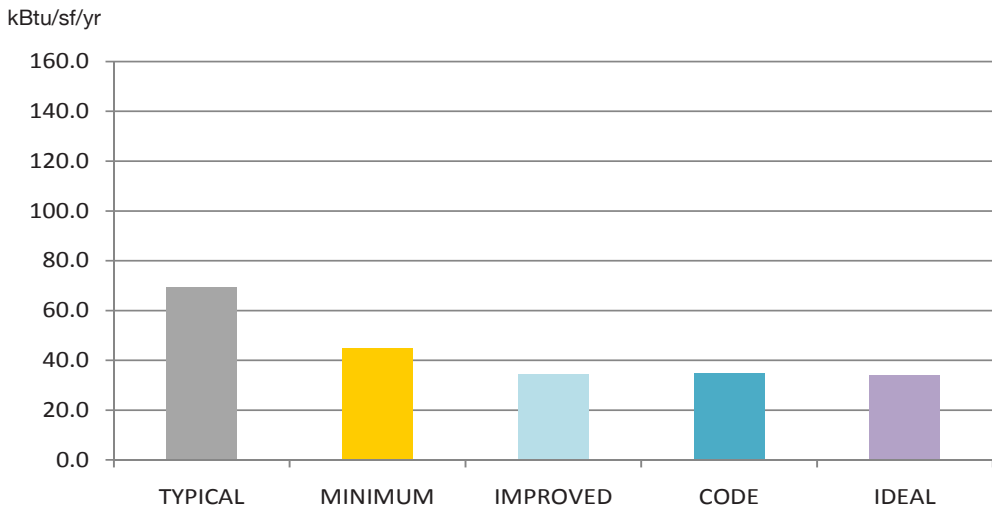
	EUI (kBtu/sqft/yr)	Total Energy (Site) (kBtu)	Cooling (kBtu)	Lighting (kBtu)	Equipment (kBtu)	Reheat?
TYPICAL	120.7	283744	252387	22177	8942	236
MINIMUM	68.3	160458	146157	5145	8942	214
IMPROVED	40.8	95916	78486	5145	11625	660
CODE	39.8	93538	76075	5145	11625	692
IDEAL	38.2	89861	72311	5145	11625	780

Add/D ENERGY STUDIES

4. OFFICE ANALYSIS

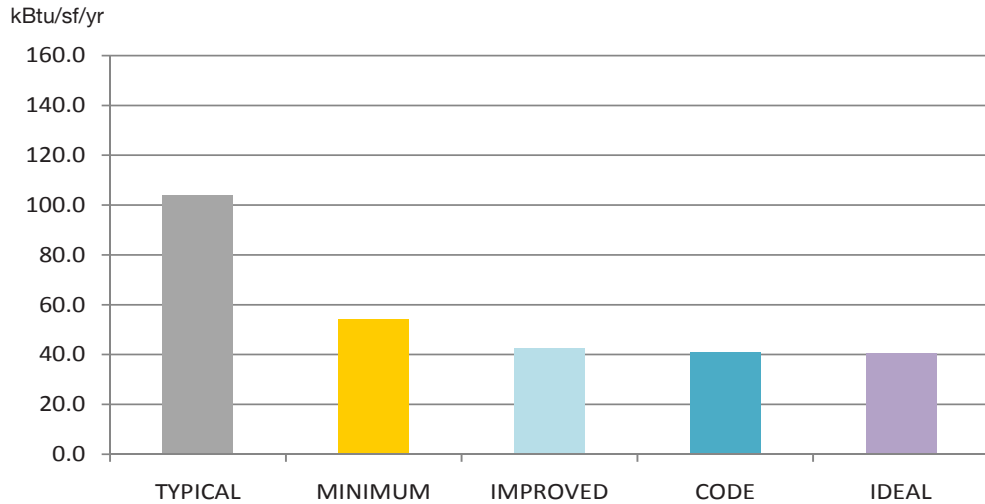


	EUI (kBTu/sqft/yr)	Total Energy (Site) (kBtu)	Cooling (kBtu)		Lighting (kBtu)		Equipment (kBtu)	Reheat?
TYPICAL	90.1	211807	175767		22517		13414	109
MINIMUM	46.9	110148	86403	103%	10208	55%	13414	124
IMPROVED	35.5	83488	53862	69%	10208	55%	19004	414
CODE	34.7	81468	51818	71%	10208	55%	19004	438
IDEAL	34.2	80483	50762	71%	10208	55%	19004	509

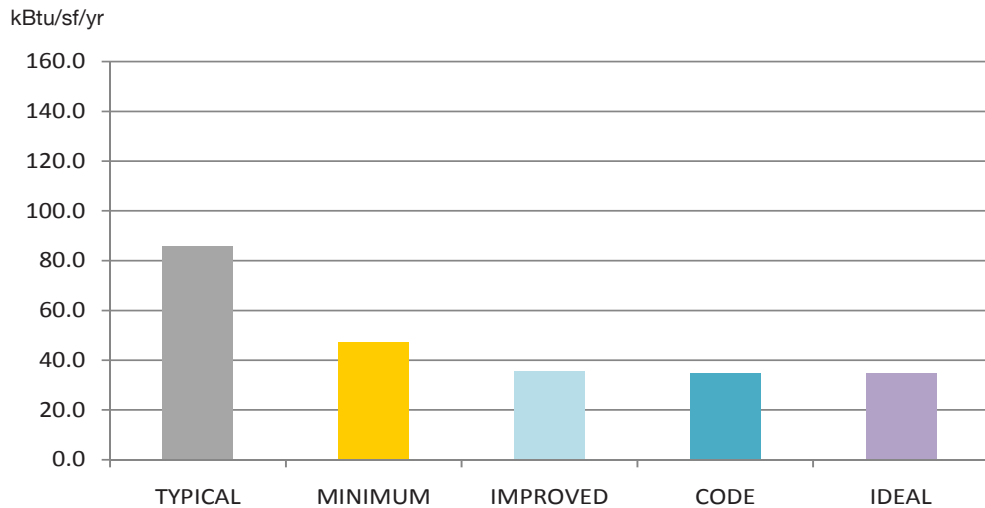


	EUI (kBTu/sqft/yr)	Total Energy (Site) (kBtu)	Cooling (kBtu)		Lighting (kBtu)		Equipment (kBtu)	Reheat?
TYPICAL	69.1	162507	126456		22517		13414	121
MINIMUM	44.8	105308	78774	39%	12988	42%	13414	132
IMPROVED	34.5	81026	48687	61%	12988	42%	19004	347
CODE	34.6	81325	48944	61%	12988	42%	19004	388
IDEAL	34.1	80198	47790	62%	12988	42%	19004	416

Add/D.4 Office Analysis (Continued)



	EUI (kBTu/sqft/yr)	Total Energy (Site) (kBTu)	Cooling (kBTu)	Lighting (kBTu)	Equipment (kBTu)	Reheat?
TYPICAL	104.2	244816	208777	22517	13414	108
MINIMUM	54.2	127323	102443	11342	13414	125
IMPROVED	42.5	99899	69144	11342	19004	409
CODE	41.0	96401	65623	11342	19004	432
IDEAL	40.4	94855	64009	11342	19004	500

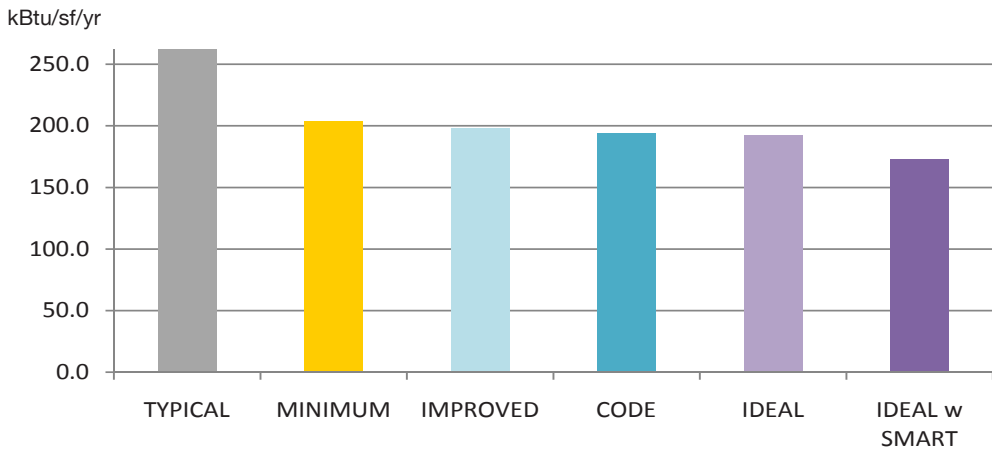


	EUI (kBTu/sqft/yr)	Total Energy (Site) (kBTu)	Cooling (kBTu)	Lighting (kBTu)	Equipment (kBTu)	Reheat?
TYPICAL	85.9	201991	165947	22517	13414	114
MINIMUM	47.0	110579	86395	10651	13414	120
IMPROVED	35.5	83335	53269	10651	19004	411
CODE	34.9	81958	51860	10651	19004	443
IDEAL	34.7	81481	51336	10651	19004	490

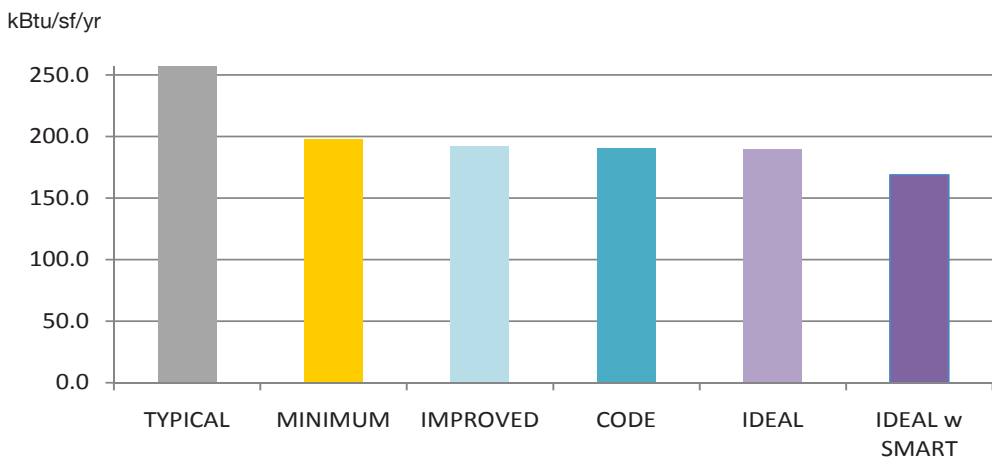
4 / ENERGY

Add/D ENERGY STUDIES

5. LABORATORY ANALYSIS

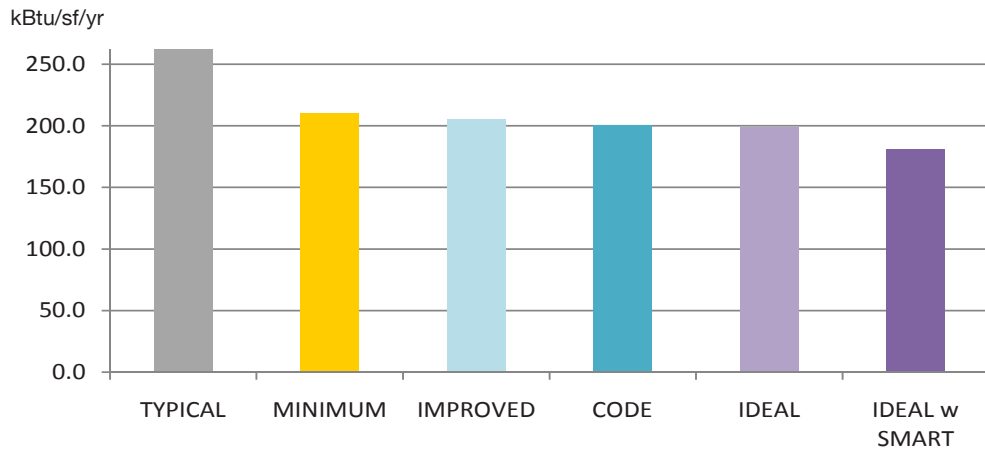


	EUI (kBTu/sqft/yr)	Total Energy (Site) (kBtu)	Cooling (kBtu)		Lighting (kBtu)		Equipment (kBtu)		Reheat?
TYPICAL	286.8	674007		412181		42910	218907		9
MINIMUM	203.5	478351	29%	334088	19%	11741	131344	40%	1178
IMPROVED	197.7	464719	31%	320466	22%	11741	131344	40%	1168
CODE	194.2	456554	32%	312267	24%	11741	131344	40%	1202
IDEAL	192.7	452861	33%	308554	25%	11741	131344	40%	1222
IDEAL w SMART	173.0	406684	40%	262938	36%	11741	131344	40%	661

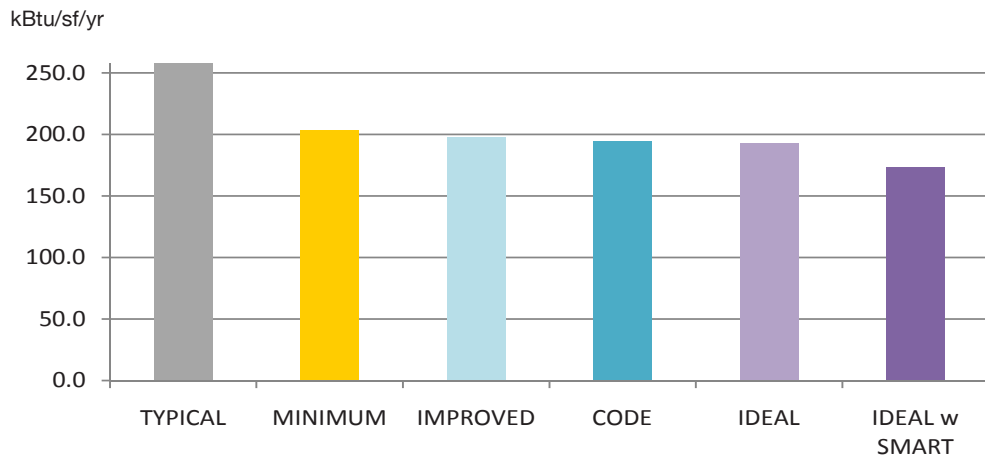


	EUI (kBTu/sqft/yr)	Total Energy (Site) (kBtu)	Cooling (kBtu)		Lighting (kBtu)		Equipment (kBtu)		Reheat?
TYPICAL	271.2	637387		375555		42910	218907		15
MINIMUM	198.1	465526	27%	321135	14%	11849	131344	72%	1198
IMPROVED	192.2	451696	29%	307369	18%	11849	131344	72%	1133
CODE	190.7	448147	30%	303799	19%	11849	131344	72%	1154
IDEAL	189.6	445706	30%	301367	20%	11849	131344	72%	1146
IDEAL w SMART	168.9	396983	38%	252885	33%	11849	131344	72%	904

Add/D.5 Laboratory Analysis (Continued)



	EUI (kBtu/sqft/yr)	Total Energy (Site) (kBtu)	Cooling (kBtu)	Lighting (kBtu)	Equipment (kBtu)		Reheat?			
TYPICAL	302.3	710509	448680	42910	218907		12			
MINIMUM	210.7	495257	30%	350824	22%	11963	72%	131344	40%	1126
IMPROVED	205.3	482634	32%	338211	25%	11963	72%	131344	40%	1117
CODE	200.9	472194	34%	327739	27%	11963	72%	131344	40%	1148
IDEAL	199.1	467901	34%	323419	28%	11963	72%	131344	40%	1175
IDEAL w SMART	181.4	426473	40%	282501	37%	11963	72%	131344	40%	666



	EUI (kBtu/sqft/yr)	Total Energy (Site) (kBtu)	Cooling (kBtu)	Lighting (kBtu)	Equipment (kBtu)		Reheat?			
TYPICAL	282.4	663611		401786	42910		218907		8	
MINIMUM	203.5	478154	28%	334100	17%	11467	73%	131344	40%	1243
IMPROVED	197.6	464386	30%	320405	20%	11467	73%	131344	40%	1171
CODE	194.5	457158	31%	313159	22%	11467	73%	131344	40%	1188
IDEAL	193.3	454174	32%	310189	23%	11467	73%	131344	40%	1174
IDEAL w SMART	173.7	408255	38%	264647	34%	11467	73%	131344	40%	797

Add/D ENERGY STUDIES**6. NET ZERO FEASIBILITY**

A preliminary basic net zero feasibility study assuming potential PV output for both typical and high performance PV panels in this climate was developed to establish the potential of each building type from achieving the net zero performance goal.

We modeled generic PV performance for a panel mounted horizontally in order to establish a relationship between effective (vs nameplate) total PV array power rating and yearly energy production. We performed this analysis using PVWatts, a tool for estimating PV energy production. PVWatts was created by and is maintained through the National Renewable Energy Laboratory (NREL). We analyzed the performance of a generic 1 kW system using degradation factors slightly greater than the default settings used in PVWatts.

See below for a summary of assumptions used in the analysis:

Location and Station Identification

Requested Location	96822
Weather Data Source	(TMY3) HONOLULU INTL ARPT, HI 7.6 mi
Latitude	21.32° N
Longitude	157.93° W

PV System Specifications

DC System Size	1 kW
Module Type	Standard
Array Type	Fixed (open rack)
Array Tilt	0°
Array Azimuth	180°
System Losses	14%
Inverter Efficiency	96%
DC to AC Size Ratio	1.1

PV kWh per kW installed 1,454 kWh per kW.

In summary, as described in the table shown in the next page, for both the classrooms and the offices, only the Improved, Code and Ideal Suites have the potential for Achieving net zero performance in two story buildings. Office buildings have the greatest potential to be net zero as they Achieve the best energy performance results in our models. Laboratory buildings are unlikely to achieve net zero performance as long as the PVs must be roof mounted on the building itself, and limited to the roof area.

Add/D.6 Net Zero Feasibility (Continued)

Month	Solar Radiation (kWh / m2 / day)	AC Energy (kWh)	Energy Value (\$)
January	3.81	90	29
February	4.49	96	31
March	5.25	124	40
April	5.74	132	43
May	6.16	144	47
June	6.39	146	47
July	6.41	150	49
August	6.40	149	48
September	5.82	132	43
October	4.79	111	36
November	4.11	94	31
December	3.65	86	28
Annual	5.25	1,454 kWh	\$ 472

A typical PV panel (230 Watts per 17.5sqft) would produce 18.9 kWh/sqft

A high performance panel (335 Watts per 17.5 sqft) would produce 27.6 kWh/sqft

CLASSROOMS	Energy use	Net Performance (Single Story)	
	EUI (kWh/sqft/yr)	w typical PV panel	w high performance PV panel
TYPICAL	35.78	16.88	8.15
MINIMUM	20.35	1.45	-7.28
IMPROVED	12.45	-6.45	-15.17
CODE	12.12	-6.79	-15.51
IDEAL	11.55	-7.36	-16.08

OFFICES	Energy use	Net Performance (Single Story)	
	EUI (kWh/sqft/yr)	w typical PV panel	w high performance PV panel
TYPICAL	25.60	6.69	-2.03
MINIMUM	14.13	-4.77	-13.49
IMPROVED	10.84	-8.06	-16.79
CODE	10.63	-8.27	-16.99
IDEAL	10.51	-8.40	-17.12

LABORATORIES	Energy use	Net Performance (Single Story)	
	EUI (kWh/sqft/yr)	w typical PV panel	w high performance PV panel
TYPICAL	83.72	64.81	56.09
MINIMUM	59.77	40.87	32.14
IMPROVED	58.09	39.19	30.46
CODE	57.17	38.27	29.55
IDEAL	56.75	37.85	29.13
IDEAL w SMART	51.07	32.17	23.45

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Add/E. EFFICIENT ELECTRIC LIGHTING EXAMPLES

Daylighted spaces and reducing the demand of electric lights are an important part of reducing energy consumption. Per the Benchmarking Study for UHM, 2004, Lighting accounts for 30% of all electricity consumption on the UHM campus.

Reducing use of electric lights by good daylighting design is the most effective way of saving energy from lighting loads while maintaining comfortably illuminated spaces. Electric Lighting and controls should be designed to supplement daylight only as needed in the daytime, and to provide a comfortably illuminated spaces at night with minimal energy use.

The University of Hawaii's outdated lighting standard was updated in 2011 to reflect current standards and to be consistent with both the campus wide energy goals.

Superceded standard:

d. Foot candles:

- i. Minimum uniform light level at desk height is to be 50 FC, after bulb burn-in and after dirt level.
- ii. Final lighting (with all lights fully on and none dimmed) FC measurement to be in 12 spots from front to back, thus: IL IC IR (Instructor left section, center section and right section) FL FC FR (Front row seating, left, center and right at any seat in each section) CL CC CR (Center row seating, left, center and right at any seat in each section) BL BC BR (Back row seating, left, center and right at any seat in each section)
- iii. These 12 measurements will be averaged to check the 50 FC in each classroom before project closeout - any "under-designs", especially at corners, will require Additional placements of light fixtures as part of errors and omissions.

Revised standard:

d. Light Levels:

- i. Average maintained lighting at work surfaces shall be 30fc, with minimum of 25fc
- ii. Measurements shall be taken at least 3' from any wall on a 5' grid.
- iii. Measurements shall be taken with an illuminance meter with a valid calibration

Add/E Efficient Electric Lighting Design Examples (Continued)

certificate.

iv. Measurements shall be taken with non-dimmed warmed up lamps after a 10-hour burn in before project closeout. If measured lighting is below 15% of recommended measurements then adjustments, Additional placements, or reconfiguration of light fixtures will be required as part of errors and omissions.

The following pages show a compilation of examples of efficient lighting designs for the three space types Addressed in the modeling and Standards. These examples serve as a reference for the design teams and validate the assumptions made in thermal comfort and energy models using lower lighting power densities than those required by ASHRAE Standards.

In summary, the following assumptions are described through these examples:

- Classrooms 0.6 W/sqft, (examples show ranges between 0.44W/sqft and 0.56W/sqft)
- Offices 0.6 W/sqft, (examples show ranges between 0.3W/sqft and 0.56W/sqft)
- Labs 1 W/sqft. (examples several designs achieving 0.92W/sqft)

Add/E Efficient Electric Lighting Design Examples (Continued)

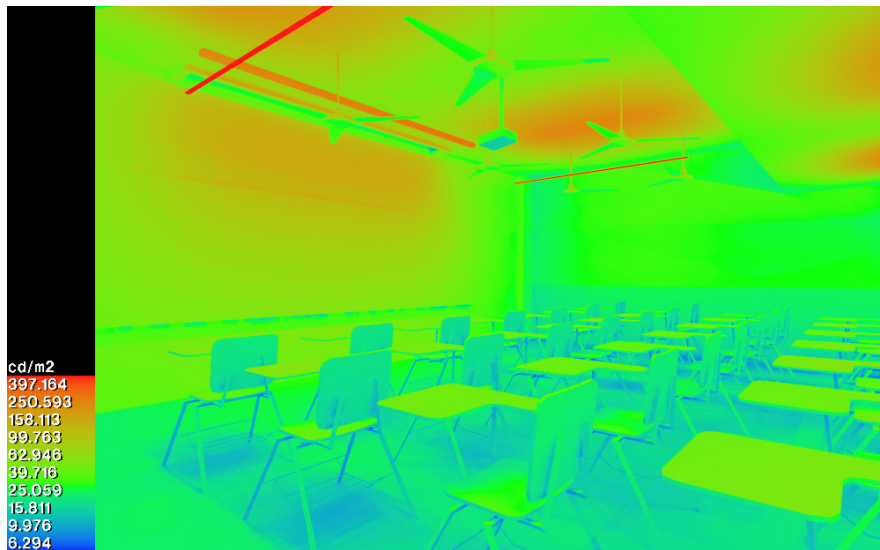
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Add/E EFFICIENT ELECTRIC LIGHTING DESIGN EXAMPLES

1. CLASSROOMS

Surface reflectances:

- Ceiling: 0.9
- Walls: 0.8
- Floor: 0.5
- Interior blinds
(deployed at night):
0.6



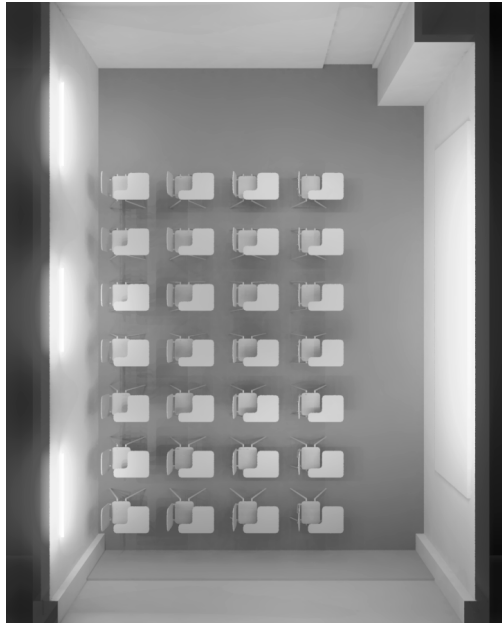
RADIANCE simulation showing luminance values of interior surfaces at night.

Add/E 1. Classrooms (Continued)

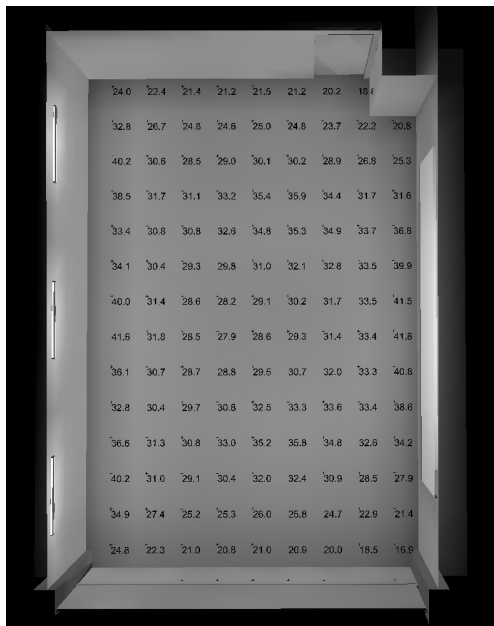
LPD:: 0.56 W/sqft

Statistics for points on 30" work-plane at least 3' from any wall:

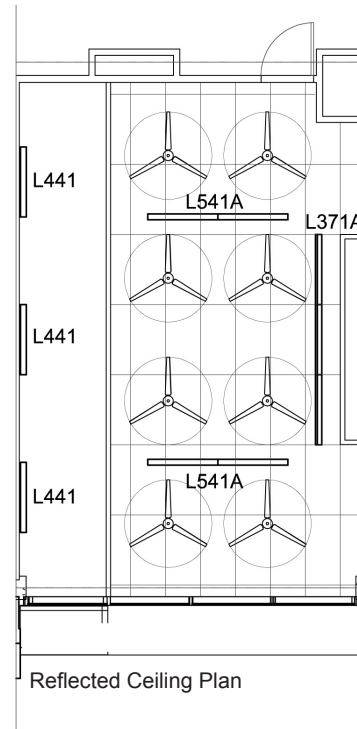
Average: 30.57 fc
 Maximum: 35.9 fc
 Minimum: 22.9 fc
 Avg/ Min Ratio: 1.33
 Max/Min Ratio: 1.57



RADIANCE simulation showing plan perspective.

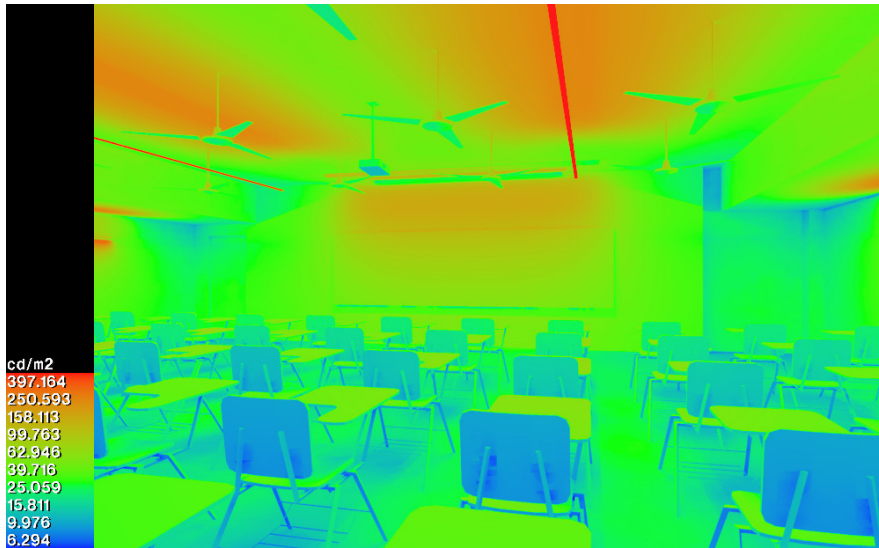


AGI simulation with illumination (fc) on 30" work-plane (2' calculation grid)



Reflected Ceiling Plan

Add/E.1 Classrooms (Continued)

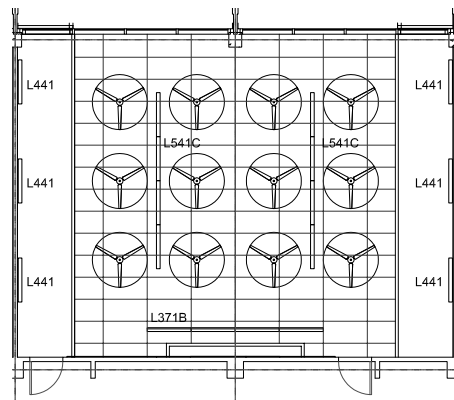
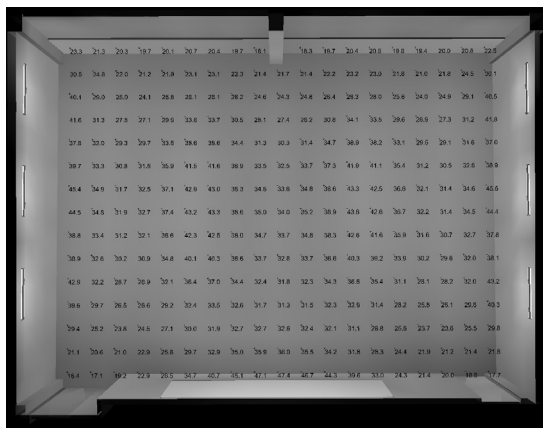
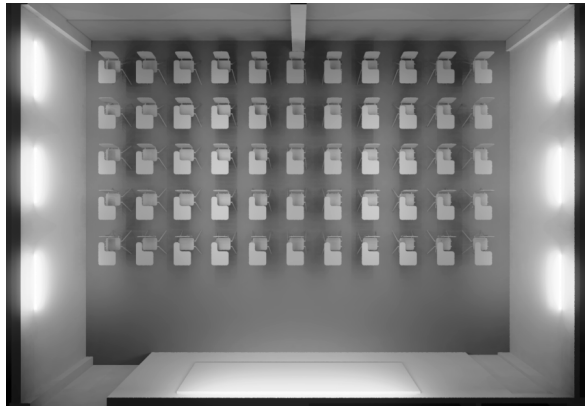


Add/E.1 Classrooms (Continued)

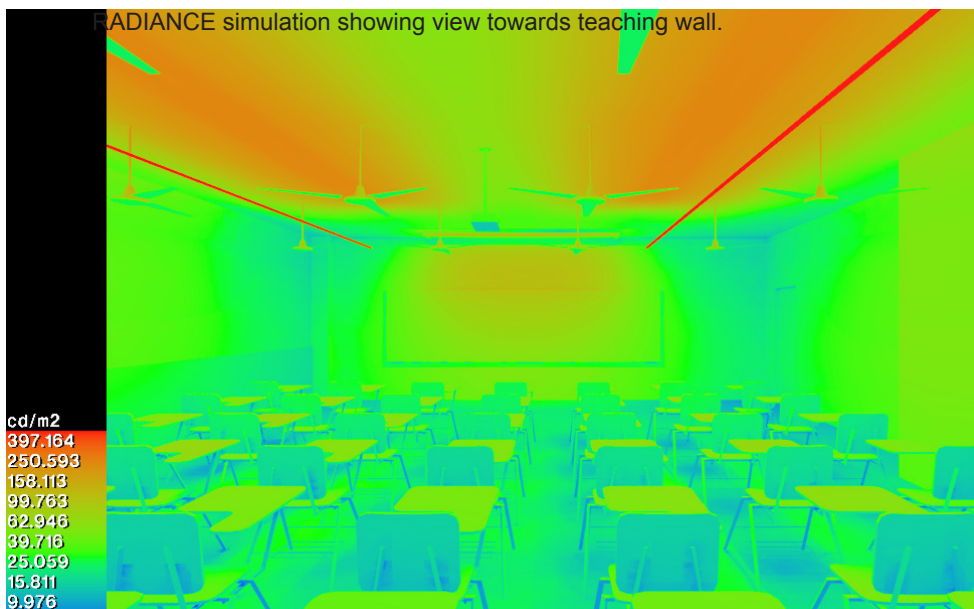
Statistics for points on 30" work-plane at least 3' from any wall:

LPD:: 0.50 W/sqft

Average:	32.72 fc
Maximum:	43.6 fc
Minimum:	23.6 fc
Avg/ Min Ratio:	1.39
Max/Min Ratio:	1.85



Add/E.1 Classrooms (Continued)



RADIANCE simulation showing luminance values of interior surfaces at night.

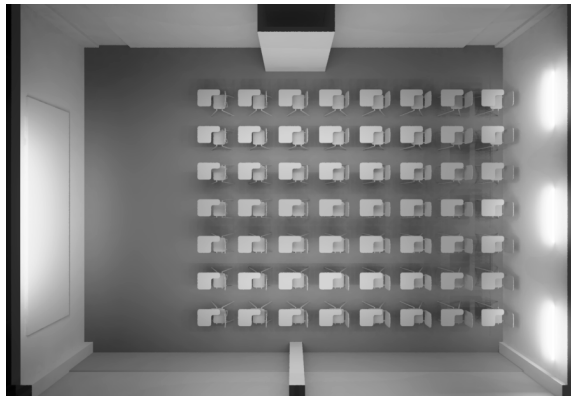
Add/E.1 Classrooms (Continued)

Statistics for points on 30" workplane at least 3' from any wall:

LPD:: 0.44 W/sqft

Average: 35.7 fc
 Maximum: 49.5 fc
 Minimum: 19.3 fc *
 Avg/ Min Ratio: 1.85
 Max/Min Ratio: 2.56

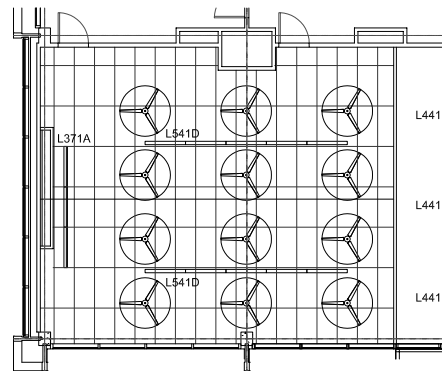
* Note:
 There are (2) points near northwest door which are below threshold of lighting standard. Per furniture plan, illumination at these points is not critical. Alternatively, pendants runs L541D could be lengthened from (5) to (6) fixtures each, resulting in an LPD of .5 W/sf for this room.



RADIANCE simulation showing plan perspective.



AGI simulation with illumination (fc) on 30" workplane (2' calculation grid)

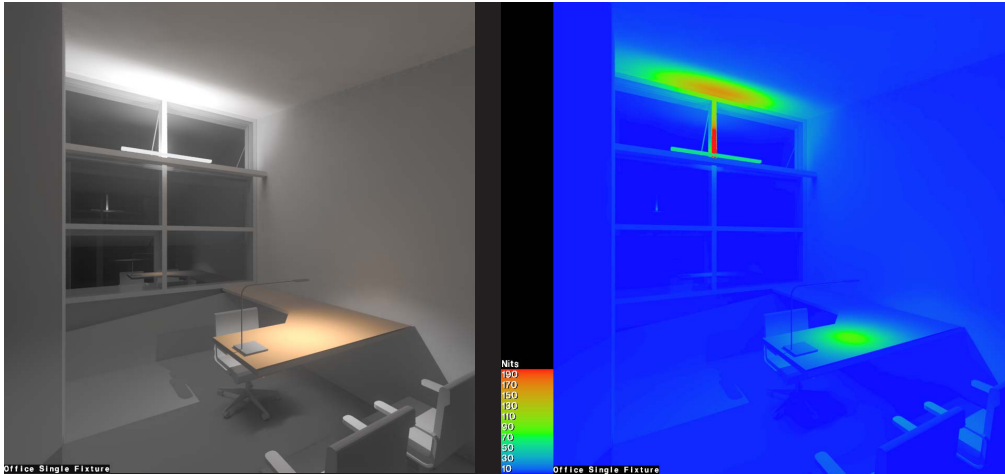


Reflected Ceiling Plan. Note that recess for screen to be moved to be centered on lighting fixture layout.

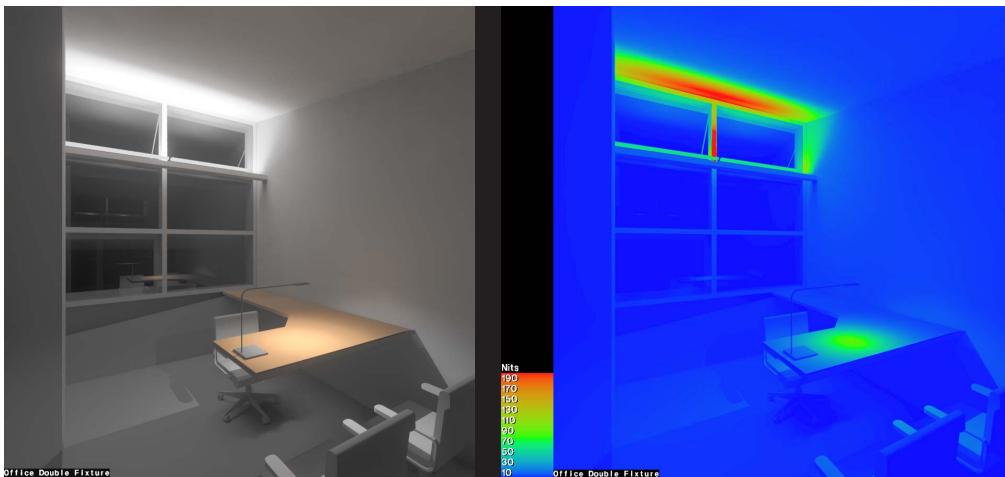
Add/E EFFICIENT ELECTRIC LIGHTING DESIGN EXAMPLES

2. OFFICES

LPD:: 0.3 W/sqft

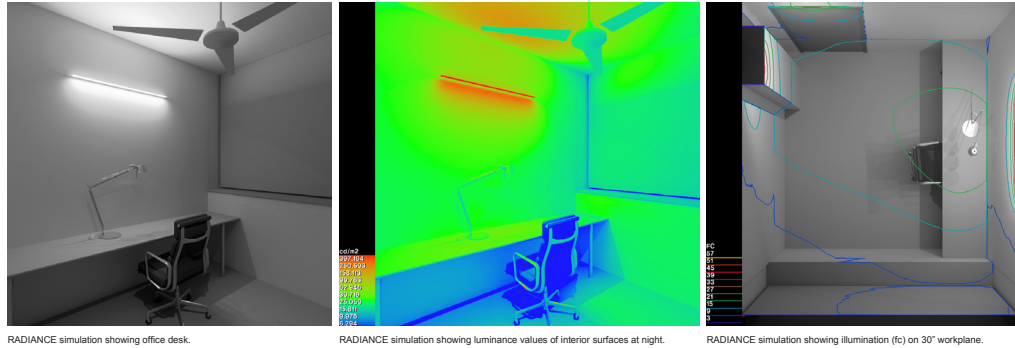


LPD:: 0.48 W/sqft



Add/E.2 Offices (Continued)

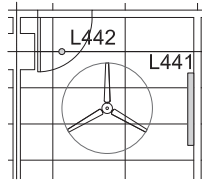
LPD:: 0.563 W/sqft



RADIANCE simulation showing office desk.

RADIANCE simulation showing luminance values of interior surfaces at night.

RADIANCE simulation showing illumination (fc) on 30° workplane.

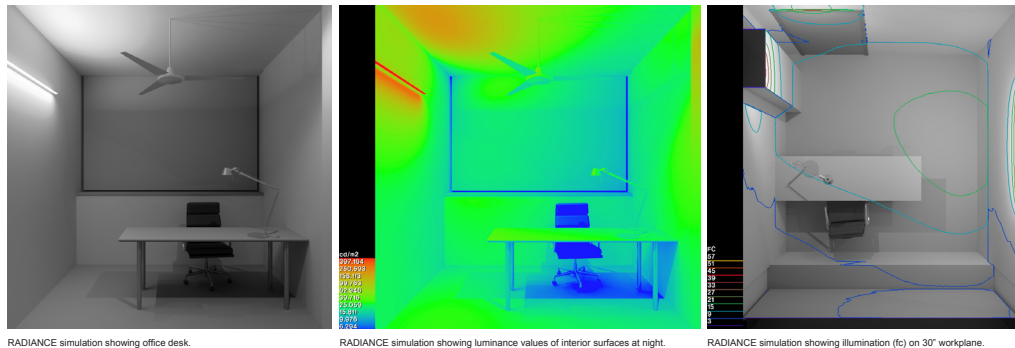


- (1) WALL MOUNTED CHOPSTICK (1T5)
- (1) RECESSED LED WALL WASHER DIRECTED TO COLUMN

LPD: 0.563 W/sf

DESK CONFIGURATION: aligned to side wall

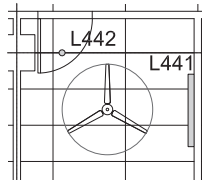
LPD:: 0.563 W/sqft



RADIANCE simulation showing office desk.

RADIANCE simulation showing luminance values of interior surfaces at night.

RADIANCE simulation showing illumination (fc) on 30° workplane.



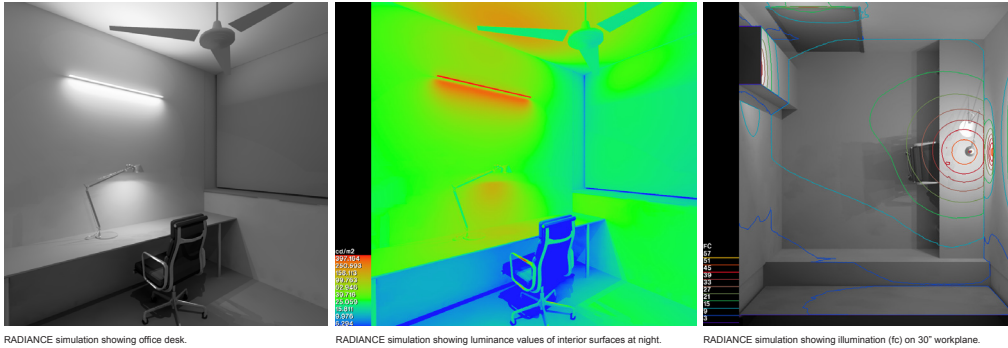
- (1) WALL MOUNTED CHOPSTICK (1T5)
- (1) RECESSED LED WALL WASHER DIRECTED TO COLUMN

LPD: 0.563 W/sf

DESK CONFIGURATION: centered in space

Add/E.2 Offices (Continued)

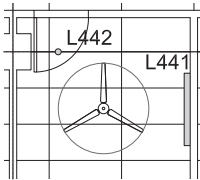
LPD:: 0.3 W/sqft



RADIANCE simulation showing office desk.

RADIANCE simulation showing luminance values of interior surfaces at night.

RADIANCE simulation showing illumination (fc) on 30° workplane.

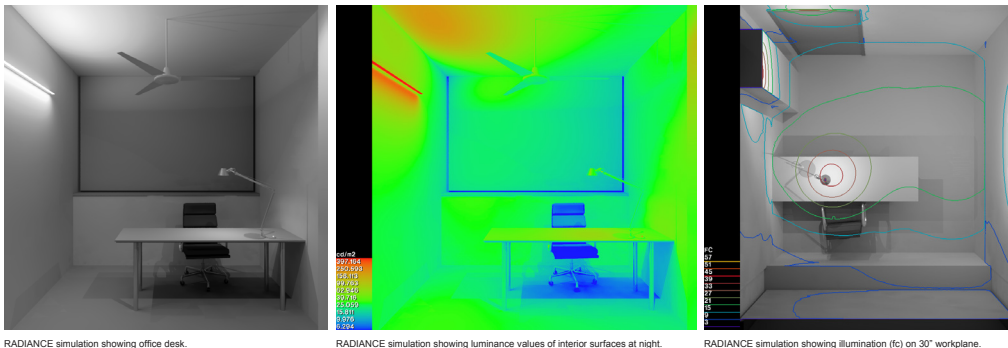


- (1) WALL MOUNTED CHOPSTICK (1T5)
- (1) RECESSED LED WALL WASHER DIRECTED TO COLUMN
- (1) LED POINT SOURCE TASKLIGHT

LPD: 0.649 W/sf

DESK CONFIGURATION: aligned to side wall

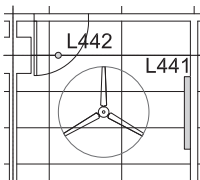
LPD:: 0.48 W/sqft



RADIANCE simulation showing office desk.

RADIANCE simulation showing luminance values of interior surfaces at night.

RADIANCE simulation showing illumination (fc) on 30° workplane.

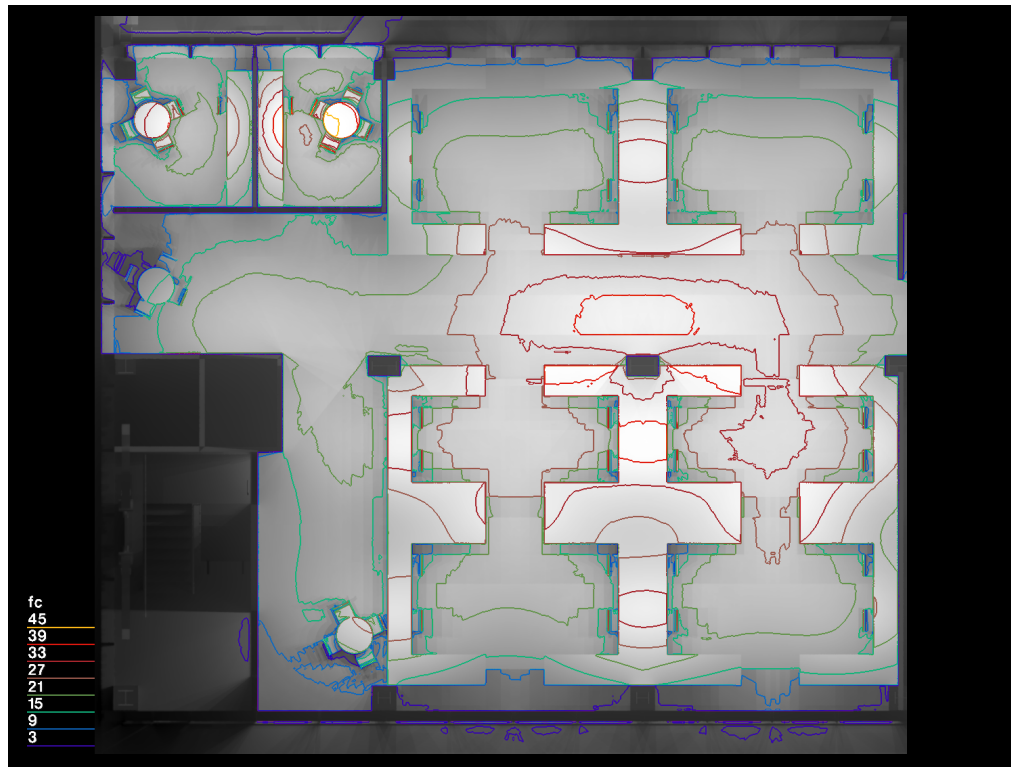
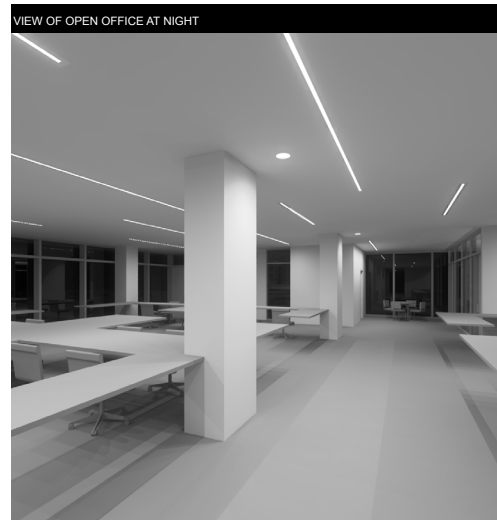


- (1) WALL MOUNTED CHOPSTICK (1T5)
- (1) RECESSED LED WALL WASHER DIRECTED TO COLUMN
- (1) LED POINT SOURCE TASKLIGHT

LPD: 0.649 W/sf

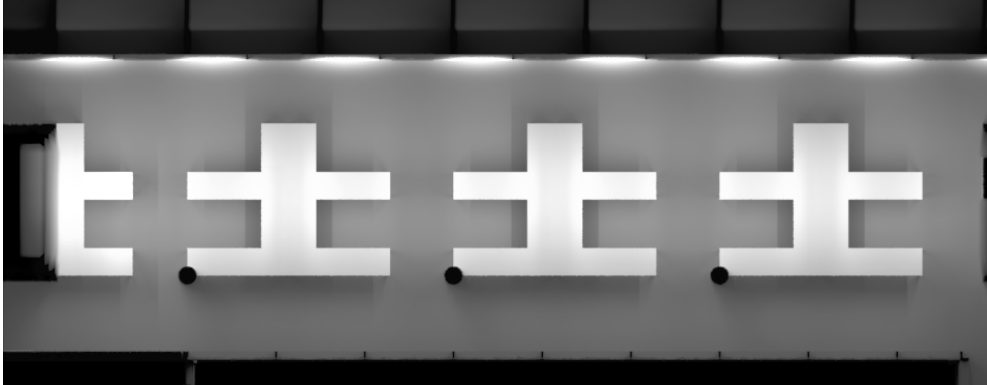
DESK CONFIGURATION: centered in space

Add/E.2 Offices (Continued)

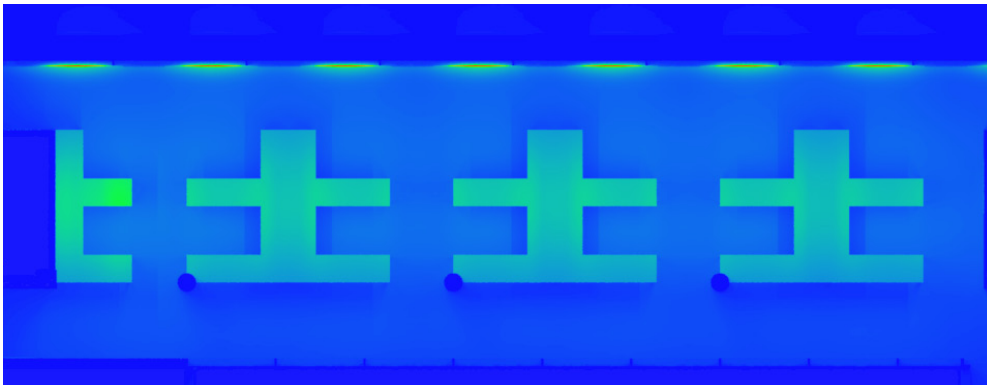


Add/E.2 Offices (Continued)

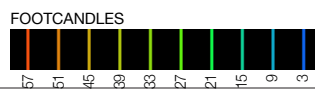
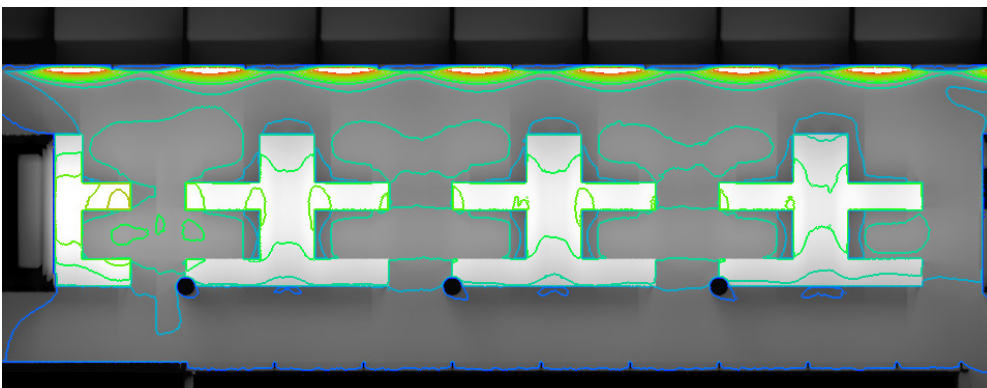
Top View Rendering



Falsecolor Luminance Map

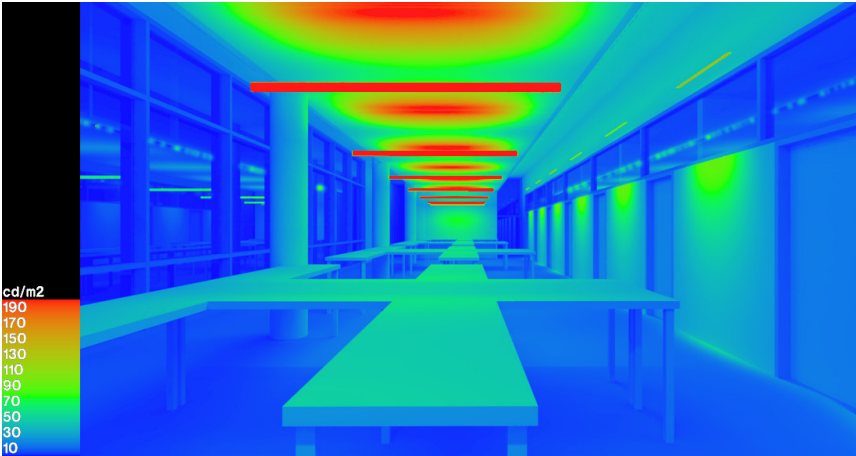


LPD:: 0.44 W/sqft

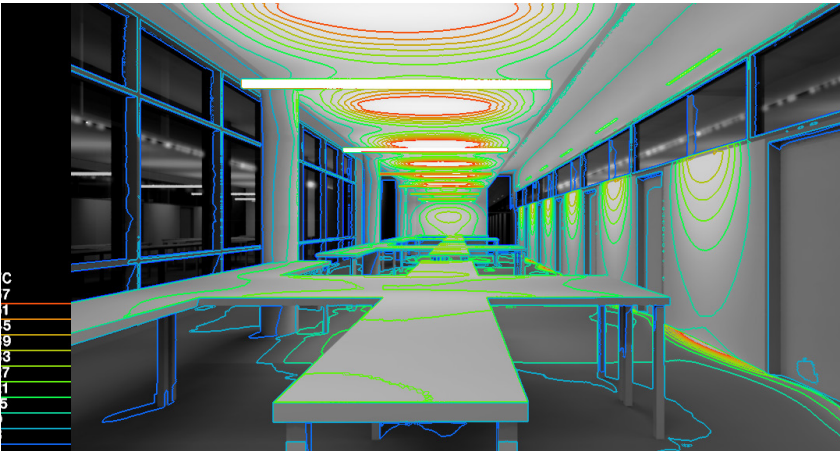


Add/E.2 Offices (Continued)

Perspective View Rendering



Falsecolor Luminance Map



Illuminance Contours

Add/E EFFICIENT ELECTRIC LIGHTING DESIGN EXAMPLES

3. LABORATORIES

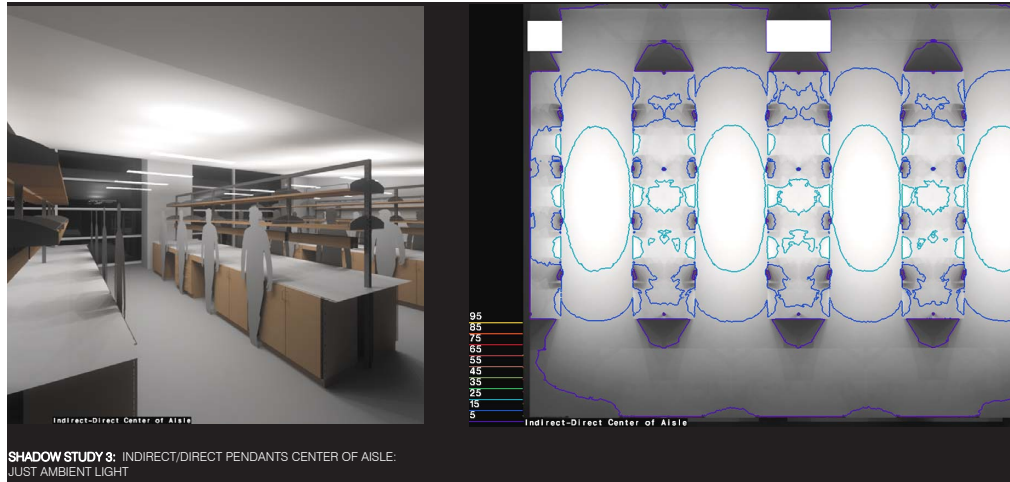
IESNA 1993 Recommended horizontal Fc for Laboratories	75-100Fc
IESNA 2000 Recommended Horizontal Fc for Laboratories	50Fc
Labs 21 Standard Practice Benchmark for task + Ambient	80-100Fc
Labs 21 Better Practice” benchmark for ambient lighting	30Fc
Labs 21 “Better Practice” Benchmark for task	50Fc

LPD:: 0.92 W/sqft

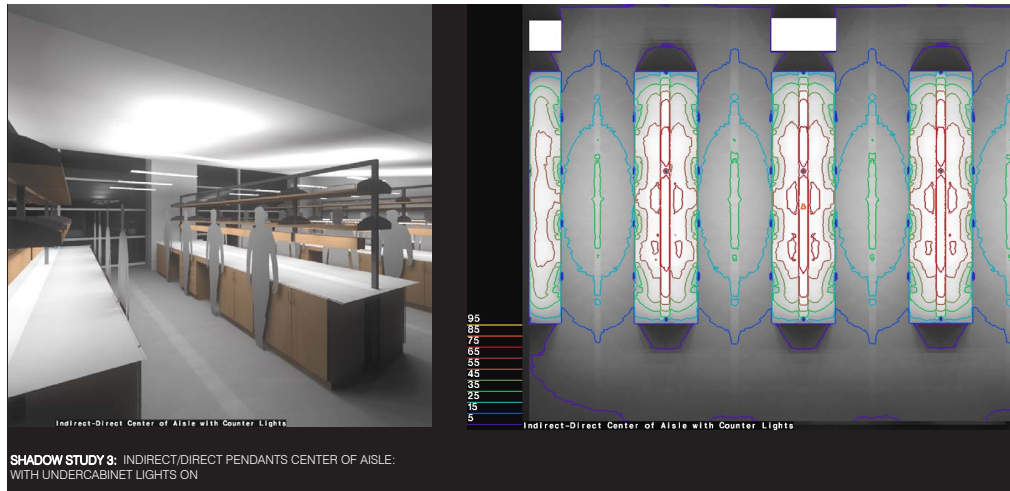


Add/E.3. Laboratories (Continued)

LPD:: 0.92 W/sqft



LPD:: 0.92 W/sqft



Ambient Lighting provided by daylight supplemented by indirect illumination with photo-sensor controls

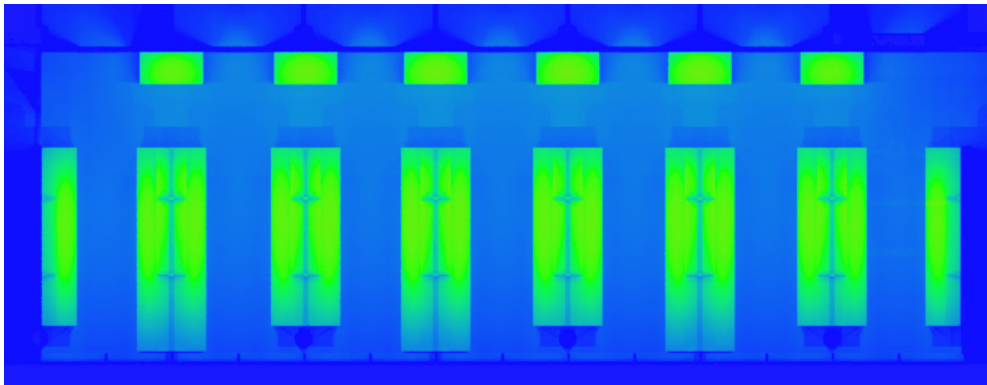
Task lighting provided on the bench by LED fixtures with occupancy controls.

Add/E.3. Laboratories (Continued)

Top View Rendering



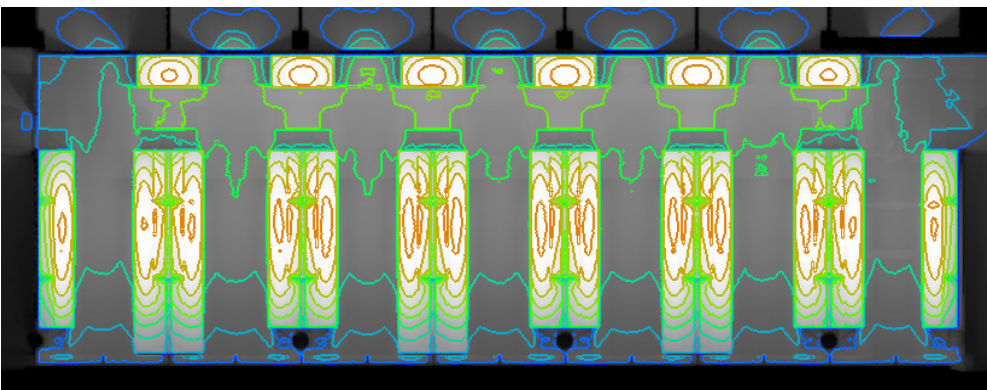
Falsecolor Luminance Map



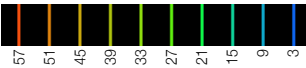
CD/M²



Illuminance Contours



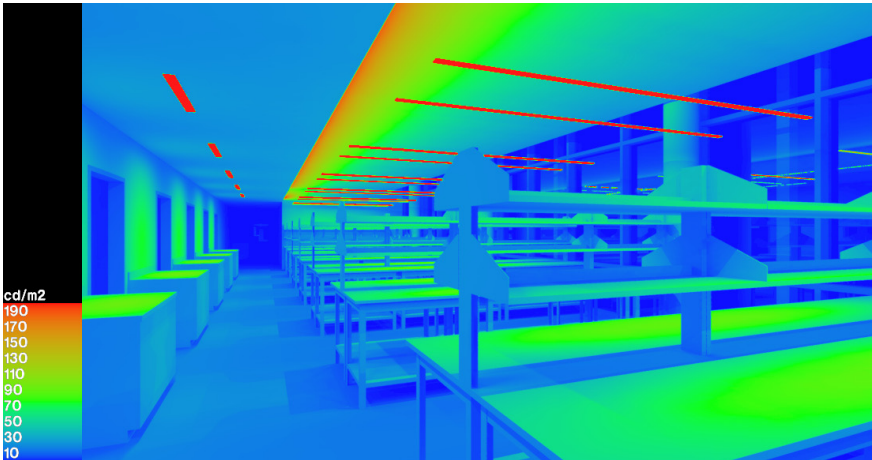
FOOTCANDLES



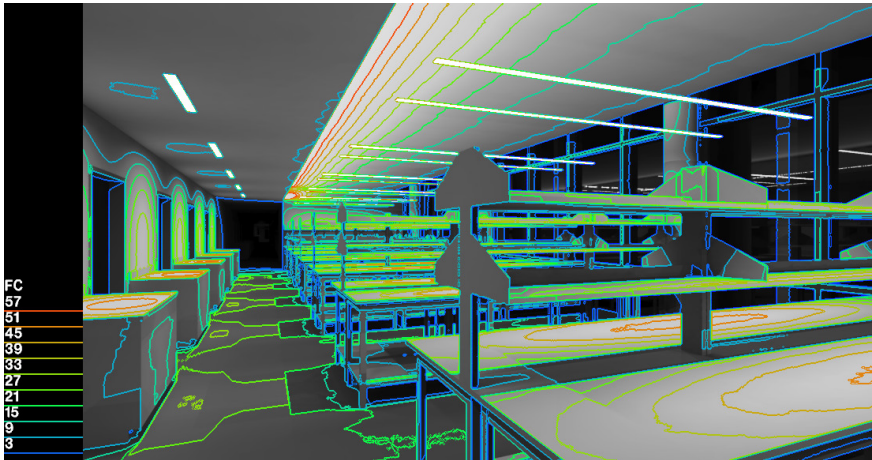
Note: Tasklights not included in simulation.
With tasklights, illumination levels on work surface will be increased by 40 to 60 footcandles, for a total of 60 to 100 footcandles.

Add/E.3. Laboratories (Continued)

Perspective View Rendering



Falsecolor Luminance Map



Illuminance Contours

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